

## Appropriations Requests for Legislatively Directed Spending Items

- 1. The sponsoring representative's first name: Jason
- 2. The sponsoring representative's last name: Woolford
- The cosponsoring representatives' names. All cosponsors must be listed. If none, please type 'n/a.' A signed letter from the sponsor approving the co-sponsorship and a signed letter from the member wishing to co-sponsor are required. Attach letters at question #9 below.
- 4. Name of the entity that the spending item is intended for: City of Howell
- 5. Physical address of the entity that the spending item is intended for: 611 E Grand River Ave Howell, MI 48843
- 6. If there is not a specific recipient, the intended location of the project or activity: I-96 and South Michigan Ave., Howell, MI 48843
- Name of the representative and the district number where the legislatively directed spending item is located: Representative Jason Woolford 50th House District
- 8. Purpose of the legislatively directed spending item. Please include how it provides a public benefit and why it is an appropriate use of taxpayer funding. Please also demonstrate that the item does not violate Article IV, S 30 of the Michigan Constitution. The Areas we have in need of infrastructure improvements are D-19 (S Michigan Ave) and the I-96 interchange. This interchange has been failing for over 4 decades and has had no to little funding made available to fix it. This interchange is the only direct connection to Howell City Downtown and Marion Township. Additionally, the City is seeking funds to help connect D-19 to Lucy Road, commonly called "the loop road". The need for this road to alleviate truck traffic from downtown has been compounded to include an emergency route and bypass when trains are blocking all City intersections for

long periods of time. This current interchange severely limits emergency response to the southern portion of Howell and the greater area of Marion Township by County services.

potential development and job creation these infrastructure improvements can bring to the City of Howell, Livingston County and the State of Michigan. Currently well-known automotive companies are considering this area to develop a potential. Developers have estimated that 1000 high paying skilled jobs would come to this area providing research & development in the transportation and energy fields.

This is a unique opportunity, and the benefits would be wide ranging for all aspects of the greater community including real estate, job creation and a strong local economy.

- 9. Attach documents here if needed: Attachments added to the end of this file.
- 10. The amount of state funding requested for the legislatively directed spending item. 6000000
- 11. Has the legislatively directed spending item previously received any of the following types of funding? Check all that apply.["Local"]
- 12. Please select one of the following groups that describes the entity requesting the legislatively directed spending item: Local unit government
- 13. For a non-profit organization, has the organization been operating within Michigan for the preceding 36 months? Not applicable
- 14. For a non-profit organization, has the entity had a physical office within Michigan for the preceding 12 months? Not applicable
- 15. For a non-profit organization, does the organization have a board of directors? Not applicable
- 16. For a non-profit organization, list all the active members on the organization's board of directors and any other officers. If this question is not applicable, please type 'n/a.' n/a
- 17. "I certify that neither the sponsoring representative nor the sponsoring representative's staff or immediate family has a direct or indirect pecuniary interest in the legislatively directed spending item."

Yes, this is correct

18. Anticipated start and end dates for the legislatively directed spending item:

Assuming that appropriation is received in the Fall of 2025, construction would proceed immediately and last approximately 1-year

## 19. "I hereby certify that all information provided in this request is true and accurate." Yes

Traffic Impact Analysis for D-19 and the Proposed National Street Extension

FOR

### City of Howell, Michigan

Revised June 2009

**Prepared by:** 



HUBBELL, ROTH & CLARK, INC. Consulting Engineers 555 Hulet Drive • P.O. Box 824 Bloomfield Hills, MI 48303-0824

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#### **APPENDICES**

| A. 2005 Intersection Turning Volum |
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- B. Level of Service Capacity Analysis without National Street
- C. 2015 and 2030 Traffic Volume Detail with National Street
- D. Level of Service Capacity Analysis with National Street
- E. Roundabout Rodel Files (2030 Volumes)
- F. SEMCOG Letter



The City of Howell proposes to extend National Street, south of Grand River Avenue (BL96), to the intersection of D-19/I-96 WB ramps. This new alignment, called the National Street Extension, is intended to provide access to proposed developments along its route and also to reduce future traffic on Grand River Avenue and D-19/Pinckney/Michigan Corridor by providing an alternative route to traveling through Historic Downtown Howell.

HRC prepared a traffic model of the study area using Synchro software to evaluate the existing and future roadway capacity of the roadway network in the study area. Specifically, the traffic impact study undertook the following tasks:

- 1. Explain the existing traffic volumes and the methodology used to calculate traffic projected to use the National Street Extension
- Perform Synchro analyses for existing, 2015 and 2030 conditions with and without the National Street Extension at four signalized intersections: Grand River Avenue/National Street; Grand River Avenue/Michigan Avenue(M-155); Pickney(Michigan)/Marion(Mason); and D-19/I-96 WB ramps.
- 3. Evaluate locations for connecting National Street to D-19.
- 4. Perform signal warrant analyses for up to two locations, if required
- 5. Evaluate signal alternatives
- Perform roundabout analysis for the D-19/I-96 ramps intersection for future years 2015 and 2030 using RODEL software
- 7. Provide report documenting the findings of the study

#### **Prior Reviews / Approvals**

HRC and the City have submitted several critical aspects of this study to MDOT for review and approval prior to the preparation of this final document. These submittals have included the following:

- 1. Growth Rates: HRC has received and utilized approved rates provided by MDOT.
- 2. Impact from Latson Road interchange: MDOT has provided a one-time adjustment to traffic volumes to account for the opening of the Latson Road interchange before 2015. This adjustment is used in this study.



- 3. Trip Generation / Site Development: HRC has submitted the proposed traffic volumes expected as part of the development along National Street, based on zoning and acreage. These projections have been approved by MDOT.
- 4. Roundabout Geometric Design: While this study focuses on the operational aspects of the project area, it also includes a proposed roundabout at the intersection of D-19/National Street/I-96 ramps. The geometric details of this roundabout have been reviewed by MDOT's Geometric Design Unit and have received a favorable response.
- 5. HRC submitted a ramp diverge analysis to MDOT. Their initial review did not indicate any concerns.
- 6. HRC directed by MDOT to add fourth lane to the I-96 WB Ramp approach at the intersection with D-19 under the signalized alternative.

#### Results

HRC's analyses indicate that the four signalized intersections will operate with an overall LOS D or better for all the scenarios. A caveat to this conclusion is that geometric and operational changes are necessary in the future 2015 and 2030 scenarios in order to achieve an acceptable level of service. For example, in the future 2030 scenario both D-19/I-96 WB ramps and D-19/Marion intersections are LOS F without geometric improvements in the AM and PM peak hours, and Grand River Avenue/National Street intersection is a LOS E in the AM peak hour and LOS F in the PM peak hour without geometric improvements.

#### Recommendations

HRC is recommending improvements to the four signalized intersections as well as two other intersections in the study area for the Future 2015 and 2030 scenarios. To achieve the level of service shown in Section 8, HRC made the following changes to the intersections:

- <u>D-19/I-96 WB Ramps</u> This intersection will significantly change with the growth in background traffic, the National Street Extension and the projected development along the extension in the future. HRC recommends a multi-lane roundabout instead of geometric improvements to the signalized intersection. The roundabout was found to operate at a Level of Service B, while a signalized intersection was shown to queue beyond the length of the exit ramp and onto mainline I-96. The final location for connecting National Street to D-19 is detailed in Section 2.
- <u>Pinckney (Michigan)/Marion(Mason)</u> A 90 second cycle length is recommended to achieve a desirable level of service. Dedicated left turn phases are recommended for northbound Pinckney

and eastbound Marion/westbound Mason, with modernization to accommodate the addition of left turn phasing. An overlap phase is also recommended for the eastbound right turning vehicles. At some point before full build out of development on National Street an eastbound exclusive right turn lane and extended right and left turn lane storage lengths will be necessary, but should be verified by a development study prior to installation.

- <u>Grand River Avenue/Michigan Avenue</u> The 90 second cycle length was not changed. However, HRC recommends that the splits and left turn phasing be modified to accommodate future traffic.
- <u>Michigan Avenue/Sibley Street</u> This intersection is approximately 280 feet south of Grand River Avenue. It is recommended that the signal timing plan here be coordinated with the plan running at Grand River Avenue/Michigan Avenue.
- <u>Grand River Avenue/National Street</u> This intersection will significantly change with the extension of National Street to D-19 in the future. HRC recommends an exclusive right turn lane for the northbound approach of National Street. Because of the high volume of left-turning traffic during the PM peak hour, HRC recommends dedicated left turn phases for westbound Grand River Avenue and southbound National Street. HRC also recommends adding an overlap phase for the northbound right turn lane. A 90 second cycle length was used for the 2015 and 2030 analyses during the AM and PM peak periods.
- <u>Lucy Road, between CSX Railroad Crossing and Grand River Avenue</u> Between the time of the opening of the National Street Extension and the full build out of the property along the National Street Extension, it is recommended to pave this section of Lucy Road to relieve the stress of the increased demand on the intersection of Grand River Avenue/National Street. Westbound left turns and northbound right turns could be split more evenly between the two intersections if this section of Lucy Road were paved to handle the additional traffic.

#### **Outstanding Issues**

Based on the submittal of this traffic impact study, the following issues are yet to be resolved:

- Receiving formal MDOT geometric approval for the roundabout and permitting through the TSC.
- The City of Howell will address the following issues under a separate cover.
  - Dedication of property for future I-96 ramp modernization.
  - Relocation of the existing Park & Ride Facility.
  - Intersection of Grand River Avenue/National Street will be designed to accommodate
     WB-62 vehicles as they turn on Grand River Avenue from northbound National Street.

## Section 1 - Introduction

The City of Howell recently reconstructed D-19 (Pinckney Road) to add a center left turn lane for a length of approximately 0.5 mile. There is a signalized intersection at D-19 and the westbound off and on ramps of I-96 south of the project limits. The City wanted to evaluate the most efficient way to accommodate and connect a future by-pass road called the National Street Extension. Several options were investigated and after reviewing the critical elements a four leg multi-lane roundabout at the intersection of D-19/I-96 WB ramps, it was determined that a roundabout was the best option for connecting the National Street Extension to the existing intersection.

National Street Extension is intended to be an alternate route for traffic through historic downtown Howell to the D-19 and I-96 interchange and to provide access to developments in a previously inaccessible section of the City. The National Street Extension is being funded with municipal bonds.

The City of Howell retained Hubbell, Roth and Clark, Inc. (HRC) to conduct a traffic impact study for intersection of D-19, I-96 WB ramps and the National Street Extension. The study was prepared with the collaboration of the Michigan Department of Transportation and the Livingston County Road Commission. The study included the following items:

- 1. What are the existing and future traffic volumes in the study area?
- 2. What are the levels of service at various key intersections for existing and future conditions?
- 3. Should more of these intersections be signalized?
- 4. Is a roundabout a better option for the National Street Extension to D-19?
- 5. Should Lucy Road be connected to the National Street Extension north of CSX railroad crossing?

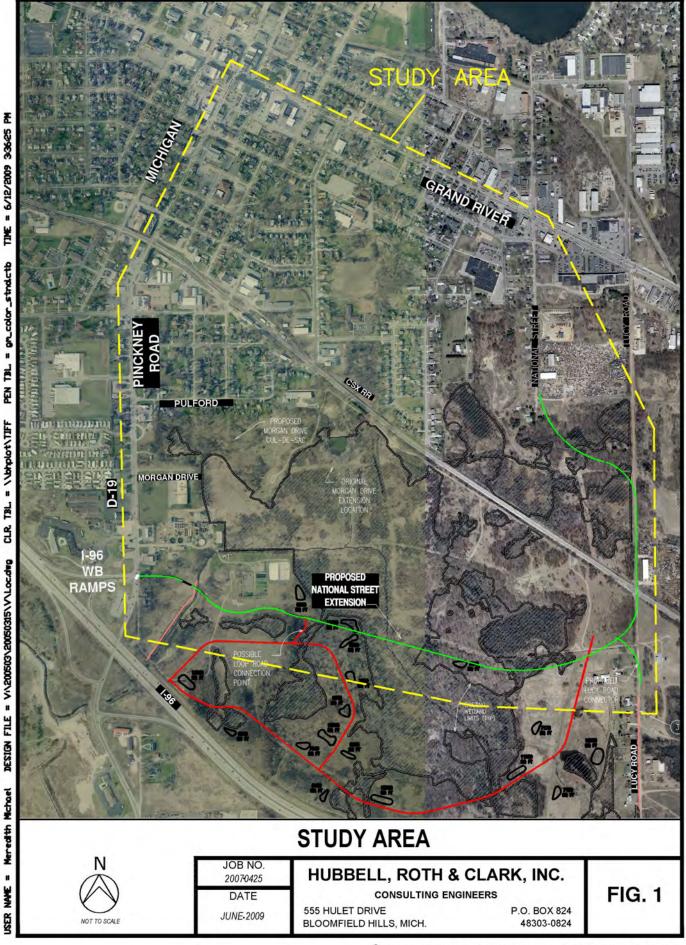
The study:

- Explains the existing traffic volumes and the methodology used to calculate traffic projected to use the National Street Extension;
- Performs Synchro analyses for existing, background 2015 and 2030 and future 2015 and 2030 conditions;
- Evaluates the performance of the I-96 WB Off ramp with and without the National Street Extension; and

• Evaluates and compares roundabout capacity analysis using Rodel software for future years 2015 and 2030 conditions.

HRC prepared a traffic model of the study area (See Figure 1) using Synchro v7 software to evaluate the existing and future capacity of the roadway network in the study area. The roundabout analysis was conducted using Rodel software. The freeway ramp analysis was conducted using Highway Capacity Software.





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# Section 2 - Alternatives Considered for National Street Extension Connection

As part of the National Street Extension, several locations were reviewed for the new intersection with D-19. The City's preferred location is at the existing intersection of D-19/I-96 WB ramps. The tie-in alternatives considered are as follows:

#### Intersection at Morgan Drive (Considered)

HRC and the City reviewed an alternative that would connect the National Street Extension with Morgan Drive as shown in Figure 2. As part of the connection, the existing unsignalized D-19/Morgan Drive intersection would be reconstructed as either a roundabout or signalized intersection. After a revised horizontal alignment was developed for this alternative, several concerns were raised.

The first concern is the increased construction cost. It was estimated that the road construction cost would increase by over \$1,000,000 due to the additional length and the need to construct the road over wetlands which involved significant deep peat excavation. This alignment would also require relocation of the City's sludge drying beds adjacent to the wastewater treatment plant. Relocating the sludge beds would cost an additional \$250,000 for a total project cost increase of \$1,250,000. In addition to the increased costs, the impact to the adjacent wetlands is far greater for this option.

The second concern is the additional right of way needed for this alignment. The National Street Extension project not only provides relief for downtown traffic on Grand River Avenue, but also development opportunities for the property owners along the roadway. The Morgan Drive alignment significantly reduces the amount of developable land. Property owners have indicated that the right of way needed for the National Street Extension would not be granted if the connection point is at Morgan Drive due to the development restrictions it causes. In addition to the property needed to extend National Street, additional right of way would be needed along existing Morgan Drive, including at the intersection with D-19. The additional right of way acquisition costs have not been estimated as part of this study.

The third concern with the Morgan Drive connection relates to traffic operations for the intersections of D-19/Morgan Drive and D-19/I-96 WB ramps. A primary goal of the National Street Extension is to

reduce traffic volume in the downtown area along Grand River Avenue by providing a bypass from Grand River Avenue to D-19 and I-96. Considering this, the proposed traffic volumes will reach the D-19/I-96 intersection even if National Street is connected at Morgan Drive. The connection of National Street to D-19 at Morgan Drive would continue to provide access for the vehicles to arrive at the D-19/I-96 WB ramps intersection. The D-19/Morgan Drive intersection was analyzed as signalized.

During the AM peak, southbound D-19 traffic at Morgan Drive backs up to the intersection at Marion/Mason. All traffic exiting the I-96 WB ramp and wishing to use National Street will be required to turn left onto D-19. As a result the ramp traffic queues onto the freeway. Also, westbound traffic on the National Street Extension at Morgan Drive queues over 1.5 miles while trying to access D-19.

| Intersection | D-19/I-96 WB Ramps | D-19/Morgan Drive |  |  |  |  |  |  |
|--------------|--------------------|-------------------|--|--|--|--|--|--|
|              | AM PEAK            |                   |  |  |  |  |  |  |
| Future 2015  | В                  | В                 |  |  |  |  |  |  |
| Future 2030  | С                  | D                 |  |  |  |  |  |  |
|              | PM PEAK            |                   |  |  |  |  |  |  |
| Future 2015  | С                  | Е                 |  |  |  |  |  |  |
| Future 2030  | D                  | F                 |  |  |  |  |  |  |

 Table 1: Intersection Level of Service for the Morgan Drive Connection Signalized Alternative

The option of connecting National Street to D-19 at Morgan Drive was also reviewed for the feasibility of installing a roundabout at D-19/Morgan Drive. Adequate right-of-way on the west side of D-19 is not available to construct a roundabout suitable to handle the projected traffic.

#### New intersection north of I-96 Ramps and South of Morgan Drive (Considered)

HRC and the City also reviewed potential intersection locations between Morgan Drive and the I-96 ramps. However, due to the City's wastewater treatment plant location, these options were limited to immediately north of I-96 or just south of Morgan Drive. The location just north of I-96 presented a significant proximity/operational problem since it would be within 200 feet of the existing signal at the I-96 ramps. This option would require the purchase of a gas station which would result in significant costs to the City. In addition, in order to construct National Street in this location, a primary Panhandle pipeline may also need relocation. HRC and the City have held several meetings about this project with Panhandle pipeline and they have expressed significant concerns regarding any relocations, which would be at the City's expense. The effort and expense of any relocation of this pipeline is well beyond the scope of this project.

The option of connecting National Street to D-19 just south of Morgan Drive and north of the treatment plant was not considered in detail. This option would require a new intersection within 400 feet of the Morgan Drive intersection and would also result in a new signalized intersection approximately 700 feet from the I-96 signal. In addition, due to the close proximity to Morgan Drive, this option was caused more operational issues when compared to the option of using Morgan Drive.

The effect of moving the National Street connection to a location on D-19 is to relocate traffic at the intersection of D-19/I-96 West ramps from the east leg to the north leg for traffic entering I-96 from National Street.

Either location described above would also result in the majority of the National Street traffic eventually getting to the existing I-96 intersection, as previously discussed in the Morgan Drive section. These options would also increase the amount of wetland impacts when compared to the I-96 intersection option.

#### Intersection at I-96 WB ramps (Preferred)

HRC and the City concluded that the existing intersection at D-19 and the westbound I-96 ramps is the preferred location to connect the National Street Extension to D-19. This preferred alternative location is evaluated in more detail throughout this report.

Due to the presence of the existing Panhandle gas storage facilities, Howell's Wastewater Treatment Plant and extensive wetlands within the National Street Extension site, the best connection to D-19 is at the existing intersection at the I-96 ramps. This direct connection results in lower costs for the construction of the National Street Extension, improved traffic capacity and minimized impacts to the wetlands and utilities.

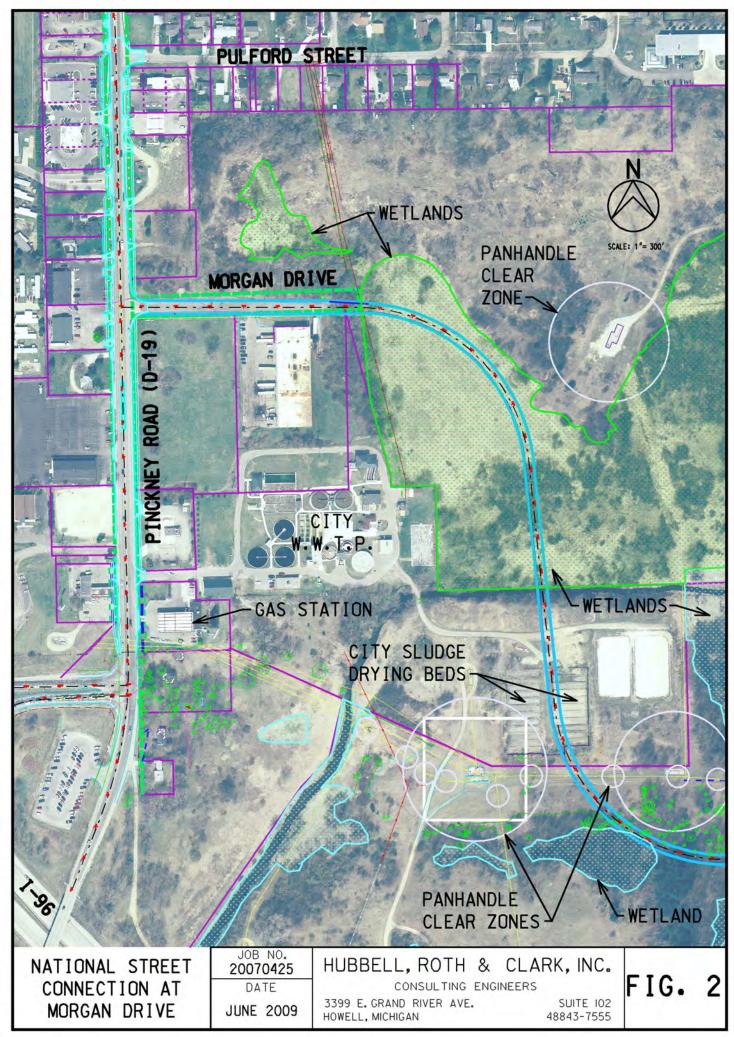
HRC and the City have coordinated this project with the property owner's where National Street is being extended. This project is intended to provide not only a bypass for the downtown traffic, but also access to property that will be developed by the owners. Providing this new development is not only important to the owners, but also to the City. The existing site conditions along National Street provide limited locations for not only the road but also for viable locations for development and parking facilities. Since the property owners will need to provide the necessary right of way, the road itself needs to provide reasonable access and development in order to make it worthwhile. After extensive conversations with the property owners, months of design and traffic modeling, geotechnical research and coordination with

Panhandle Pipeline representatives, the most desirable access is at the existing I-96 intersection when compared to the other alternatives considered.

#### Summary

The traffic impacts of connecting National Street to D-19 at the I-96 ramps are documented in detail in this study. As part of the study, the operation of a signalized intersection was evaluated as well as that of a four-legged roundabout. A roundabout will provide an exceptional level of service (LOS B) while a signalized intersection will ultimately fail with a level of service of E, even with geometric improvements. This improved operations at the D-19/I-96 WB ramps intersection was one key factor in the City's desire to construct a roundabout at this location.





USER NAME - mmeredith

## Section 3 - Existing Traffic Volumes

The study area was bounded by: D-19/Pinckney/Michigan Corridor from I-96 at the south to Grand River Avenue at the north; Grand River Avenue from Michigan Avenue in the west to Lucy Road in the east; and the National Street Extension from National Street to the intersection of D-19/I-96 WB ramps.

The City of Howell provided peak hour turning movement counts, taken in September 2005, at the majority of the key intersections within the study area. HRC supplied the peak hour turning movement counts for Grand River Avenue and Michigan Avenue which were taken in February 2005. The intersections studied were:

| 1. | D-19 & I-96 WB Ramps                                     | Signalized     |
|----|--|----------------|
| 2. | D-19/Pinckney Road & Pulford Street.                     | Non-signalized |
| 3. | Pinckney Road/Michigan Avenue & Marion Street/Mason Road | Signalized     |
| 4. | Michigan Avenue(M-155) & Livingston Street               | Non-signalized |
| 5. | Michigan Avenue(M-155) & Washington Street               | Non-signalized |
| 6. | Grand River Avenue & Michigan Avenue(M-155)              | Signalized     |
| 7. | Grand River Avenue & Court Street                        | Non-signalized |
| 8. | Grand River Avenue & Barnard Street                      | Non-signalized |
| 9. | Grand River Avenue & Fowler Street                       | Non-signalized |
| 10 | . Grand River Avenue & National Street                   | Signalized     |

For the key intersection of D-19/I-96 WB ramps, the Michigan Department of Transportation (MDOT) provided peak hour turning movement counts taken in August 2004. MDOT also supplied the current traffic signal timings for the four signalized intersections to be analyzed within the study area.

#### **Roadway Geometry**

The D-19/Pinckney/Michigan corridor is predominantly two lanes and runs north-south. The corridor has three names in the study area. D-19 is the segment from south of the I-96 WB ramps north to Pulford Street; it is a four-lane road with a speed limit of 45 mph. Pinckney Road is the segment between Pulford Street north to Marion Street and the speed limit is lowered to 35 mph. The Michigan Avenue (M-155) segment is between Marion Street and Grand River Avenue and the speed limit is only 25 mph. The number of local streets crossing Michigan Avenue (M-155) increases as it approaches Grand River Avenue.

Grand River Avenue (BL96) is a mix of a five and three lane roadway with a speed limit of 35 mph. Onstreet parking is allowed on certain segments of Grand River Avenue in downtown Howell. The roadway has been improved at the signalized intersections with Michigan Avenue (M-155) and National Street.

#### **Intersection Geometry**

The intersections of greatest importance in this study are D-19/I-96 WB ramps and Grand River Avenue/National Street. The National Street Extension will connect these two intersections and is expected to impact the intersection operations.

As shown in Photograph 1, the intersection of D-19/I-96 WB ramps has three legs and is signalized. There is a dedicated right turn lane on southbound D-19 and an intersection passing lane on northbound D-19. The off ramp and on-ramp are adjacent to each other.



Photograph 1: Southbound D-19 North of I-96 WB Ramps

As shown in Photograph 2, the intersection of Grand River Avenue/National Street is a signalized, four leg intersection. The approaches on Grand River Avenue have been improved to five lanes with a dedicated left turn lane. National Street is three-lanes with a dedicated left turn lane and a shared through and right turn lane. Immediately west of National Street, Grand River Avenue narrows to three

lanes. Approximately 1,500 feet east of National Street, the center left turn lane on Grand River Avenue ends just before a railroad bridge overpass.



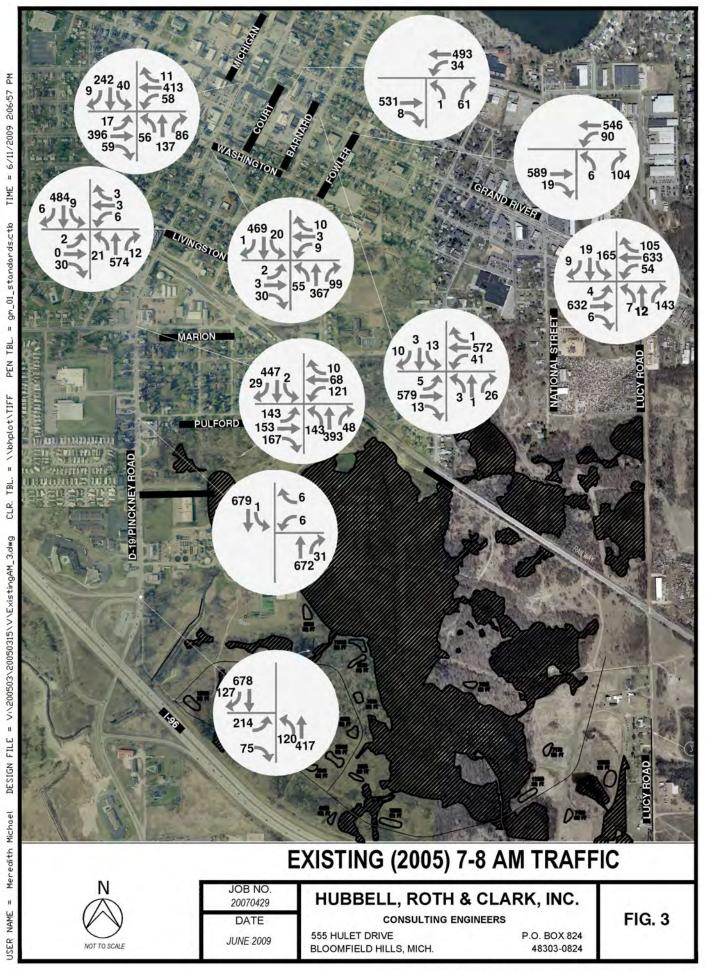
Photograph 2: Northbound National Street at Grand River Avenue

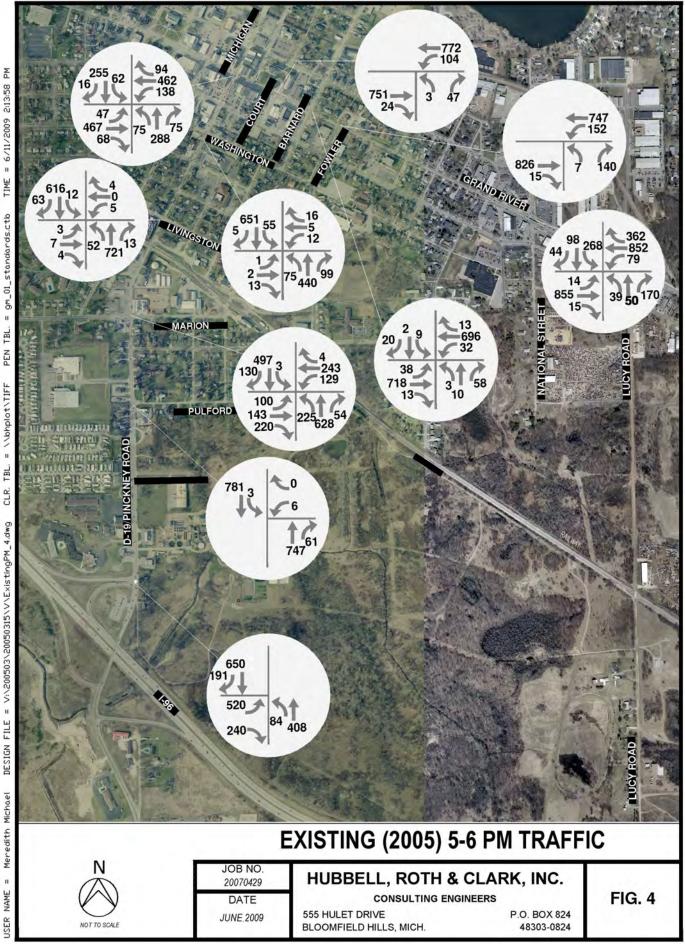
#### **Existing Traffic Volumes**

MDOT provided turning movement count data for the peak hours of 7:00 to 8:00 AM and 5:00 to 6:00 PM for the intersection of D-19/I-96 WB ramps. From the turning movement counts taken by the City of Howell, the peak hours for the intersection of Grand River Avenue/National Street were 7:15 to 8:15 AM and 4:30 to 5:30 PM. The peak hours for the remainder of the eight intersections within the study area varied by location. Given the inconsistency of peak times, HRC recommended using the same peak hours for the level of service analysis as for the intersection of D-19/I-96 WB ramps. Therefore, the peak hours for the analysis were 7:00 to 8:00 AM and 5:00 to 6:00 PM with the exception that MDOT and LCRC directed that the counts performed for the Grand River Signal Optimization project for the 4:30 to 5:30 PM period be used for level of service analysis at Grand River Avenue and National Street.

Figures 3 and 4 display the existing traffic volumes at all the study intersections for the AM peak hour and the PM peak hour respectively.







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### Section 4 - Background Traffic Growth

Background traffic is the considered the growth in traffic volumes between the time when traffic counts are taken and a future analysis year. Background traffic growth is due to development or traffic pattern changes outside of the study area, but which affect traffic within the study area. Two specific analysis years were chosen due to dates associated with the National Street project. For analysis purposes, the scenarios are:

- Existing scenario refers to September 2005 traffic volumes. (See Figures 3 and 4, Section 3)
- 2015 scenario is the projected build-out date for new development along the National Street Extension.
- 2030 scenario provides analysis for a twenty year horizon for the study area as requested by MDOT.

HRC calculated background growth for each of these scenarios and then annually until 2030: in order to project traffic to the 2015 and 2030 scenarios. It must be noted that the use of growth rates can overestimate the number of vehicles when used to project for a period greater than five years.

To determine traffic growth factors, HRC compared the turning movement counts taken by the Livingston County Road Commission (LCRC) in September 2001 with the counts taken by the City of Howell in 2005. In the table below, the PM peak hour volumes have increased an average of 6.6% for the four (4) years. This translates into an annual growth rate of 1.65%. The AM peak hour volumes grew an average of only 1.2% over the four years or an annual growth rate of 0.3%.

|                        | AM                 | Peak               | PM F                      | PM Peak            |  |
|------------------------|--------------------|--------------------|---------------------------|--------------------|--|
| Intersection           | 2001 LCRC<br>Count | 2005 City<br>Count | 2001 LCRC<br>Count        | 2005 City<br>Count |  |
| Pinckney & Pulford     | 1615               | 1567               | 1525                      | 1868               |  |
| Pinckney & Marion      | 1672               | 1914               | 1944                      | 2446               |  |
| Michigan & Washington  | 1197               | 1208               | 1519                      | 1486               |  |
| Grand River & Court    | 1291               | 1164               | 1713                      | 1781               |  |
| Grand River & Barnard  | 1415               | 1274               | 1645                      | 1762               |  |
| Grand River & Fowler   | 1259               | 1402               | 2058                      | 1993               |  |
| Grand River & National | 1832               | 1873               | 2958                      | 2909               |  |
| Totals                 | 10281              | 10402              | 13362                     | 14245              |  |
| Average Growth Rate    | 10402/102          | 281 <b>= 1.2%</b>  | 14245/13362 <b>= 6.6%</b> |                    |  |

 Table 2: Peak Hour Traffic Comparison between 2001 & 2005



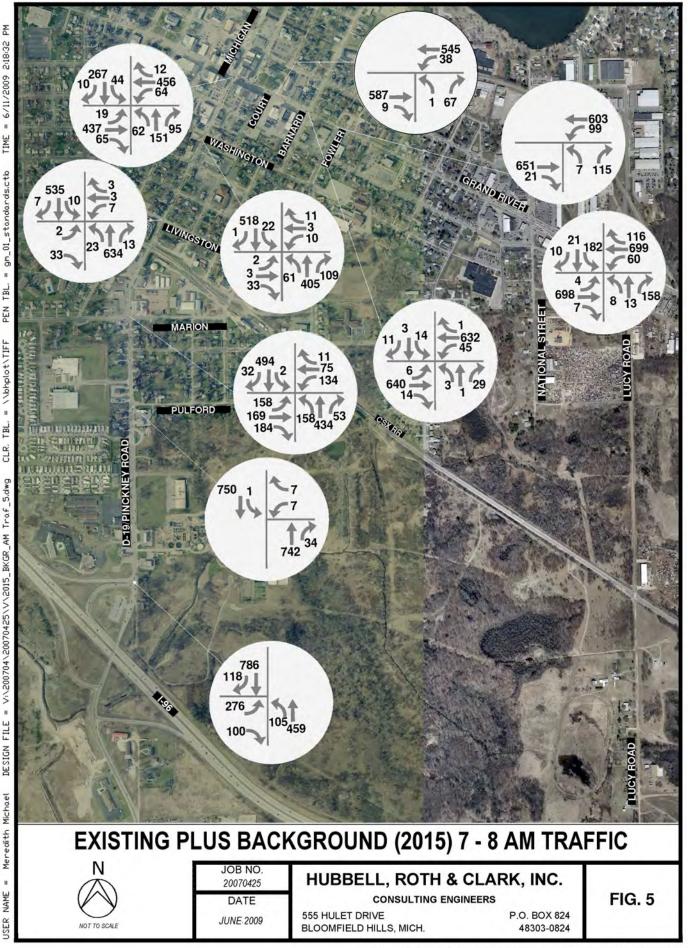
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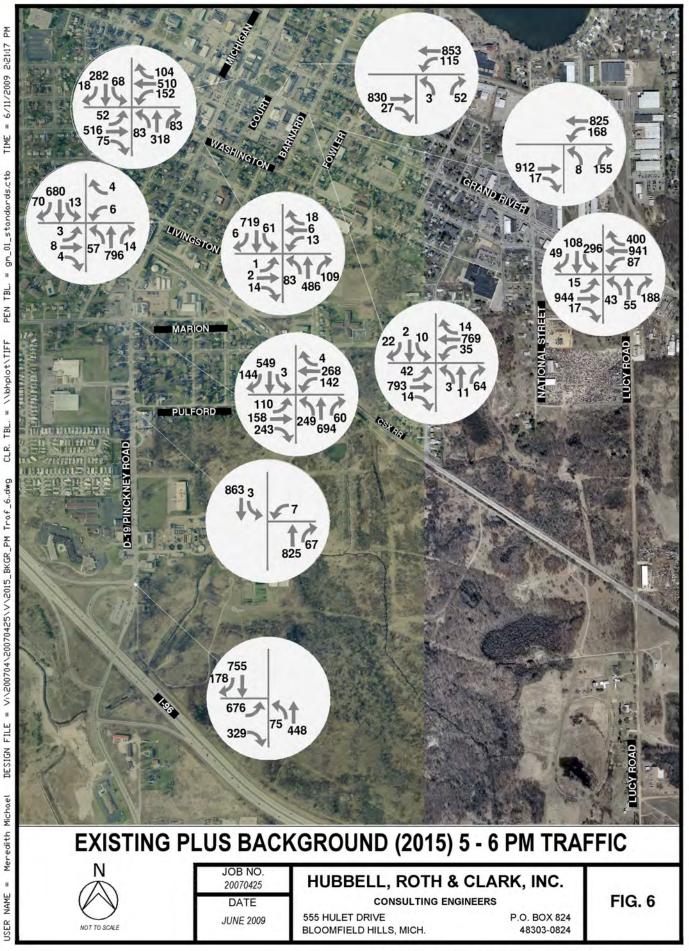
Discussions with LCRC, MDOT and consultation with the Southeast Michigan Council of Governments' (SEMCOG) Regional Transportation Model resulted in the direction that a 1 percent annual growth rate be applied to traffic within the City of Howell for both the AM and PM peak period. A 1.5 percent annual growth rate, as directed by MDOT, was used for traffic outside the City of Howell limits, which affects some turning movements at the intersection of D-19/I-96 WB ramps. In addition one time factors were applied at the intersection of D-19/I-96 WB ramps to account for changes in traffic patterns due to the opening of the I-96 interchange at Latson Road before 2015.

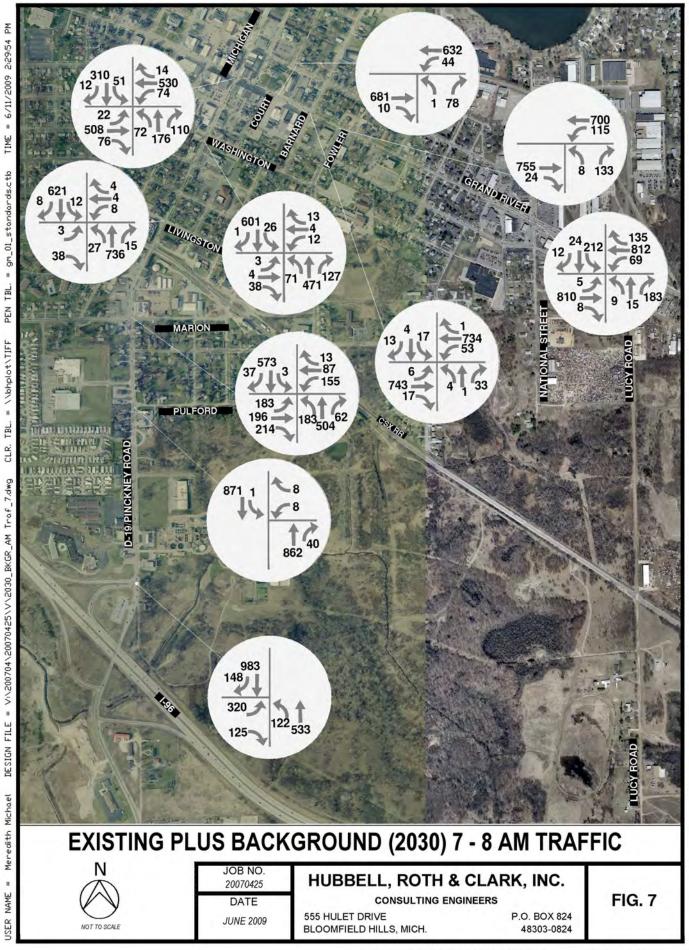
Figures 5 and 6 show the intersection volumes for the 2015 scenario for the AM and PM peak hours respectively.

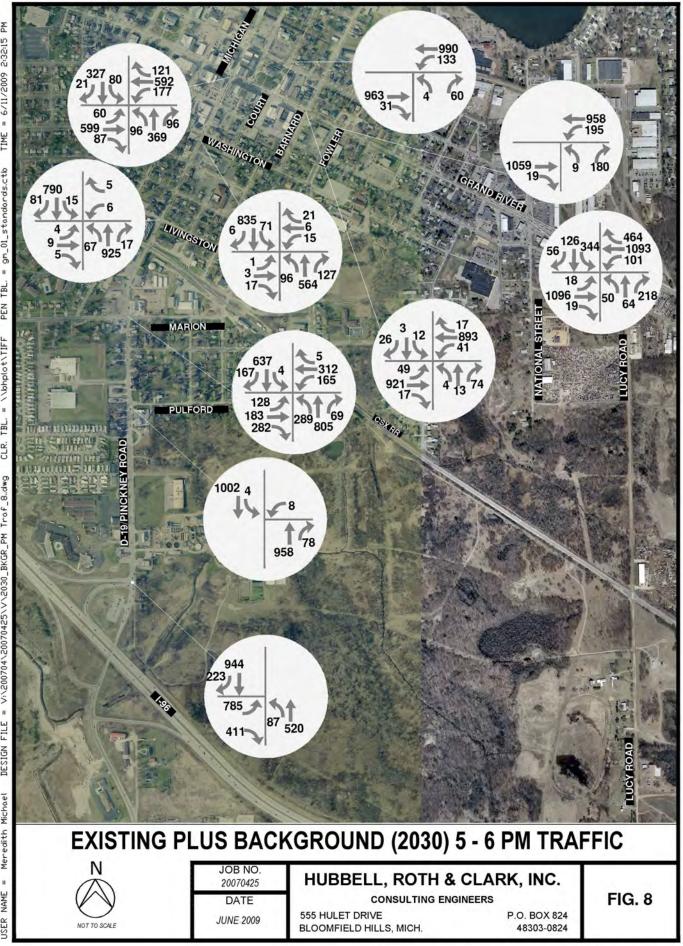
Figures 7 and 8 show the intersection volumes for the 2030 scenario for the AM and PM peak hours respectively.











## Section 5 - Level of Service Analysis – Without National Street

HRC analyzed the intersection level of service at all ten intersections for three traffic scenarios for both the AM and PM peak hours assuming that the National Street Extension has not been built.

- Existing scenario existing volumes.
- Background 2015 scenario existing traffic volumes projected through 2015.
- Background 2030 scenario existing traffic volumes projected through 2030.

#### Signalized Intersections

HRC used the current signal timing plans in the Synchro analysis (timing permits provided by MDOT with revision dates between 12/2006 and 11/2007). The D-19/I-96 WB Ramp intersection is an uncoordinated semi-actuated four phase signal and the cycle length varies based on the number of vehicles that arrive and actuate the signal. The Pinckney/Marion intersection has a 90 second cycle length with a two-phase operation. The Grand River Avenue/Michigan Avenue intersection operates a 90 second cycle length; it is a four-phase operation with a leading protected left-turn phase. The Grand River Avenue/National Street intersection also operates a 90 second cycle length with a two-phase operation.

#### Analysis Procedure for Signalized Intersections

The procedures for analysis and criteria were those outlined in <u>2000 Highway Capacity Manual</u>. This manual defines level of service for signalized intersections in terms of control delay. Delay may be measured in the field, or it may be estimated. Delay is a complex measure, and is dependent on a number of variables, including the quality of progression, the cycle length, the green ratio, and the volume to capacity ratio for the lane group or approach in question.

| Level of Service | Stopped Delay per Vehicle<br>(Seconds) | Delay Level              |
|------------------|--|--------------------------|
| А                | <10                                    | Little or no delay       |
| В                | $10 \le 20$                            | Short traffic delays     |
| С                | $20 \le 35$                            | Average traffic delays   |
| D                | $35 \leq 55$                           | Long traffic delays      |
| E                | $55 \le 80$                            | Very long traffic delays |
| F                | >80                                    | Severe congestion        |

 Table 3: Level of Service Criteria for Signalized Intersections



*Level of Service* A describes operations with very low control delay up to 10.0 sec per vehicle. This occurs when progression is extremely favorable, and most vehicles arrive during the green phase. Most vehicles do not stop at all. Short cycle lengths may also contribute to low delay.

*Level of Service B* describes operations with control delay in the range of 10.1 to 20.0 sec per vehicle. This generally occurs with good progression and/or short cycle lengths. More vehicles stop than for Level of Service A, causing higher levels of average delay.

*Level of Service C* describes operations with control delay in the range of 20.1 to 35.0 sec per vehicle. These higher delays may result from fair progression and/or longer cycle lengths. Individual cycle failures may begin to appear in this level. The number of vehicles stopping is significant at this level, although many still pass through the intersection without stopping.

*Level of Service D* describes operations with control delay in the range of 35.1 to 55.0 sec per vehicle. At level D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, or high volume to capacity ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable.

*Level of Service* E describes operations with control delay in the range of 55.1 to 80.0 sec per vehicle. This is considered to be the limit of acceptable delay. These high delay values generally indicate poor progression, long cycle lengths, and high volume to capacity ratios. Individual cycle failures are frequent occurrences.

*Level of Service* F describes operations with control delay in excess of 80.1 sec per vehicle. This is considered to be unacceptable to most drivers. This condition often occurs with over saturation, i.e., when arrival flow rates exceed the capacity of the intersection. It may also occur at high volume to capacity ratios below 1.00 with many individual cycle failures. Poor progression and long cycle lengths may also be major contributing causes to such delay levels.

#### Level of Service (LOS) Analysis for Signalized Intersections

The table below shows the LOS summaries for the four signalized intersections. The complete Synchro reports can be found in Appendix B. All intersections achieve a LOS D or better during the AM and PM



peak hours for all scenarios. Traffic signal timing was optimized to accommodate traffic growth at some study intersections. In the case of the D-19/I-96 WB ramps intersection the I-96 ramps were favored at the expense of D-19 in signal timing optimization to prevent queues from forming on the I-96 WB Off Ramp.

|          | Scenario |                    |                    |          |                    |                 |  |
|----------|----------|--------------------|--------------------|----------|--------------------|-----------------|--|
| Movement |          | AM Peak Ho         | ur                 |          | PM Peak Hour       |                 |  |
| wovement | Existing | Background<br>2015 | Background<br>2030 | Existing | Background<br>2015 | Background 2030 |  |
| EBL      | D        | D                  | D                  | Е        | D                  | F               |  |
| EBR      | С        | С                  | С                  | С        | В                  | С               |  |
| NBL      | ٨        | ٨                  | В                  | В        | С                  | C               |  |
| NBT      | А        | A                  | D                  | D        | C                  | C               |  |
| SBT      | А        | В                  | С                  | С        | D                  | Е               |  |
| SBR      | А        | А                  | А                  | С        | В                  | А               |  |
| Overall  | В        | В                  | С                  | С        | С                  | Ε               |  |

Table 4: Level of Service for the Intersection of D-19/I-96 WB Ramps

|          | Scenario     |                     |                     |              |                     |                     |  |
|----------|--------------|---------------------|---------------------|--------------|---------------------|---------------------|--|
| Movement | AM Peak Hour |                     |                     | PM Peak Hour |                     |                     |  |
| Wovement | Existing     | Background<br>2015* | Background<br>2030* | Existing     | Background<br>2015* | Background<br>2030* |  |
| EBL      | С            | С                   | С                   | С            | С                   | С                   |  |
| EBT      | С            | D                   | D                   | D            | С                   | С                   |  |
| EBR      | C            | D                   | D                   | D            | С                   | С                   |  |
| WBL      | Е            | С                   | D                   | F            | С                   | С                   |  |
| WBT      | С            | D                   | D                   | С            | D                   | Е                   |  |
| WBR      | C            | D                   |                     |              |                     | E                   |  |
| NBL      | С            | С                   | E                   | С            | D                   | F                   |  |
| NBT      | В            | B B C C             |                     |              | C                   | D                   |  |
| NBR      | D            | D                   | D                   | C            | C                   | D                   |  |
| SBL      | В            | В                   | В                   | А            | С                   | С                   |  |
| SBT      | В            | С                   | D                   | В            | D                   | Е                   |  |
| SBR      | В            | В                   | В                   | В            | С                   | В                   |  |
| Overall  | С            | С                   | D                   | С            | D                   | Ε                   |  |

Table 5: Level of Service for the Intersection of Pickney/Michigan & Marion/Mason

\* Includes additional EB Mason right turn lane, NB Pickney lagging permitted protected left turn phase, and EB Mason/WB Marion leading permitted protected left turn phase.



|          | Scenario |                    |                    |          |                    |                 |  |
|----------|----------|--------------------|--------------------|----------|--------------------|-----------------|--|
| Movement |          | AM Peak Ho         | ur                 |          | PM Peak Hour       |                 |  |
| wovement | Existing | Background<br>2015 | Background<br>2030 | Existing | Background<br>2015 | Background 2030 |  |
| EBL      | D        | D                  | D                  | D        | D                  | D               |  |
| EBT      | С        | С                  | С                  | С        | С                  | D               |  |
| EBR      | C        | U                  | C                  | C        | C                  | D               |  |
| WBL      | D        | D                  | D                  | D        | D                  | D               |  |
| WBT      | В        | В                  | С                  | В        | С                  | D               |  |
| WBR      | D        | D                  | C                  | D        | C                  | D               |  |
| NBL      | D        | D                  | D                  | Е        | D                  | E               |  |
| NBT      | В        | С                  | С                  | D        | D                  | D               |  |
| NBR      | D        | C                  | C                  | D        | D                  | D               |  |
| SBL      | D        | D                  | D                  | D        | D                  | D               |  |
| SBT      | D        | D                  | D                  | С        | С                  | С               |  |
| SBR      | D        | D                  | D                  | C        | C                  | C               |  |
| Overall  | С        | С                  | С                  | С        | D                  | D               |  |

Table 6: Level of Service for the Intersection of Grand River/Michigan

Table 7: Level of Service for the Intersection of Grand River/National Street

|          | Scenario            |                    |                     |            |                    |                  |
|----------|---------------------|--------------------|---------------------|------------|--------------------|------------------|
| Movement | AM Peak Hour PM Pea |                    |                     | PM Peak Ho | Hour               |                  |
| wovement | Existing            | Background<br>2015 | Background<br>2030* | Existing   | Background<br>2015 | Background 2030* |
| EBL      | А                   | А                  | В                   | В          | В                  | С                |
| EBT      | В                   | А                  | С                   | В          | В                  | D                |
| EBR      | D                   | A                  | C                   | D          | D                  | D                |
| WBL      | В                   | А                  | В                   | В          | С                  | С                |
| WBT      | С                   | В                  | С                   | С          | D                  | F                |
| WBR      | В                   | А                  | В                   | В          | В                  | В                |
| NBL      | В                   | С                  | С                   | С          | С                  | С                |
| NBT      | С                   | С                  | D                   | С          | С                  | D                |
| NBR      | C                   | C                  | D                   | C          | C                  | D                |
| SBL      | С                   | D                  | D                   | D          | D                  | F                |
| SBT      | В                   | С                  | С                   | С          | С                  | В                |
| SBR      |                     | C                  | C                   | C          | C                  | Б                |
| Overall  | В                   | В                  | С                   | С          | С                  | Ε                |

\* Includes SB National Street and WB Grand River Avenue permitted protected left turn phases.

#### Analysis Procedure for Unsignalized Intersections

The procedures for analysis and criteria for unsignalized intersections were also outlined in <u>2000</u> <u>Highway Capacity Manual</u>. At an un-signalized intersection with stop control on the minor approach, LOS F occurs when there are not enough gaps of suitable size to allow a minor-street demand to safely cross through traffic on the major street. This is typically evident from extremely long control delays experienced by minor-street traffic and by queuing on the minor approaches. LOS F may also appear in



the form of drivers on the minor street selecting smaller than usual gaps. In such cases, safety may be a problem, and some disruption to the major traffic stream may result. Note that LOS F may not always result in long queues but in adjustments to normal gap acceptance behavior.

At Two Way Stop Controlled intersections, the critical movement, often the minor-street left turn, may control the overall performance of the intersection. The lower threshold for LOS F is set at 50 seconds of delay per vehicle. In some cases, the delay equations will predict delays greater than 50 seconds for minor-street movements under very low-volume conditions on the minor street (less than 25 veh/h). A LOS F threshold is reached with a movement capacity of approximately 85 veh/h or less.

| Level of Service | Stopped Delay Per Vehicle (Seconds) |
|------------------|-------------------------------------|
| А                | <10                                 |
| В                | 10 ≤ 15                             |
| С                | $15 \le 25$                         |
| D                | $25 \le 35$                         |
| Е                | $35 \le 50$                         |
| F                | >50                                 |

 Table 8: Level of Service Criteria for Un-signalized Intersections

#### Level of Service (LOS) Analysis for Unsignalized Intersections

HRC performed level of service analysis using Synchro software at the six unsignalized intersections in the study area for the four scenarios. The complete Synchro reports can be found in Appendix B. The Synchro results show that in most cases, the major street turning movements are operating at a LOS A or B, but the stop controlled minor streets are experiencing a LOS F.

#### Traffic Signal Warrant Analysis for Unsignalized Intersections

Warrant analyses for unsignalized intersections are conducted to determine whether they qualify for signalization. The signal warrants require minimum traffic thresholds in order to warrant installing a traffic signal. There are six unsignalized intersections in the study area. Based on the existing peak hour volumes, the minor streets would not qualify for a traffic signal as their traffic volumes are too low. Therefore, warrant analyses at the unsignalized intersections were not pursued further.



## Section 6 - Trip Generation – With National Street

One of the most critical elements of a traffic impact study is estimating the amount of traffic to be generated by proposed developments. This is usually done by using trip generation rates or equations. Trip generation rates or equations provide an estimate of all trips generated by a site.

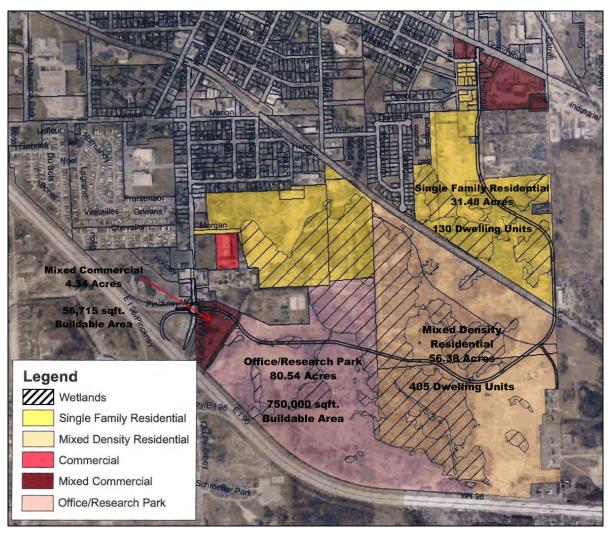
Rates are commonly expressed in trips per unit of development. For example, trips per dwelling unit are commonly used for residential developments, while trips per 1,000 square feet of gross floor area are used for offices and retail. Equations provide a direct estimate of trips based upon development units being multiplied in a mathematical relationship.

Trips are defined as a single or one directional movement with either the origin or destination of the trip inside the study site. Thus, a car entering and leaving a site would be recorded as generating two trips. Trip generation estimates are often the most critical factors in assessing impacts and needs of a proposed development.

#### **Target Area**

In accordance with the February 14, 2007 meeting of the City of Howell, MDOT and LCRC, the trip generation report was revised. It was decided by MDOT and the City of Howell that the current City Master Plan should be used to determine the anticipated trips generated by development along the National Street Extension. The basis for the land uses and acreage figures was provided by the Amended Loop Road (National Street Extension) Target Area Plan completed in August 2006 as an addendum to the City of Howell Master Plan. Several alternatives were discussed in the plan and one was selected as the Preferred Land Use Alternative. The National Street target area includes a large amount of wetlands that make the land unsuitable for development. Figure 9 shows the target area overlaid with the preferred land-uses and the amount of buildable acreage for each land use. A summary of the buildable acreage is also shown in Table 9.







Source: City of Howell Master Plan, Amended Loop Road (National Street Extension) Target Area Plan, August 2006

The trip generation methodology assumed certain maximum lot coverage by land use;

- a maximum lot coverage of 30% was used for the mixed commercial land use
- a maximum lot coverage of 80% was used for the single family residential land use
- a maximum lot coverage of 80% was used for the mixed density residential land use
- for the office/research park land use, HRC consulted with the City Planner and city's planning consultant to determine an appropriate building size for the site, location and economic conditions. It was concluded that this site could support a maximum buildout of the Office/Research Park land use of approximately 750,000 square feet. As a comparison, ITE's Trip Generation Manual provides information on sizes of office developments studied. Under General Office Building the average square footage is 220,000 SF, under corporate headquarters Building the average square footage is 275,000 SF, under the Single Tenant Office Building the

average square footage is 164,000 SF and under the Medical-Dental Office Building the average square footage is 35,000 SF. Based on ITE studies, an office/research park of even 750,000 SF is an exceptionally large development.

| Land Use   | Buildable | Land Area   | Buildings<br>GFA / DU <sup>1</sup> |
|--|-----------|-------------|------------------------------------|
|  | Acres     | Square Feet |                                    |
| Mixed Commercial                                     | 4.34      | 189,050     | 56,715 GFA                         |
| Single Family Residential<br>(min lot size 8,400 SF) | 31.48     | 1,371,312   | 130 DU                             |
| Mixed Density Residential<br>(min lot size 4,840 SF) | 56.38     | 2,455,913   | 405 DU                             |
| Office/Research Park                                 | 80.54     | 3,508,322   | 750,000 GFA                        |

Table 9: Buildable Land and Maximum Build-Out

#### **Trip Generation Rates**

There are several sources for trip generation rates and equations, which are based on data collected from locations in the United States and Canada. These are compilations of data that have been gathered over many years for various land uses. National data sources are starting points in estimating the amount of traffic that may be generated by a specific building or land use. Whenever possible, the National rates should be adjusted to reflect local or forecasted conditions. These National sources are not intended to be used without question, deviation or sound judgment. They often reflect what are supposed to be the average or typical conditions. Data collected from local sites may be more representative than National averages of other developments within the area.

The most widely used source of National Trip Generation data is the <u>Trip Generation Manual</u>, published by the Institute of Transportation Engineers. The information in this report is almost solely derived from suburban and urban sites. Data included in trip generation was obtained from actual driveway counts of vehicular traffic entering and exiting the site. The seventh edition contains more than 2,000 data sets from individual trip generation studies. The report also includes discussions on the application and use of trip generation rates and equations; descriptions of the characteristics of each land use; maximum/minimum average rates for weekdays, weekends and peak hours of the generator and adjacent street traffic; and additional statistical data regarding data variability.

 $<sup>^{1}</sup>$  GFA = Gross Floor Area DU = Dwelling Unit

Based on the land uses in the Preferred Land Use Alternative, appropriate land use codes from the ITE <u>Trip Generation Manual</u> were selected. The following table provides the daily as well as the AM and PM peak hour trip volumes. Where the coefficient of determination factor was  $\geq$  .75, the fitted curve equation was used to generate the trips.

| Land Use (ITE Code)           | Intensity        | Daily |       | AM Peak |     | PM Peak |      |
|-------------------------------|------------------|-------|-------|---------|-----|---------|------|
|                               |                  | In    | Out   | In      | Out | In      | Out  |
| Mixed Commercial              | 56.715<br>SF GFA | 2,349 | 2,349 | 36      | 23  | 207     | 224  |
| Shopping Center (820)         |                  |       |       |         |     |         |      |
| Office/Research Park          | 750<br>SF GFA    | 4,129 | 4,129 | 997     | 95  | 156     | 763  |
| General Office Building (710) |                  |       |       |         |     |         |      |
| Single Family Residential     | 130<br>DU        | 662   | 662   | 32      | 78  | 86      | 50   |
| Single Family Detached (210)  |                  |       |       |         |     |         |      |
| Mixed Density Residential     | 405              | 1,054 | 1,054 | 27      | 131 | 127     | 62   |
| Res. Condo/Townhouse (230)    | DU               |       |       |         |     |         |      |
| Total Trips                   |                  | 8,194 | 8,194 | 1092    | 327 | 576     | 1099 |

Table 10: Summary of Trip Generation Analysis by Land Use

MDOT was concerned that, "the Preferred Land Use Alternative (Figure 9) shows a shaded area of "mixed commercial" at the intersection of Grand River Avenue/National Street and a shaded area of "commercial" near Morgan Drive. These land uses were not accounted for in the trip generation calculations."

These areas were accounted for in the analysis, specifically:

- The shaded mixed commercial area at the intersection of Grand River Avenue/National Street is currently a strip commercial center and a gas station and this area is not anticipated to be redeveloped. The strip commercial development was in place when traffic counts were taken, thus the trips from this development are already included in the traffic impact study.
- The shaded commercial area at Morgan Drive is currently a commercial use that is not anticipated to be redeveloped. The commercial development was in place when traffic counts were taken, thus the trips from this development are already included in the traffic impact study.

#### Pass-By and Diverted Linked Trips

The Preferred Land Use Alternative includes mixed commercial which is affected by the pass-by trip phenomenon. HRC followed guidelines for pass-by trips provided by the second edition of the <u>Trip</u> <u>Generation Handbook</u> published by the Institute of Transportation Engineers. The effect of the Pass-by trip reduction will be seen in the future intersection volumes and not at the driveways. Table 11 provides

the percentages of pass-by trips during the PM peak for the mixed commercial. It should be noted that there were no pass-by data for trips in the AM peak hour.

| Land Liss            | Tradamater       | Daily |       | AM Peak |     | PM Peak |     |
|----------------------|------------------|-------|-------|---------|-----|---------|-----|
| Land Use             | Intensity        | In    | Out   | In      | Out | In      | Out |
| Mixed Commercial     | 56.715<br>SF GFA | 2,349 | 2,349 | 36      | 23  | 207     | 224 |
| Pass-By (ITE Avg PM) | 34%              |       |       |         |     | 70      | 76  |
| New External         |                  | 2,349 | 2,349 | 36      | 23  | 137     | 148 |

Table 11: PM Peak Hour Pass-By Trip Adjustment

In summary, the Preferred Land Use Alternative for the Loop Road target area will generate the following trips that will need to be assigned to the two key intersections, Grand River Avenue/National Street and D-19/I-96 WB ramps.

|                          | Daily |       | AM Peak |     | PM Peak |      |
|--------------------------|-------|-------|---------|-----|---------|------|
| Land Use                 | In    | Out   | In      | Out | In      | Out  |
| Total New External Trips | 8,194 | 8,194 | 1,092   | 327 | 506     | 1023 |

Table 12: Adjusted Trip Generation for the Loop Road



# Section 7 - Trip Distribution and Assignment – With National Street

Traffic expected to be generated by a project must be distributed and assigned to the roadway system so that the impacts of the proposed project on roadway links and intersections within the study area can be analyzed. After an estimate of the total traffic into and out of the site has been made, that traffic must be distributed and assigned to the roadway system. The trip distribution step produces estimates of trip origins and destinations. The assignment step produces estimates of the amount of site traffic that will use certain access routes between their origin and destination.

HRC evaluated the existing traffic patterns in Howell to determine the future travel demand on the National Street Extension in the City of Howell. HRC suggested a methodology to the City to estimate the number of potential users of the National Street Extension. The City of Howell staff identified Sibley Street as a possible alternate route for vehicles on westbound Grand River Avenue intending to go south on Michigan Avenue and traffic on northbound Michigan Avenue intending to go eastbound on Grand River Avenue. Heavy demand and peak hour congestion attract many drivers to use less congested and easily accessible Sibley Street to avoid the Grand River Avenue/Michigan Avenue intersection. HRC proposed conducting a license plate survey to identify how many vehicles were using Sibley Street to access southbound Michigan Avenue or eastbound Grand River Avenue. HRC also counted turn movements during the peak hours at Grand River Avenue/Michigan Avenue to identify and quantify the demand for the National Street Extension.

#### **License Plate Survey**

HRC conducted a limited origin-destination study using the license plate survey technique. The license plate survey uses a simple technique of tracking a vehicle through a study area by observation at selected points.

HRC staff and the City of Howell Public Works Department employees conducted the survey on February 3, 2005 from 7:00-9:00 AM in the morning and 4:00-6:00 PM in the afternoon. The city recommended doing the survey on Court Street, Fowler Street and National Street as the key routes between Grand River Avenue and Sibley Street. Four stations were established and one observer was assigned at each station to record license plates. The field data collected was thoroughly analyzed and license plates recorded at the four stations were compared. The matching license plates were determined to be the cut-through traffic.

During the 7:00 – 9:00 AM time period, observers counted 121 vehicles making a right turn from northbound Michigan Avenue onto eastbound Sibley Street. The survey identified 47 vehicles that eventually turned eastbound onto Grand River Avenue. Observers counted 79 vehicles making a left turn from westbound Sibley Street onto southbound Michigan Avenue. Of these, the survey identified 13 vehicles that had originated on Grand River Avenue. See Figure 10.

During the 4:00 – 6:00 PM time period, observers counted 175 vehicles making a right turn from northbound Michigan Avenue onto eastbound Sibley Street. Out of these, the survey identified 70 vehicles or 40% of the total that were destined for Grand River Avenue. A total of 379 vehicles made a left turn from westbound Sibley Street onto southbound Michigan Avenue. The survey identified 130 vehicles that were destined for D-19. See Figure 11. The tables below summarize the results of the license plate survey.

| Table 13: License Plate Survey Results |  |
|--|--|
| 7:00-9:00 AM February 3, 2005          |  |
|  |  |

. . . .

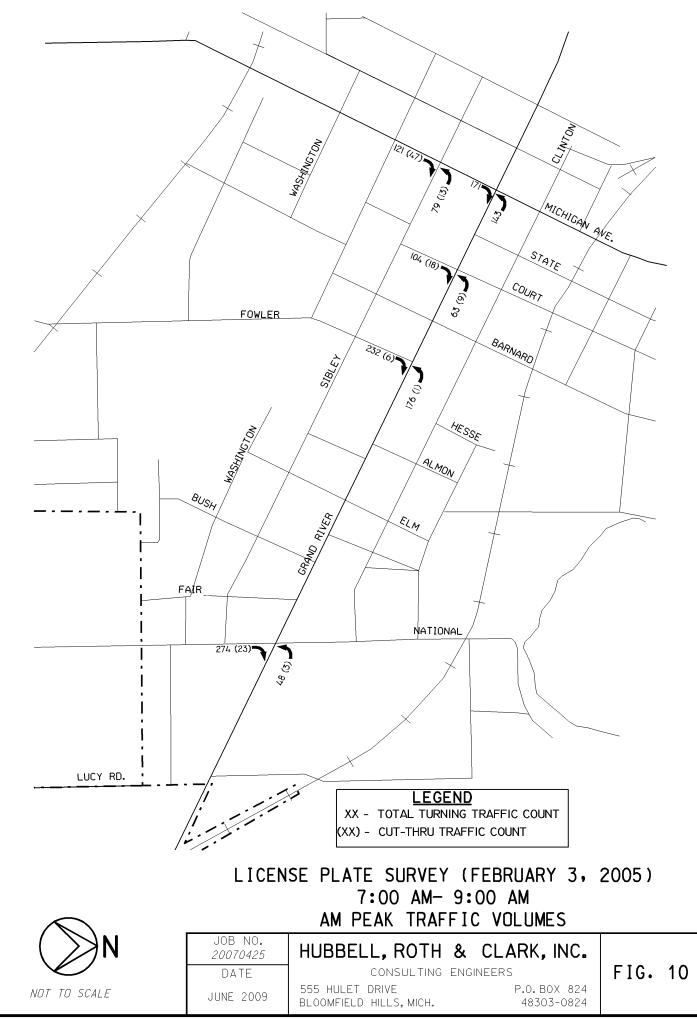
| From Michigan Avenue Via                | To Gra           | nd River Av           | Total                 | Percent |          |
|---|------------------|-----------------------|-----------------------|---------|----------|
| Sibley Street                           | Court            | Fowler                | National              | Total   | rercent  |
| 121                                     | 18               | 6                     | 23                    | 47      | 39%      |
|   |                  |                       |                       |         |          |
| To Michigan Avenue Via                  | From Gr          | and River A           | venue Via             | Total   | Democrat |
| To Michigan Avenue Via<br>Sibley Street | From Gr<br>Court | and River A<br>Fowler | venue Via<br>National | Total   | Percent  |

# Table 14: License Plate Survey Results4:00-6:00 PM February 3, 2005

| From Michigan Avenue Via | To Grand River Avenue Via |             | Total    | Percent |         |  |
|--------------------------|---------------------------|-------------|----------|---------|---------|--|
| Sibley Street            | Court                     | Fowler      | National | Total   | rercent |  |
| 175                      | 20                        | 14          | 36       | 70      | 40%     |  |
| To Michigan Avenue Via   | From Gr                   | and River A | Total    | Doncont |         |  |
| Sibley Street            | Court                     | Fowler      | National | Total   | Percent |  |
| 379                      | 84                        | 24          | 22       | 130     | 34%     |  |

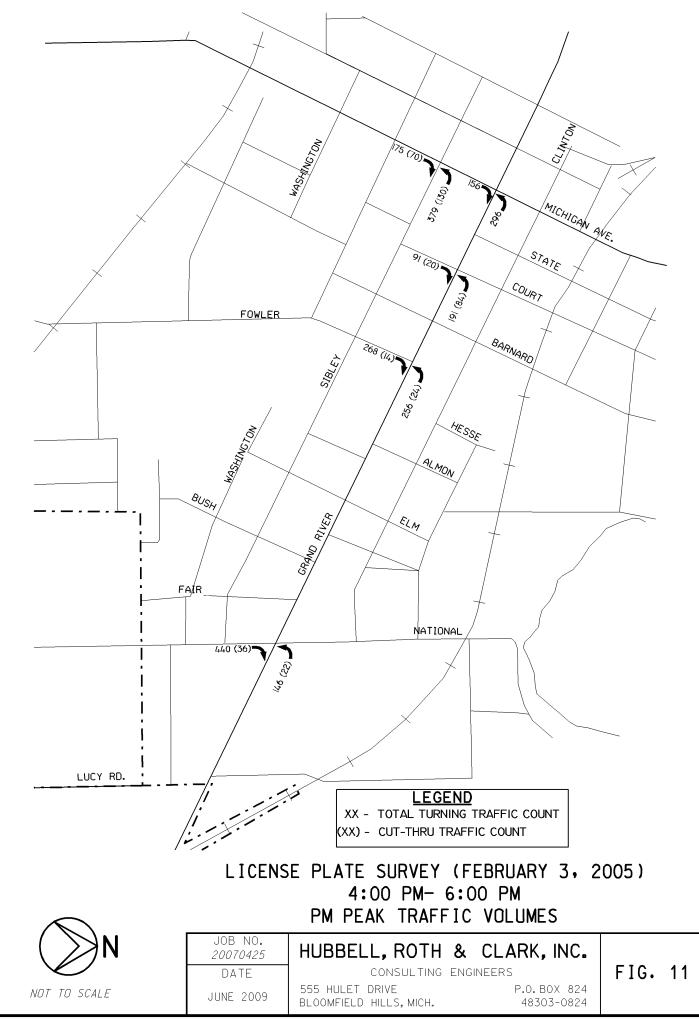
The license plate survey shows that a significant number of motorists use Sibley Street to avoid the Grand River Avenue/Michigan Avenue intersection. About 40 percent of the traffic heading for eastbound Grand River Avenue is turning onto Sibley Street to access Grand River Avenue. The percentage of traffic from Grand River Avenue cutting over to Sibley Street varies from 16% in the AM peak to 34% in the PM peak.

It is important to note that license plates were counted at only three cross streets on Grand River Avenue and there are more than three cross streets that connect Grand River Avenue to Sibley Street. Counts



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USER NAME - mmeredith



USER NAME - mmeredith

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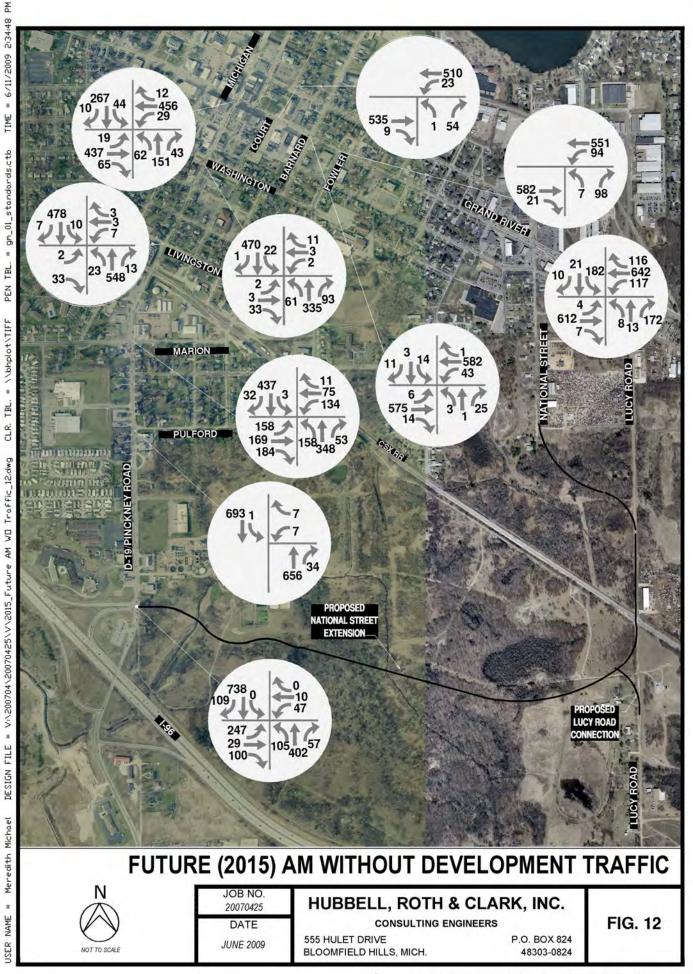
were taken at these locations based on the recommendations by the City of Howell staff. Therefore it is reasonable to estimate that if all cross streets were surveyed, 50% of northbound right-turn traffic and westbound left-turning traffic at the intersection of Michigan Avenue/Sibley Street could be using Sibley Street as an alternative to Grand River Avenue. It is also reasonable to estimate that this same traffic will use the National Street Extension, once it is available.

#### Future 2015 and 2030 Traffic Volumes

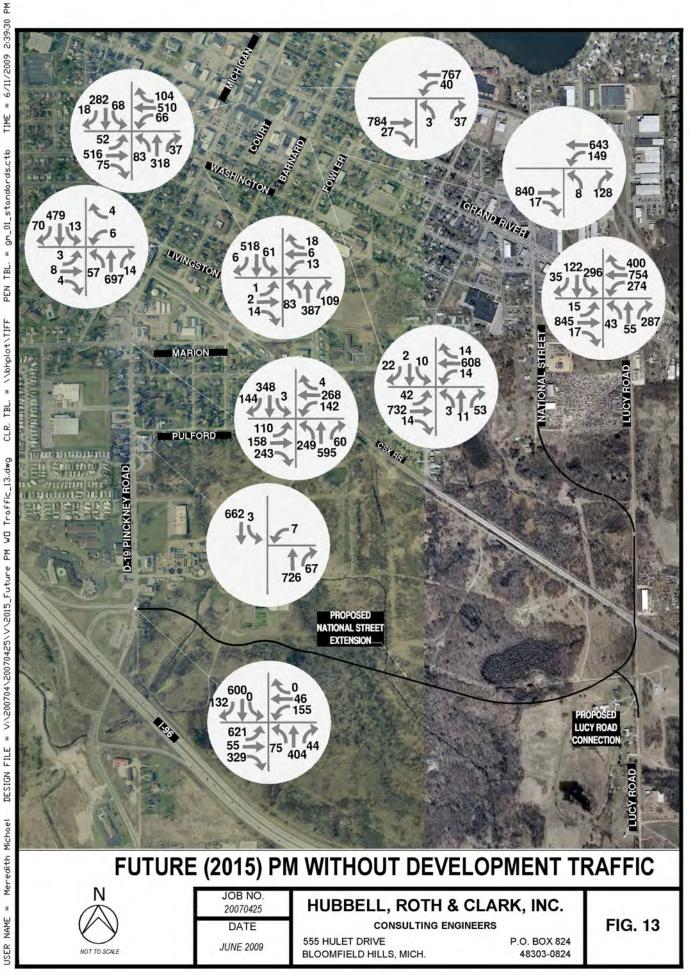
Future 2015 and 2030 traffic volumes on the network needed to be estimated with the National Street Extension. Beginning with the existing 2005 volumes at the intersections, HRC used the following methodology to calculate traffic expected to use the National Street Extension.

- As directed by MDOT, background traffic growth rate of 1% per year was used for both the AM and PM peak hour, with 1.5% per year used for traffic outside the City of Howell affecting some turning movements at the intersection of D-19/I-96 WB ramps. One time adjustments were made to specific turning movements at the D-19/I-96 WB ramps intersection in 2015 to account for the effects of the proposed I-96/Latson Road interchange.
- 50% of all trips turning left from Grand River Avenue to Michigan Avenue and all trips turning right from Michigan Avenue to Grand River Avenue will elect to utilize the National Street Extension to get to D-19. This logic is verified by the results of the travel demand forecast modeling work performed by SEMCOG for the 2030 Regional Transportation Plan. SEMCOG projected that a bypass would attract approximately 3,300 trips daily from Grand River Avenue and D-19. In urban areas, a rule of thumb is that the PM peak hour represents 8% to 12% of the average daily trips. HRC calculated that 300 trips will be diverted to the National Street Extension during the PM peak hour, which represents 9.1% of the average daily trips. The forecast modeling results can be found in Appendix F.
- New trips generated by the development along the National Street Extension were assigned to the roadway so that 70% will head west to intersection of D-19/I-96 WB ramps and 30% will go towards the intersection of Grand River Avenue/National Street. This split was based on the relative volume of traffic carried on Grand River Avenue (BL-96) versus I-96 according to the 2004 annual average 24-hour traffic volumes collected by MDOT. In 2004, the annual average on BL-96 is 18,200 and on I-96 is 45,800 (the average for the counts taken on segments on either side of the D-19 interchange).

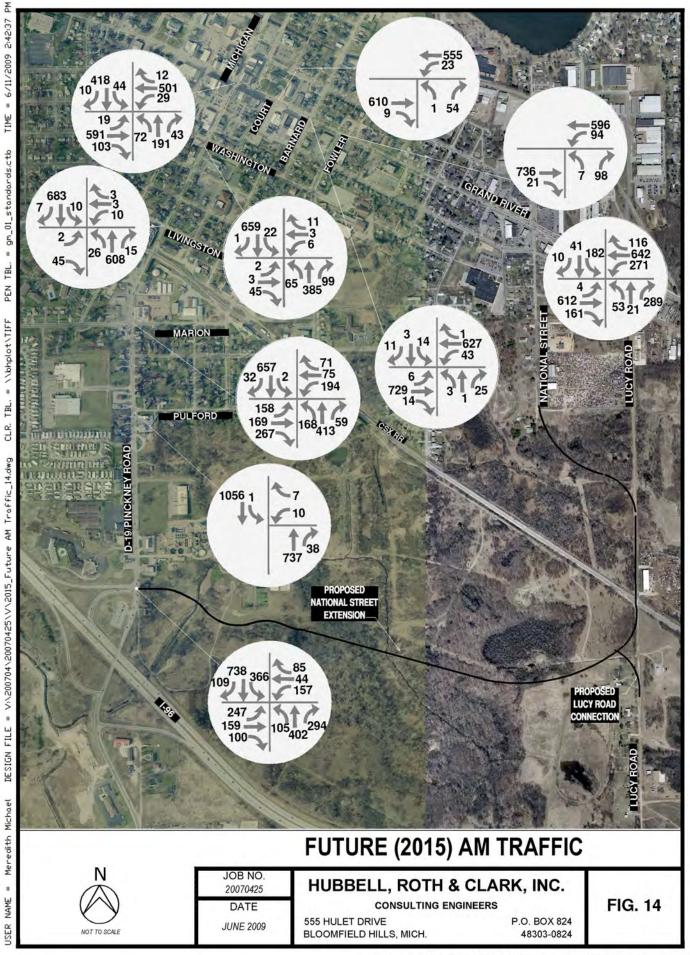
The detailed tables showing how the turning movements for the future 2015 and 2030 were derived, using the methodology above, are included in Appendix C. Figures 12 - 15 show the future 2015 and 2030 traffic volumes with a National Street Extension.



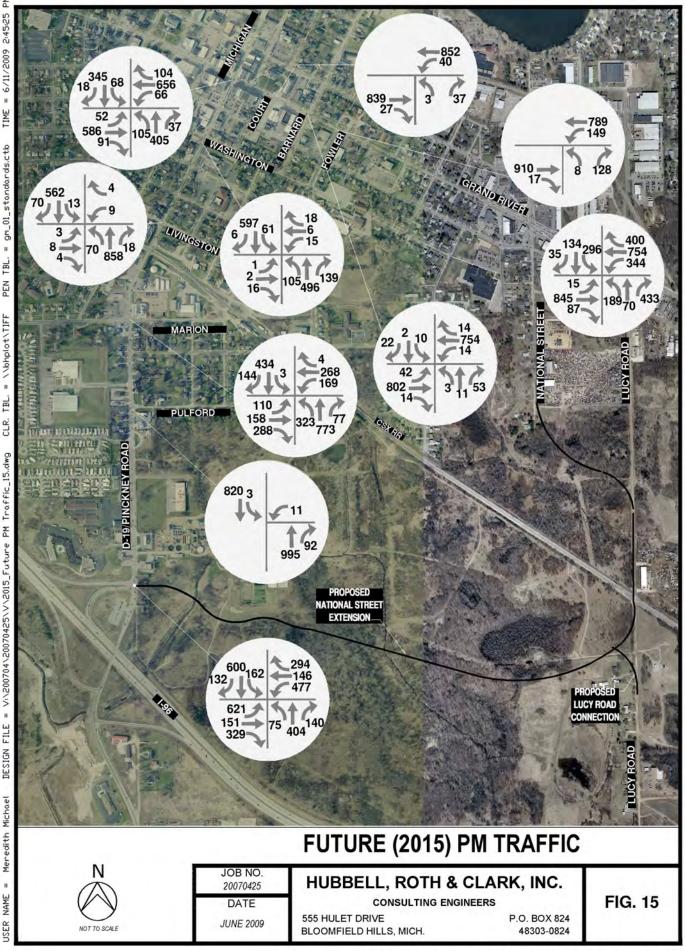
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#### Left Turn Phasing Warrants

Guidelines regarding warrants for left turn protection published on the MDOT website on December 8,

2006, entitled "Left-Turn Phasing Signal Guidelines", states:

"Left turn protection should be considered at signalized intersections when:

- the left-turn peak hour volume exceeds 90 vehicles per hour (VPH) or 50 VPH on streets with through traffic over 45 mph, or
- the product of opposing through hourly volume (VHP) and left-turn hourly volumes (VHP) exceeds 50,000, if there is one opposing lane or 100,000, if there are two opposing lanes, or
- a crash pattern is evident at the intersection which could be corrected with left-turn phasing."

This policy is more conservative than some of the commonly used techniques for warranting left-turn phasing as noted in the April 1986 ITE Journal article *A Summary Of The Use Of Warrants For The Installation Of Left-Turn Phasing At Signalized Intersections*:

- Warrants Based on Volumes
  - Cross product of left turn x opposing
     2 lane exceeds 30,000-50,000
     4 lane exceeds 50,000-100,000

#### Grand River Avenue/National Street

Existing PM peak hour left turn volumes for southbound National Street exceed 200 VPH, but the cross product with northbound through vehicles does not exceed 50,000 until you consider northbound through and right turning vehicles in the Background 2015 scenario. In the Future 2015 scenario the cross product of southbound left turns and northbound through and right turns exceeds 100,000. Northbound National Street left turning volumes do not reach the warrant thresholds for protection.

Westbound Grand River Avenue Future 2015 PM peak hour left turn volumes exceed 200 VPH, and the cross product with eastbound through vehicles exceed 100,000. Eastbound Grand River Avenue left turning volumes do not reach the warrant thresholds for protection.

#### Pinckney(Michigan)/Marion(Mason)

Existing PM peak hour left turn volumes for northbound Pinckney exceed 200 VPH, and the cross product with southbound through vehicles exceeds 100,000 in the existing condition. Southbound Michigan Avenue (M-155) left turning volumes do not reach the warrant thresholds for protection. However, at this location north-south left turns should be protected due to sight distance restrictions on the north leg.



Eastbound and westbound Marion Street (Mason) left turns do not reach the 200 VPH threshold, nor does the cross product with opposing through vehicles exceed 100,000. In the Future 2015 PM peak hour scenario the cross product of westbound left turns and eastbound through and right turns exceeds 50,000.

#### Lucy Road Connection Analysis

HRC evaluated future operation of Lucy Road when the National Street Extension is constructed and operational. Lucy Road is currently unpaved, parallel to National Street and intersects with Grand River Avenue approximately 1,130 feet east of National Street (see Figure 1). It intersects CSX railway line at grade and dead ends just north of I-96.

The National Street Extension alignment will use the existing CSX railway line crossing at Lucy Road because a second at grade crossing in this area was unacceptable to CSX. The National Street Extension will divide Lucy Road into two sections. Lucy Road south of CSX railway line will be connected to the National Street Extension via un-signalized intersection. Lucy Road north of the CSX railway line is being evaluated for the following options.

- Cul-de-sac at the southern end
- Un-signalized intersection with the National Street Extension

In order to determine the best option for Lucy Road, the traffic volume on Lucy Road and near by intersection needs to be considered. Lucy Road is an unpaved low volume road operating below capacity. The following table provides peak hour and daily traffic demand on Lucy Road.

| Time  | 5/19/2004 | 4/28/2003 | 4/29/2003 | 4/30/2003 |
|-------|-----------|-----------|-----------|-----------|
| 8:00  | 30        | 12        | 21        | 14        |
| 9:00  | 54        | 8         | 23        | 11        |
|       |           | 1         |           |           |
| 17:00 | 42        | 14        | 16        | 10        |
| 18:00 | 34        | 10        | 11        | 11        |
|       |           |           |           |           |
| Daily | 605       | 188       | 211       | 244       |

Table 15: Average Daily Traffic on Lucy RoadSource: Livingston County Road Commission

Lucy Road's future connection to the National Street Extension could possibly impact the operation of the Grand River Avenue/National Street intersection. A connection between Lucy Road and the National Street Extension may reduce the turning traffic to/from the east at Grand River



Avenue/National Street. Motorists heading westbound on Grand River Avenue turning left at National Street to go southbound may use Lucy Road when the left turn demand exceeds 300 vehicles per hour.

The following table provides estimates of future peak hour turning traffic volume at Grand River Avenue/National Street for the two key movements that may be affected by future alignment of Lucy Road. The table provides the comparison of traffic with and without the Lucy Road.

| Period      | Scenario                     | Northbound<br>Right Turn | Westbound<br>Left Turn |  |  |  |  |  |
|-------------|------------------------------|--------------------------|------------------------|--|--|--|--|--|
|             | 2015                         |                          |                        |  |  |  |  |  |
| AM Peak     | Without Lucy Road Connection | 289                      | 271                    |  |  |  |  |  |
| AW Feak     | With Lucy Road Connection    | 217                      | 203                    |  |  |  |  |  |
|             |                              |                          |                        |  |  |  |  |  |
| PM Peak     | Without Lucy Road Connection | 433                      | 344                    |  |  |  |  |  |
| r Ivi r Cak | With Lucy Road Connection    | 251                      | 235                    |  |  |  |  |  |
|             | 2030                         |                          |                        |  |  |  |  |  |
| AM Deals    | Without Lucy Road Connection | 335                      | 314                    |  |  |  |  |  |
| AM Peak     | With Lucy Road Connection    | 323                      | 239                    |  |  |  |  |  |
|             | •                            | -                        |                        |  |  |  |  |  |
| DM Dool     | Without Lucy Road Connection | 502                      | 400                    |  |  |  |  |  |
| PM Peak     | With Lucy Road Connection    | 323                      | 261                    |  |  |  |  |  |

Table 16: Turning Traffic at Grand River Avenue/National Street

A cul-de-sac will eliminate National Street Extension access to Lucy Road and as a result the intersection of Grand River Avenue/Lucy Road will not be able to serve additional traffic if bottlenecks occur at Grand River Avenue/National Street.

By connecting Lucy Road with the National Street Extension, Grand River Avenue/National Street intersection will benefit due to reduce traffic load during peak hours. HRC estimates that during peak hours when the left turn demand is in excess of 300 vph, approximately 25-35% of this traffic is expected to seek an alternative route via Lucy Road. These volumes are reflected in the Synchro files used for the level of service analysis found in Section 8. HRC therefore, recommends connecting Lucy Road to the National Street Extension through an un-signalized intersection and controlled by a stop sign for Lucy Road traffic.



# Section 8 - Level of Service Analysis – With National Street

HRC analyzed the intersection level of service at all ten intersections for future scenarios for both the AM and PM peak hours with traffic diverted to the new National Street Extension and traffic generated by developments in accordance with the Amended Loop Road Target Area Plan completed in August 2006 as an addendum to the City of Howell Master Plan.

#### **Analysis Procedure for Signalized Intersections**

As explained in Section 5, the procedures for analysis and criteria were those outlined in <u>2000 Highway</u> <u>Capacity Manual</u>. The following AM and PM peak hour scenarios were studied:

- Future 2015 with National Street Extension and future development traffic volumes without Geometric Improvements
- Future 2015 without future development traffic volumes on National Street Extension with Geometric Improvements
- Future 2015 with National Street Extension and future development traffic volumes with Geometric Improvements
- Future 2015 with National Street Extension and future development traffic volumes without Geometric Improvements
- Future 2030 with National Street Extension and future development traffic volumes with Geometric Improvements

Table 17 details the overall level of service for the signalized intersections in the study area during the AM and PM peak hours. Tables 18 through 21 provide the level of service by movement for each of the study intersections for the five scenarios during the AM and PM peak hours.



| Period             | Scenario  | D-19/I-96 WB<br>Ramps | Michigan/<br>Marion | Grand River/<br>Michigan | Grand River/<br>National |
|--------------------|---|-----------------------|---------------------|--------------------------|--------------------------|
|                    | Future 2015 without<br>Geometric Improvements                             | F                     | F                   | С                        | С                        |
| АМ                 | Future 2015 without<br>Development Traffic with<br>Geometric Improvements | В                     | С                   | С                        | С                        |
| Peak<br>Hour       | Future 2015 with Geometric<br>Improvements                                | С                     | D                   | С                        | С                        |
|                    | Future 2030 without<br>Geometric Improvements                             | F                     | F                   | D                        | Е                        |
|                    | Future 2030 with Geometric<br>Improvements                                | D                     | Е                   | D                        | С                        |
|                    | Future 2015 without<br>Geometric Improvements                             | F                     | Е                   | D                        | Е                        |
| DM                 | Future 2015 without<br>Development Traffic with<br>Geometric Improvements | С                     | С                   | С                        | С                        |
| PM<br>Peak<br>Hour | Future 2015 with Geometric Improvements                                   | С                     | D                   | D                        | С                        |
|                    | Future 2030 without<br>Geometric Improvements                             | F                     | F                   | D                        | F                        |
|                    | Future 2030 with Geometric<br>Improvements                                | D                     | Е                   | D                        | С                        |

Table 17: Overall Intersection Level of Service with National Street Extension



|               |  | AM  | Peak Hour   |  |   |
|---------------|--|---|---|--|---|
|               |  |   | Futur   | re 2030                                    |   |
| Move-<br>ment | w/o Geometric<br>Improvements <sup>1</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>2</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>2</sup> | w/o Geometric<br>Improvements <sup>1</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>2</sup> |
| EBL           | D  | С   | С   | F  | D   |
| EBT           | D  | С   | D   | Е  | D   |
| EBR           | D  | С   | С   | E  | С   |
| WBL           | Е  | D   | D   | F  | D   |
| WBT           | D  | D   | D   | D  | С   |
| WBR           | D  | -   | D   | С  | С   |
| NBL           |  | В   | С   |  | С   |
| NBT<br>NBR    | С  | А   | С   | E  | D   |
| SBL           | -  | -   | С   | -  | D   |
| SBT           | F  | В   | С   | F  | С   |
| SBR           | В  | А   | В   | В  | В   |
| Overall       | F  | В   | С   | F  | D   |
|               |  | PM  | Peak Hour   |  |   |
|               |  | Future 2015   |   | Futur                                      | re 2030   |
| Move-<br>ment | w/o Geometric<br>Improvements <sup>1</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>2</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>2</sup> | w/o Geometric<br>Improvements <sup>1</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>2</sup> |
| EBL           | F  | С   | D   | F  | D   |
| EBT           | E  | С   | С   | Г  | С   |
| EBR           | F  | С   | С   | F  | D   |
| WBL           | F  | С   | D   | F  | D   |
| WBT           | D  | С   | С   | С  | С   |
| WBR           | D  | -   | С   | D  | D   |
| NBL           |  | В   | С   |  | С   |
| NBT<br>NBR    | D  | В   | С   | D  | D   |
| SBL           | -  | -   | С   | -  | D   |
| SBT           | F  | В   | С   | F  | D   |
| SBR           | В  | В   | С   | В  | С   |
| Overall       | F  | C   | С   | F  | D   |

Table 18: Level of Service for the Intersection of D-19/I-96 WB Ramps

<sup>1</sup>Includes left turn phase for EB I-96 Ramp/WB National Street <sup>2</sup>Includes left turn phases for all approaches



|               |  | AM   | Peak Hour  |  |  |
|---------------|--|--|--|--|--|
|               |  | Future 2015  |  | Futur                                      | e 2030   |
| Move-<br>ment | w/o Geometric<br>Improvements <sup>4</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>34</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>34</sup> | w/o Geometric<br>Improvements <sup>4</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>34</sup> |
| EBL           | С  | С  | С  | С  | D  |
| EBT           | F  | D  | D  | F  | D  |
| EBR           | Г  | D  | D  | Г  | D  |
| WBL           | F  | С  | E  | F  | F  |
| WBT           | С  | D  | D  | С  | D  |
| WBR           | C  | D  | D  | C  | D  |
| NBL           | F  | С  | E  | F  | F  |
| NBT           | С  | В  | В  | С  | В  |
| NBR           |  |  |  |  |  |
| SBL           | В  | С  | В  | В  | В  |
| SBT           | F  | С  | D  | F  | F  |
| SBR           | А  | С  | A  | В  | В  |
| Overall       | F  | С  | D  | F  | Ε  |
|               |  | PM   | Peak Hour  |  |  |
|               |  | Future 2015  |  | Futur                                      | e 2030   |
| Move-<br>ment | w/o Geometric<br>Improvements <sup>4</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>34</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>34</sup> | w/o Geometric<br>Improvements <sup>4</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>34</sup> |
| EBL           | С  | С  | С  | С  | С  |
| EBT           | F  | С  | С  | F  | D  |
| EBR           | Г  | С  | С  | Г  | С  |
| WBL           | D  | С  | С  | E  | С  |
| WBT           | С  | D  | D  | D  | F  |
| WBR           | C  | D  | D  | D  | 1  |
| NBL           | E  | С  | D  | F  | E  |
| NBT           | Е  | С  | D  | F  | Е  |
| NBR           |  |  |  |  |  |
| SBL           | С  | С  | С  | С  | С  |
| SBT           | E  | С  | D  | D  | E  |
| SBR           | С  | D  | С  | С  | С  |
| Overall       | Ε  | С  | D  | F  | Ε  |

Table 19: Level of Service for the Intersection of Pickney/Michigan and Marion/Mason

<sup>3</sup>Includes additional EB Mason right turn lane and extended right turn and left turn lane storage lengths <sup>4</sup>Includes NB Pickney and EB Mason/WB Marion lead permitted left turn phases and overlap phase for EB right turns



|               | AM Peak Hour                  |  |  |                               |  |  |  |
|---------------|-------------------------------|--|--|-------------------------------|--|--|--|
|               |                               | Future 2015  |  | Futu                          | re 2030  |  |  |
| Move-<br>ment | w/o Geometric<br>Improvements | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes | w/ Geometric<br>Improvements<br>& Development<br>Volumes | w/o Geometric<br>Improvements | w/ Geometric<br>Improvements<br>& Development<br>Volumes |  |  |
| EBL           | D                             | D  | D  | D                             | D  |  |  |
| EBT<br>EBR    | С                             | С  | С  | D                             | D  |  |  |
| WBL           | D                             | D  | D  | D                             | D  |  |  |
| WBT<br>WBR    | С                             | В  | С  | D                             | D  |  |  |
| NBL           | D                             | D  | D  | D                             | E  |  |  |
| NBT<br>NBR    | В                             | С  | С  | С                             | С  |  |  |
| SBL           | D                             | D  | D  | D                             | D  |  |  |
| SBT<br>SBR    | D                             | D  | D  | D                             | D  |  |  |
| Overall       | С                             | С  | С  | D                             | D  |  |  |
|               |                               | PMI  | Peak Hour  |                               |  |  |  |
|               |                               | Future 2015  |  | Future 2030                   |  |  |  |
| Move-<br>ment | w/o Geometric<br>Improvements | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes | w/ Geometric<br>Improvements<br>& Development<br>Volumes | w/o Geometric<br>Improvements | w/ Geometric<br>Improvements<br>& Development<br>Volumes |  |  |
| EBL           | D                             | D  | D  | D                             | D  |  |  |
| EBT<br>EBR    | С                             | С  | С  | D                             | D  |  |  |
| WBL           | D                             | D  | D  | D                             | D  |  |  |
| WBT<br>WBR    | D                             | С  | D  | D                             | D  |  |  |
| NBL           | D                             | D  | D  | Е                             | Е  |  |  |
| NBT<br>NBR    | D                             | С  | С  | Е                             | D  |  |  |
| SBL           | D                             | D  | D  | D                             | D  |  |  |
| SBT<br>SBR    | D                             | С  | С  | D                             | D  |  |  |
| Overall       | D                             | С  | D  | D                             | D  |  |  |





|                |  | AM   | Peak Hour  |  |   |
|----------------|--|--|--|--|---|
|                |  | Future 2015  |  | Futur                                      | re 2030   |
| Move-<br>ment  | w/o Geometric<br>Improvements <sup>5</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>56</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>56</sup> | w/o Geometric<br>Improvements <sup>5</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>567</sup> |
| EBL            | С  | В  | С  | С  | В   |
| EBT<br>EBR     | D  | С  | С  | Е  | С   |
| WBL            | С  | В  | С  | Е  | С   |
| WBT            | С  | С  | С  | D  | В   |
| WBR            | В  | В  | В  | В  | В   |
| NBL            | С  | С  | С  | С  | D   |
| NBT<br>NBR     | D  | C<br>D   | C<br>D   | D  | D<br>C  |
| SBL            | D  | С  | С  | Е  | D   |
| SBT<br>SBR     | В  | В  | В  | В  | C<br>C  |
| Overall        | С  | С  | С  | Ε  | С   |
|                |  | PM   | Peak Hour  |  |   |
|                |  | Future 2015  |  | Futur                                      | re 2030   |
| Move-<br>ment  | w/o Geometric<br>Improvements <sup>5</sup> | w/ Geometric<br>Improvements &<br>w/o Development<br>Volumes <sup>56</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>56</sup> | w/o Geometric<br>Improvements <sup>5</sup> | w/ Geometric<br>Improvements<br>& Development<br>Volumes <sup>567</sup> |
| EBL            | D  | С  | С  | С  | С   |
| EBT<br>EBR     | F  | С  | D  | D  | D   |
| WBL            | Е  | С  | D  | F  | D   |
| WBT            | D  | В  | С  | D  | В   |
| WBR            | В  | А  | А  | В  | В   |
| NBL            | D  | D  | D  | D  | E   |
| NBT            | F  | D  | С  | F  | С   |
| NBR            |  | С  | C  |  | С   |
| SBL            | E  | D  | С  | F  | D   |
| SBT            | В  | С  | D  | С  | C   |
| SBR<br>Overall | Е  | С  | С  | F  | B<br>C  |

Table 21: Level of Service for the Intersection of Grand River/National Street

<sup>5</sup>Includes permitted left turn phases for SB National Street and WB Grand River Avenue and overlap phase for NB right turns

<sup>6</sup>Includes additional NB National Street right turn lane

<sup>7</sup>Includes WB Grand River Avenue right turn lane converted to shared through/right turn lane and additional SB National Street right turn lane



A previous MDOT review questioned the B### nodes that appeared in the SimTraffic reports. From the *Traffic Signal Software- User Guide for Synchro Studio 7, Synchro plus SimTraffic and 3D Viewer* published by Trafficware (Page 23-12),

"B## is a column that is not always present and is used for reports on the queue for a bend link. If an approach link has a bend upstream, the queue for the bend link is recorded separately. The queue is reported with the downstream intersection because the queue is caused by that intersection. The queue for the bend links is recorded separately because the number of lanes can change at the bend."

At the D-19/I-96 WB ramps intersection, one limiting factor is the maximum three lanes approaching the intersection at the exit ramp due to the short decision distance on the I-96 WB Off ramp. The decision distance for the ramp is not adequate to allow for a four lane approach. MDOT has directed HRC to analyze the signalized intersection with a fourth lane for right turn traffic with 300 feet of storage. Under these traffic volumes a roundabout with a similar three lane entry from the ramps will show better performance for a longer period of time. This is described in more detail in Section 10 - Roundabout Analysis.

#### Recommendations

- <u>D-19/I-96 WB Ramps</u> This intersection will significantly change with the growth in background traffic, the National Street Extension and the projected development along the extension in the future. HRC recommends a multi-lane roundabout instead of geometric improvements to the signalized intersection.
- <u>Pinckney (Michigan)/Marion(Mason)</u> A 90 second cycle length is recommended to achieve a desirable level of service. Dedicated left turn phases are recommended for northbound Pinckney and eastbound Marion/westbound Mason, with modernization to accommodate the addition of left turn phasing. An overlap phase is also recommended for the eastbound right turning vehicles. At some point before full build out of development on National Street an eastbound exclusive right turn lane and extended right and left turn lane storage lengths will be necessary, but should be verified by a development study prior to installation.
- <u>Grand River Avenue/Michigan Avenue</u> The 90 second cycle length was not changed. However, HRC recommends that the splits and left turn phasing be modified to accommodate future traffic.
- <u>Michigan Avenue/Sibley Street</u> This intersection is adjacent to Grand River Avenue. It is recommended that the signal timing plan here be coordinated with the plan running at Grand River Avenue/Michigan Avenue.

- <u>Grand River Avenue/National Street</u> This intersection will significantly change with the extension of National Street to D-19 in the future. HRC recommends an exclusive right turn lane for the northbound approach of National Street. Because of the high volume of left-turning traffic during the PM peak hour, HRC recommends dedicated left turn phases for westbound Grand River Avenue and southbound National Street. HRC also recommends adding an overlap phase for the northbound right turn lane. A 90 second cycle length was used for the 2015 and 2030 analyses during the AM and PM peak periods.
- Lucy Road, between CSX Railroad Crossing and Grand River Avenue between the time of the opening of the National Street Extension and the full build out of the property along the National Street Extension it is recommended to pave this section of Lucy Road to alternate path for right turning vehicles because of the increased demand on the intersection of Grand River Avenue/National Street. Westbound left turns and northbound right turns could be split more evenly between the two intersections if this section of Lucy Road were paved to handle the additional traffic.



# Section 9 - I-96 WB Off Ramp Analysis – With National Street

To analyze the operations of an off ramp there are two separate analyses to be performed:

- Diverge analysis capacity analysis of the freeway to ramp connection using Highway Capacity Software
- 2. Ramp terminal analysis capacity and queuing analyses of the intersection at the end of the ramp using Synchro

#### **Diverge Analysis**

MDOT requested that HRC provide a diverge analysis to determine what year the ramp will fail based on the freeway/ramp junction. Diverge analysis refers to the ability of traffic to exit the mainline freeway and merge onto the ramp. A diverge analysis looks at the amount of traffic carried by the freeway and the distance ramp traffic is given to exit the freeway and enter the ramp area.

The diverge point from I-96 WB to the I-96 WB Off Ramp was analyzed using Highway Capacity Software (HCM+) for the AM and PM peak hours for two scenarios with and without the added traffic from the National Street development for the two analysis years associated with the roundabout analysis:

- Future 2015 Existing traffic projected to 2015 using revised growth rates provided by MDOT.
- Future 2030 Future 2015 traffic projected to 2030 using revised growth rates provided by MDOT.

Westbound I-96 traffic exiting at D-19 was projected to increase at a growth rate of 1.5% per year from existing 2005 traffic volumes with an 18% increase in 2015 to account for the effects of the opening of the Latson Road / I-96 interchange. The following table details the level of service for the freeway /ramp diverge.



| Period  | Scenario                          | Future<br>2015 | Future<br>2030 |
|---------|-----------------------------------|----------------|----------------|
| AM Peak | Without National Street Extension | В              | С              |
|         | With National Street Extension    | В              | С              |
|         |                                   |                |                |
| PM Peak | Without National Street Extension | В              | В              |
|         | With National Street Extension    | В              | В              |

# Table 22: Level of Service Results of Diverge AnalysisI-96 WB / I-96 WB Off Ramp

In the year 2030, the ramp diverge area will operate at an acceptable level of service with or without the addition of National Street traffic. The ramp does not fail between now and the year 2030.

#### Queuing Analysis for the I-96 WB Off Ramp

HRC was asked by MDOT to determine at what year the queue from the signalized intersection on the I-96 WB Off Ramp would reach a point of interference with the I-96 WB freeway traffic. Based on I-96 WB Off ramp geometry, the distance to the gore area of the ramp is between 500 and 600 feet. To ensure no interference with the I-96 freeway traffic, a distance of 500 feet was taken as the maximum distance. The background analyses are based on optimized signal timings. The future analyses include maximum laneage and optimized signal timings. PM peak hour was reviewed due to higher ramp volumes.

The Synchro traffic model uses two links to model the I-96 WB Off Ramp (one link for the approach to the intersection and the second for the loop segment that extends to the gore area of the freeway ramp). Queues are reported for each turning movement and the longest of the eastbound queues will be used to determine the maximum queue length. SimTraffic queues are reported by link, requiring that the queues for the two links making up the total ramp be added together to obtain the total queue length.

Table 23: Queue Analysis for the I-96 WB Off Ramp

| Period         | Scenario        | Synchro<br>95 <sup>th</sup> Percentile Queue<br>(feet) | SimTraffic<br>95 <sup>th</sup> Percentile Queue<br>(feet) |
|----------------|-----------------|--|---|
|                | Background 2015 | 624  | 304+623=927   |
| PM Peak Hour   | Future 2015     | 243  | 351+770=1,121   |
| PIVI Peak Hour | Background 2030 | 811  | 308+615=923   |
|                | Future 2030     | 336  | 287+610=1,197   |

The 95<sup>th</sup> percentile queue will exceed the ramp distance when the background 2015 PM Peak hour scenario is in place.



# Section 10 - Roundabout Analysis – With National Street

For the roundabout analysis, HRC and the City partnered with DLZ Michigan, Inc. (DLZ) to evaluate the performance of a roundabout and compare it against a signalized option at the D-19/I-96/National Street interchange. An analysis of the intersection was performed using the roundabout modeling software Rodel for the year 2030 peak hour volumes to determine the required geometry and future Level of Service. The roundabout was analyzed at the 50 percent confidence level for capacity (i.e., the capacity that is most likely to occur at the intersection). The roundabout was also tested at the 85 percent confidence level (i.e., a pessimistic capacity) to ensure the roundabout would provide acceptable LOS in a "worst case" scenario.

Based on the Rodel analysis, all approaches would have two-lane entries except for the I-96 off ramp which would be three lanes (Figure 16). The roundabout would have two circulating lanes that are each 16 feet wide (curb face to curb face) except for the south part of the circulating road which would have three 14-foot wide circulating lanes. The diameter of the roundabout would be approximately 210 feet.

The Rodel analysis showed that the above-noted geometry would provide LOS A in year the 2030 for the AM and PM peak hours at the 50 percent confidence level, with an average delay per vehicle of 5.1 and 6.0 seconds, respectively. At the 85 percent confidence level, the roundabout would still provide acceptable traffic operations for this scenario in 2030 (LOS A with average delay of 8.5 seconds in the AM and LOS B with average delays of 10.0 seconds in the PM). See attached Rodel outputs in Appendix E.

If traffic volumes eventually exceed the 2030 projections, right turn semi-bypass lanes could be constructed on the eastbound and westbound approaches to increase capacity and provide acceptable operations. The eastbound bypass lane would likely need to be constructed first. These improvements would be relatively low cost and would increase total capacity at the roundabout by approximately 25 percent.

#### Queuing Analysis for the I-96 WB Off Ramp

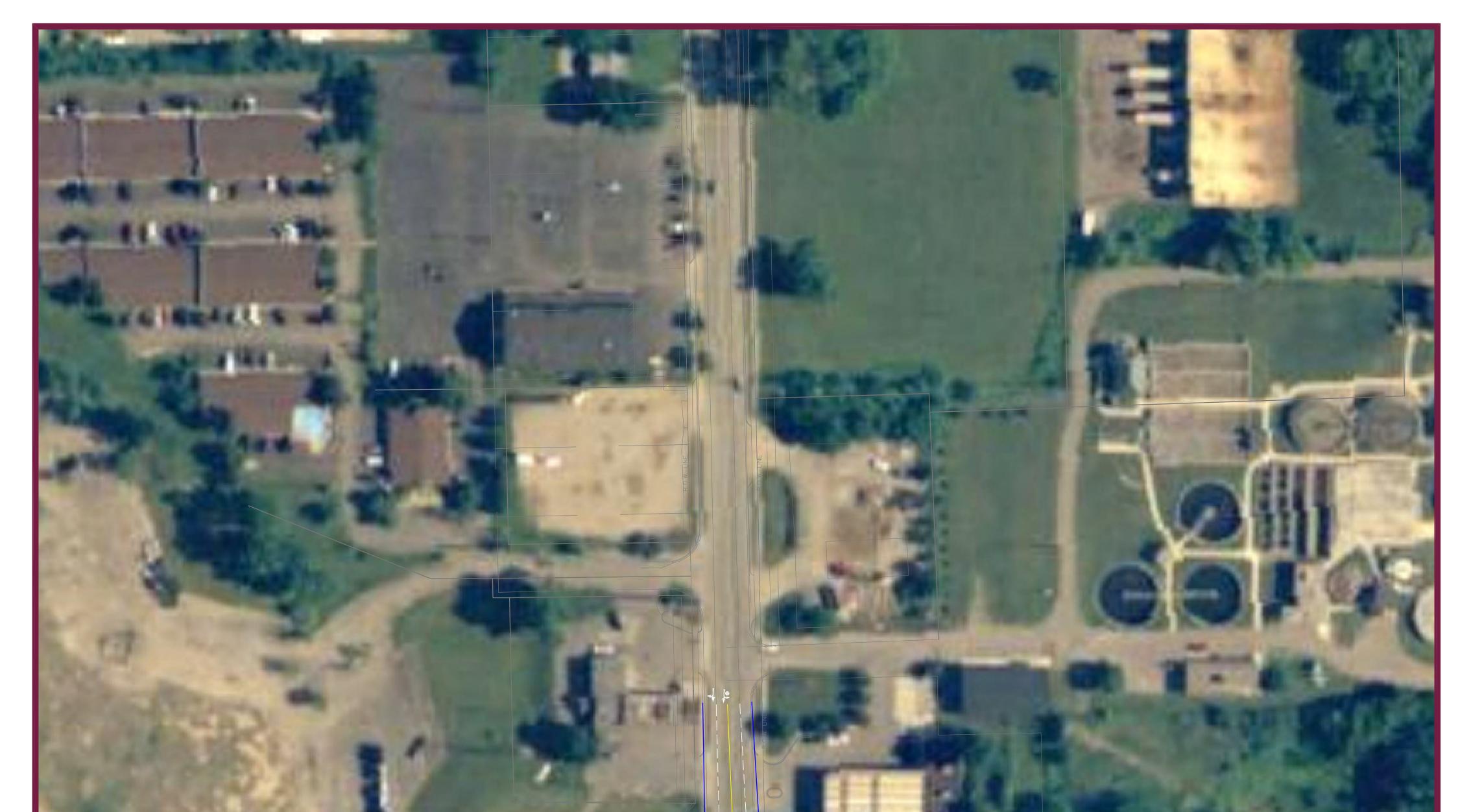
This geometry was also analyzed to determine potential queue lengths on the eastbound approach (I-96 off ramp). In order to ensure queues from the roundabout would not back down the off ramp and onto



the freeway, a worst-case scenario was used to determine the queue length. Using 2030 traffic volumes and 1-minute time slices in Rodel, the maximum queue at the 85 percent confidence level was doubled to determine the maximum number of vehicles queuing. This resulted in a queue of 14 vehicles. As shown in Figure 16, the queue length would be approximately 130 feet long and would not back up anywhere near the freeway. As per the MDOT roundabout guide, the preferred method for calculating queue length is to double the maximum queue at the 50 percent confidence level. Using this method, the queue would be six vehicles (approximately 50 feet). Considering this information, the maximum queue expected at the roundabout in 2030 is likely less than 10 cars.

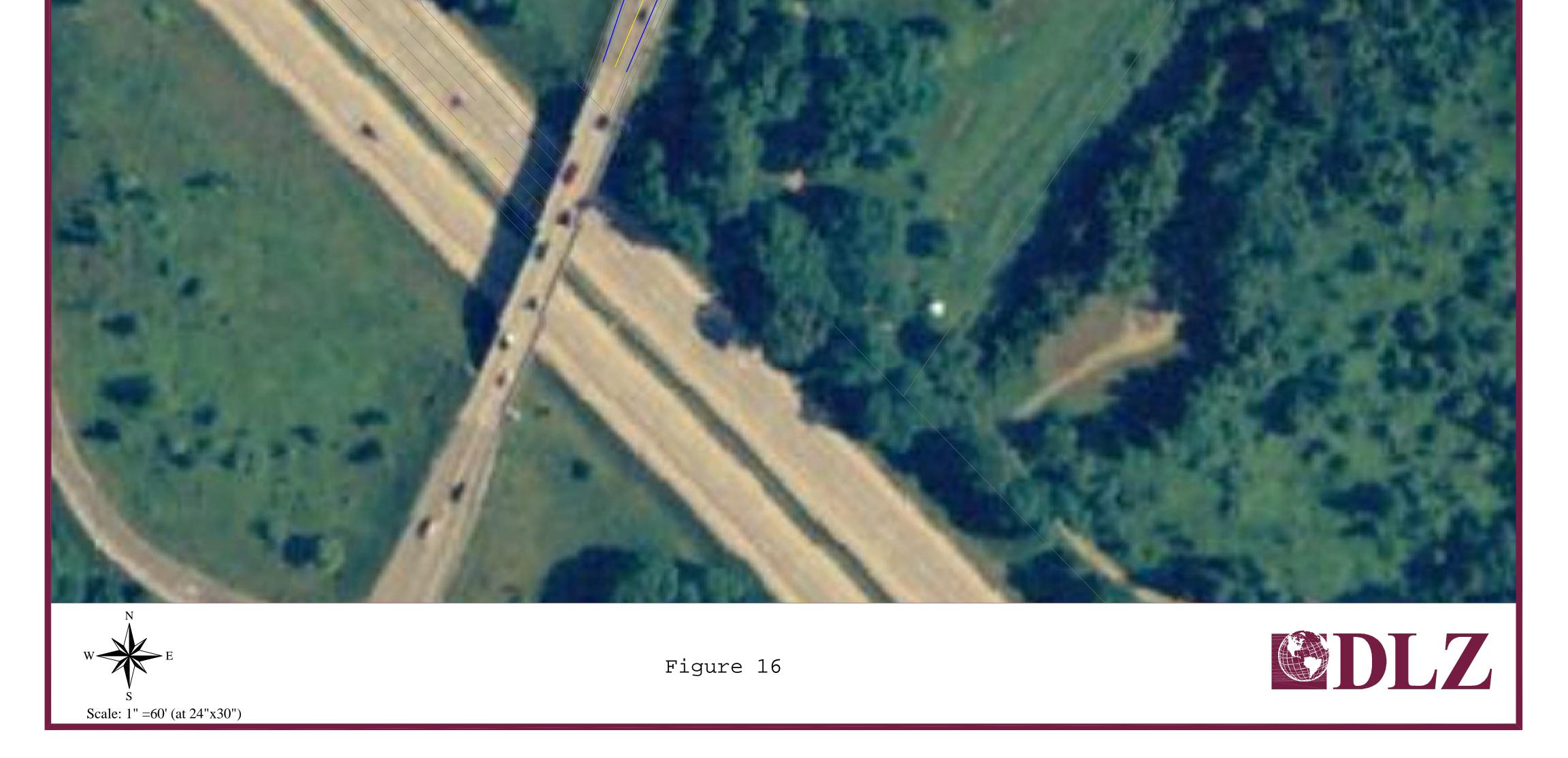
When compared to the traffic signal option, the roundabout provides better Level of Service, shorter queues and does not negatively impact the operation of the I-96 Off ramp.





 85% CL, 15 min fime slice, max queue = 5 vehicles
 50% CL, 15 min time slice, max queue x 2 = 6 vehicles (recommended method per MDOT Rdbt guide)

85% CL, 1min time slice, max queue = 7 vehicles
50% CL, 1 min time slice, max queue x 2 = 8 vehicles
85% CL, 1min time slice, max queue x 2 = 14 vehicles



#### Conclusions

HRC was directed by MDOT to use growth rates to project background traffic volumes for the years 2015 and 2030 and HRC developed a methodology for calculating the traffic expected to use a new bypass called the National Street Extension. Trips to be generated by proposed projects along the National Street Extension were assigned to the network and incorporated into the future 2015 scenario.

When projecting traffic to the background 2015 and 2030 scenarios, growth rates were utilized because the regional transportation planning model could not provide specific growth factors for each intersection turning movement. The use of growth rates can overestimate the number of vehicles when used to project for a period greater than five years. The Future 2015 Scenario includes the redistribution of traffic due to the connection of the National Street Extension, and the additional traffic due to the development expected along the National Street Extension. Future 2030 traffic was projected using Future 2015 traffic and growth rates provided by MDOT to project traffic to 2030.

Using Synchro software, HRC conducted capacity analyses for ten intersections in the study area within the City of Howell. Four of these intersections are signalized. The remaining six intersections do not warrant signalization. HRC developed five scenarios to analyze: Existing, Background 2015, Background 2030, and Future 2015 and Future 2030 with a National Street Extension.

The benefits of the National Street Extension are seen in two unsignalized intersections and one signalized intersection. Both Grand River Avenue/Barnard and Grand River Avenue/Washington showed an improvement between Background 2015 and Future 2015 scenarios in several turning movements level of service with the opening of the National Street Extension. The signalized intersection of Grand River Avenue/Michigan Avenue will have an overall delay reduction and improvement in some turning movements due to signal timing modifications only.

An alternative to traffic signalization was evaluated at the D-19/I-96 WB ramps. Using RODEL software, HRC and DLZ, Inc. evaluated a four leg multi-lane roundabout for Future 2030 volumes. The RODEL results showed that a roundabout will handle traffic volumes in 2030 with a LOS B or better.



#### Recommendations

HRC is recommending improvements to several signalized intersections in the study area for the Future 2015 and 2030 scenarios. To achieve the level of service shown in Section 8, HRC made the following changes to the intersections:

- <u>D-19/I-96 WB Ramps</u> This intersection will significantly change with the growth in background traffic, the National Street Extension and the projected development along the extension in the future. HRC recommends a multi-lane roundabout instead of geometric improvements to the signalized intersection. The roundabout was found to operate at a Level of Service B, while a signalized intersection was shown to queue beyond the length of the exit ramp. The selection of this location for connecting National Street is detailed in Section 2.
- <u>Pinckney (Michigan)/Marion(Mason)</u> A 90 second cycle length is recommended to achieve a desirable level of service. Dedicated left turn phases are recommended for northbound Pinckney and eastbound Marion/westbound Mason, with modernization to accommodate the addition of left turn phasing. An overlap phase is also recommended for the eastbound right turning vehicles. At some point before full build out of development on National Street an eastbound exclusive right turn lane and extended right and left turn lane storage lengths will be necessary, but should be verified by a development study prior to installation.
- <u>Grand River Avenue/Michigan Avenue</u> The 90 second cycle length was not changed. However, HRC recommends that the splits and left turn phasing be modified to accommodate future traffic.
- <u>Michigan Avenue/Sibley Street</u> This intersection is adjacent to Grand River Avenue. It is recommended that the signal timing plan here be coordinated with the plan running at Grand River Avenue/Michigan Avenue.
- <u>Grand River Avenue/National Street</u> This intersection will significantly change with the extension of National Street to D-19 in the future. HRC recommends an exclusive right turn lane for the northbound approach of National Street. Because of the high volume of left-turning traffic during the PM peak hour, HRC recommends dedicated left turn phases for westbound Grand River Avenue and southbound National Street. HRC also recommends adding an overlap phase for the northbound right turn lane. A 90 second cycle length was used for the 2015 and 2030 analyses during the AM and PM peak periods.
- <u>Lucy Road, between CSX Railroad Crossing and Grand River Avenue</u> Between the time of the opening of the National Street Extension and the full build out of the property along the National Street Extension, it is recommended to pave this section of Lucy Road to relieve the stress of the increased demand on the intersection of Grand River Avenue/National Street. Westbound left

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turns and northbound right turns could be split more evenly between the two intersections if this section of Lucy Road were paved to handle the additional traffic.



# Section 12 - Qualifications of Preparers



*Education* B.S., Civil Engineering *University of Michigan 1967* 

M.S., Transportation and Traffic Engineering University of Michigan 1968

Professional Registration/ Certification Professional Engineer, Michigan No. 19919

Professional Traffic Operations Engineer No. 393

Professional Engineer, Illinois No. 30429

Traffic Engineer, California No. TR363

Professional Engineer, Missouri No. E 30024

Professional Engineer, Florida No. 67867

Real Estate Broker, Michigan No. 3617631

Affiliations

American Public Works Association

American Society of Civil Engineers

Engineering Society of Detroit

Past International President-Institute of Transportation Engineers

Intelligent Transportation Society of America

Intelligent Transportation Society of Michigan

International Municipal Signal Association



### Richard Beaubien, P.E., PTOE

Associate Transportation Department Head

Mr. Beaubien has been the Transportation Director for Hubbell, Roth & Clark, Inc. since 1989. He has 40 years of experience in municipal traffic engineering, transportation planning, highway design, traffic system operations, right-of-way acquisition, and Intelligent Transportation Systems.

#### **Professional Experience**

Mr. Beaubien's prior experience includes 14 years as the Transportation Director for the City of Troy, Michigan; 2 years as Chief Engineer for Reid, Cool & Michalski Traffic and Transportation Engineers; and 5 years as a Highway Engineer for the Federal Highway Administration. He chairs the Metro Detroit Incident Management Coordinating Committee. He was the 2006 – 2007 President of the Intelligent Transportation Society of Michigan.

Mr. Beaubien has been recognized as a traffic engineering expert in litigation involving traffic crashes. He is a registered professional engineer in Michigan, Illinois, Missouri, Florida and California. He has been certified as a Professional Traffic Operations Engineer by the Transportation Professional Certification Board, Washington, D.C. He is a past International President of the Institute of Transportation Engineers and a recipient of the Institute's Marsh Award.

#### Advanced Traffic Management System Road Commission of Macomb County

Project Manager for the Road Commission of Macomb County to design and install an Advanced Traffic Management System (ATMS) for portions of Mound Road, Metropolitan Parkway and Harper Avenue. This project adds four new systems to the closed-loop signal system being implemented throughout Macomb County. This project integrates the latest technology for traffic signal systems, which communicates directly with the Road Commission's Traffic Operations Center in Mt. Clemens. The project provides a wireless communication system between traffic signal systems, ITS components and the Traffic Operations Center. The benefits of this new system include an improved traffic flow with the capability to change traffic signal timings based on traffic volumes and in the case of emergency situations as well as reductions in operations expenses on signals.

#### *Road Safety Audit for the Proposed Brandon Elementary School* Charter Township of Brandon

Project Manger for the road safety audit of a driveway onto Oakwood Road from the proposed Brandon Elementary School. A road safety audit is an examination of a roadway, in which an independent qualified auditor identifies and reports on safety issues. The road safety audit included: 24 hour traffic volumes and speeds; sight distance evaluation; a detailed crash analysis; projected traffic volumes and patterns for the proposed elementary school and recommended road improvements for safe access to and from the site.



International Right-of-Way Association

National Society of Professional Engineers

Michigan Society of Professional Engineers

SEMCOG Transportation Advisory Council

Transportation Research Board

#### Awards

President's Award, Intelligent Transportation Society of Michigan, 2003

Marsh Award, Institute of Transportation Engineers, 1998

Coordinating Council Award, Institute of Transportation Engineers, 1996

Arthur C. Gibson Award, Institute of Transportation Engineers, Michigan Section, 1990

Engineer of the Year, Michigan Society of Professional Engineers, Oakland Chapter, 1987

Outstanding Civil Engineer, American Society of Civil Engineers, Southeast Michigan Branch, 1986

Outstanding Engineer in Government, Michigan Society of Professional Engineers, 1985

## Richard Beaubien, P.E., PTOE

Associate Transportation Department Head

#### *Traffic Circulation Analysis – Ann Arbor High School* City of Ann Arbor

Project Manager for a Circulation and Safety Study to improve overall safety in and around school campus for drivers, bus users and pedestrians. Analyzed existing traffic conditions, identified deficiencies and suggested countermeasures. Conducted license plate survey to track traffic on the school premise. Performed capacity analysis using HCS and detailed crash analysis at two intersections and two driveways.

#### *Intersection Safety Audits* City of Wixom

Project Manager for Safety Studies at three intersections in Wixom. Performed peak hour turning movement counts, collected 24-hour traffic volume and speed data, reviewed crash history, reviewed geometrics, and suggested countermeasures with cost estimates for two adjacent intersections on Beck Road in Wixom.

#### Williams Lake Road Environmental Assessment Road Commission for Oakland County

Project Development Study to evaluate alternative alignments and geometry for Williams Lake Road in Waterford Township. Conducted traffic and safety analyses to determine the preferred alternative for a realigned Williams Lake Road. Conducted traffic crash analysis and license plate survey to determine the safety and traffic flow impacts of the proposed realignment. Assessed environmental impacts.

#### Oakland County Signal Systems Optimization Project, Phase 2 Road Commission for Oakland County

Project Manager for the Road Commission for Oakland County project to analyze and retime 324 traffic signals in 13 communities in southeast Oakland County. The project was funded by MDOT with a federal grant from the Congestion Mitigation Air Quality program. The program improved the efficiency and safety of the roadway network and improved air quality by optimizing the signal timings and providing of progression on the major corridors.

#### *I-696/Franklin Road Interchange Roadway Network Evaluation* City of Southfield

Project Manager for a roadway network evaluation, including signal retiming, with the construction of slip ramps at Franklin Road to improve access to the area without detrimental effects on the operation of I-696. Southfield retained HRC to determine if the slip ramps were constructed as planned, what local road system improvements would be needed to make both slip ramps operate effectively. HRC tested the design strategies using Synchro and the CORSIM simulation model with policy and program priorities as determined by the City of Southfield.

#### Oakland County SCATS Clearance Interval Study Road Commission for Oakland County

Project Manager for the Road Commission for Oakland County project to develop clearance interval timing for Sydney Coordinated Adaptive Traffic Systems (SCATS) signals in Oakland County. A total of 274 intersections were surveyed for approach speed, grade, pedestrian and vehicle clearance distances. Data collected for each SCATS signal was





Associate Transportation Department Head

used to calculate the required vehicle change and clearance intervals according to RCOC and ITE standards. Results were calculated and reported in an easy to use spreadsheet format.

#### Squirrel Road Corridor Traffic Study Auburn Hills, Michigan

Project Manager for development of a Master Plan for road improvements in eastern Auburn Hills and western Rochester Hills, Michigan. HRC was retained by the Cities of Auburn Hills and Rochester Hills to study the future needs of the Squirrel Road Corridor in the City of Auburn Hills. The study area included the eastern part of Auburn Hills, and a portion of the western part of the City of Rochester Hills. The study area suggested intersection and segment improvements where needed.

#### *Northville Traffic Study* Northville, Michigan

Project Manager for the City of Northville Downtown Traffic Study. The City of Northville retained HRC in 1998 to undertake a comprehensive citywide traffic study to determine what improvements, if any, will be necessary to safely accommodate the future traffic volumes. An important emphasis was on retaining the city's small town heritage and attractive downtown shopping area.

#### State Farm Intersection Safety Studies Road Commission for Oakland County

Project Manager for the State Farm Insurance project to conduct a traffic operations and safety study at three high crash intersections.

The safety work consisted of identifying existing safety issues through a thorough analysis of traffic crash data and traffic conflict characteristics for each of the study intersections. The study of traffic conflicts augments the traffic crash analysis by providing real-time information about potential collision causation.

The traffic operations work included a review of the physical and geometric attributes of the intersection, adjacent land uses and turn movement counts during the AM and PM Peak hours. HRC then conducted capacity analysis by intersection by approach by time of day.

#### *Tienken Road Corridor Study* Rochester Hills, Michigan

Project Manager for a study of Tienken Road in Rochester Hills, Michigan to evaluate what road, signal, and pedestrian improvements are needed to accommodate development activities in the northeast portion of the City.

The HRC team analyzed a comprehensive array of data about the corridor including topographical data, environmental assessment and right-of-way. The major roads in the area were simulated using CORSIM/NETSIM software in order to simulate existing traffic conditions and to test which future alternative had a high probability of success.

#### Access Management Study for Main Street City of Adrian

Project Manager for a study to analyze the safety and operational





Associate Transportation Department Head

characteristics of access to a redevelopment site near downtown Adrian.

## 26 Mile Road Corridor Study

#### **Road Commission of Macomb County**

Project Manager for an environmental assessment of 26 Mile Road in Macomb County, Michigan. The Road Commission of Macomb County selected a team headed by Hubbell, Roth & Clark, Inc. (HRC) to prepare an Environmental Assessment for the 26 Mile Road corridor in Macomb County. This project required the analysis of the impacts of upgrading 26 Mile Road (2-lane rural type road) in Macomb County, Michigan. The limits of the project were the Oakland County line (Dequindre Road extended) on the west to the St. Clair County line on the east.

## M-15 Access Management Plan

#### Michigan Department of Transportation

Project Manager for the MDOT project to develop an Access Management Plan for M-15, I-75 to I-69. The M-15 corridor is 20 miles long, traverses through seven communities and is maintained by two county road commissions. Recommendations for existing problems focused on Access Management techniques such as sharing and consolidating driveways, separating driveways from intersections, and correcting offset problems.

#### Abbott Road Environmental Assessment City of East Lansing

Transportation Manager responsible for developing and evaluating design concepts to widen Abbott Road from 2 to 5 lanes to meet future capacity needs. Concepts included safety and access management concerns.

# *Evergreen Corridor Study* Detroit, Michigan

Project Manager for the AAA Michigan Study of the Evergreen Corridor in the City of Detroit. AAA Michigan retained HRC to conduct a safety study for the Evergreen Road corridor (between 8 Mile Road and Warren Avenue). The purpose of this study was to conduct a review of the traffic conditions and collision characteristics of the Evergreen Road corridor, to identify any operational deficiencies that may be affecting traffic safety, and to develop countermeasures to reduce the collision risk along the corridor. The study also included re-timing of the signals along the corridor.

#### M-24 Corridor Study

Project Manager for study of M-24 corridor to document existing traffic conditions, forecast future traffic volumes and develop long- and short-term corridor improvements.

#### Macomb County Traffic Operations Center Road Commission of Macomb County

Project Manager for the development of an ITS Master Plan and the Design/Build of a Traffic Operations Center for the Road Commission of Macomb County in Mt. Clemens, Michigan. The new traffic operations center was designed to monitor and communicate with 170 signalized intersections on the most congested arterials in southern Macomb County. In addition to building a new facility to centralize all of the traffic signal operations, the project developed an Intelligent Transportation Systems





Associate Transportation Department Head

Master Plan to guide the Road Commission's future investments in technologies and equipment to improve traffic flow and reduce congestion throughout the county.

#### ITS/ATMS/ATIS Deployment-Metro Detroit

Project Manger for the HRC portion of the design/build of 145 miles of ITS equipment on metro Detroit freeways. HRC was part of the Iteris (formerly Rockwell) team responsible for the implementation of one of the world's largest freeway instrumentation projects in Metropolitan Detroit. Nearly 145 miles of freeway were equipped with both Advanced Transportation Management System (ATMS) and Advanced Traveler Information System (ATIS) elements. A major feature of the project was the integration of MDOT's intelligent transportation systems center (MITS Center) in downtown Detroit with the Road Commission for Oakland County's arterial traffic operations center in Waterford Township.

#### Oakland County Real Time, Adaptive, Advanced Traffic Management

Project Manager for the first phase of the FAST-TRAC project in Oakland County, Michigan. The project installed an advanced Traffic Management System which incorporates the Sydney Coordinated Adaptive Traffic System (SCATS) for real time adaptive traffic control and Autoscope Machine Vision Vehicle Detection System. This is the first application of the SCATS Traffic Control System in the western hemisphere. This is also the first widespread application of the Autoscope Machine Vision Vehicle Detection System to an arterial street system. HRC's role in this project included plans for the new Traffic Operations Center.

#### **Presentations/Publications**

"A Regional Concept of Transportation Operations for Metropolitan Detroit," 14<sup>th</sup> World Congress on Intelligent Transport Systems, Technical Paper 1068, Beijing, China, October 2007.

"The Metro Detroit Regional Transportation Operations Collaboration and Coordination Initiative," Institute of Transportation Engineers 2006 Annual Meeting Compendium of Technical Papers, August 2006.

"Traffic Incident Management in Metro Detroit: A Prelude to Regional Operations," Institute of Transportation Engineers 2004 Annual Meeting Compendium of Technical Papers, August 2004

"How a Good Traffic Engineering Program Can Help Defend Public Agencies," Institute of Transportation Engineers 2001 Annual Meeting Compendium of Technical Papers, August 2001

"Working Together for a Safer Construction Zone," Institute of Transportation Engineers 2000 Annual Meeting Compendium of Technical Papers, August 2000

"What Every City Should Know About Intelligent Transportation Systems," National League of Cities Issues and Options, Volume 7, No. 1, January/February 1999, (with Beata Lamparski), pp. 7-11.





Associate Transportation Department Head

"Harmonization Programs: What is the Role of Liability?", Compendium of Technical Papers, Institute of Transportation Engineers Conference on Enhancing Transportation Safety in the 21<sup>st</sup> Century, March 1999.

"The Joy of Traffic Engineering... and ITE," ITE Journal, Vol. 68, No. 10, October 1998, pp. 34-36.

"Designing and Building ITS for Metro Detroit Freeways - Lessons Learned," 1998 Compendium of Technical Papers, Institute of Transportation Engineers, August 1998.

"Does Traffic Calming Make Streets Safer?" Compendium of Technical Papers, Institute of Transportation Engineers, Conference on Harmonizing Transportation and Community Goals, March 1998.

"Early Winners for Metro Detroit's Incident Management Program," 1996 ITE International Conference Resource Papers, March 1996, pp. 21-25.

"Advanced Technology - A Tool for Urban Traffic Engineers in Incident Management," 1995 Compendium of Technical Papers, Institute of Transportation Engineers, August 1995, pp. 248-252.

"Metro Detroit's Incident Management Program - Applying ITS Technology," ITE Journal, Vol. 65, No. 4, April 1995 (with Kunwar Rajendra), pp. 19-24.

"Smart Streets - A Tool for Urban Traffic Engineers," Traffic Technology International '95, pp. 162-167.

"Incident Management as a Platform for IVHS Deployment in Metropolitan Detroit," Compendium of Technical Papers, Institute of Transportation Engineers, Canadian District, June 1994, pp. 307-321.

"Bringing 'Smart Streets' to Metropolitan Detroit," Planning & Zoning News, Vol. 12, No. 7, May 1994 (with Kunwar Rajendra) pp. 14-17.





#### Education

B.S., C.E., Transportation *Wayne State University 2000* 

M.S., C.E., Transportation Wayne State University 2002

#### Professional Registration/ Certification

Professional Engineer, Michigan No. 51514

Professional Traffic Operations Engineer No. 1427

#### Affiliations

American Society of Civil Engineers

Institute of Transportation Engineers

Michigan Traffic Signal Summit

Tau Beta Pi, The Engineering Honor Society

Women's Transportation Seminar

# Colleen Hill, P.E., PTOE

Transportation Project Engineer

Ms. Hill prepares transportation studies, impact studies for land developments, traffic crash analysis, traffic operations, and safety studies. Responsible for modeling and simulating transportation networks to optimize, also evaluating safety and operational improvements. Software proficiency in Highway Capacity Software, Synchro/SimTraffic, CORSIM, ACCUSIM II, MicroStation, Autodesk Map 3D, RODEL. Also responsible for preparing traffic control and detours plans, traffic signal design and layout plans. Officer of the Institute of Transportation Engineers, Michigan Section.

#### **Professional Experience**

#### Abbott Road Environmental Assessment City of East Lansing

Responsible for preparing Environmental Assessment to widen one mile of Abbott Road from a 2 to 5 lane road. Prepared crash analysis and responsible for design concept report. Conducted noise analysis in accordance with provisions of 23 CFR Section 772 of Federal Code of Regulations. Type I project did not trigger noise abatement measures.

#### *Road Safety Audit for the Proposed Brandon Elementary School* Charter Township of Brandon

Project Engineer for the road safety audit of a driveway onto Oakwood Road from the proposed Brandon Elementary School. Ms. Hill performed a sight distance evaluation and a detailed crash analysis for the road segment to be accessed by the proposed driveway. A road safety audit is an examination of a roadway, in which an independent qualified auditor identifies and reports on safety issues. The road safety audit included: 24 hour traffic volumes and speeds; sight distance evaluation; a detailed crash analysis; projected traffic volumes and patterns for the proposed elementary school and recommended road improvements for safe access to and from the site.

#### *Traffic Circulation Analysis for Ann Arbor Huron High School* City of Ann Arbor

Circulation and Safety Study to improve overall safety in and around school campus for drivers, bus users and pedestrians. Analyzed existing traffic conditions, identified deficiencies and suggested countermeasures. Conducted license plate survey to track traffic on the school premise. Performed capacity analysis using HCS and detailed crash analysis at two intersections and two driveways.

#### *Intersection Safety Audits* City of Wixom

Safety Studies at two intersections in Wixom. Performed peak hour turning movement counts, collected 24-hour traffic volume and speed data, reviewed crash history, reviewed geometrics, and suggested countermeasures with cost estimates for two adjacent intersections on Beck Road in Wixom.

#### Oakland County SCATS Clearance Interval Study Road Commission for Oakland County

Coordinated the data collection effort for a total of 274 intersections included in the project. Each intersection was surveyed for approach speed, grade, pedestrian and vehicle clearance distances. Developed a user-friendly





# Colleen Hill, P.E., PTOE

Transportation Project Engineer

spreadsheet to calculate and report vehicle and pedestrian clearance intervals.

#### *Squirrel Road Corridor Study* City of Auburn Hills

Involved in data collection, development and optimization of 35 mile network using Synchro for the study to evaluate the future capacity needs of the Squirrel Road Corridor. Study area encompassed 36 signalized intersections, 5 interchanges, and several unsignalized intersections.

#### Oakland County Signal Systems Optimization Project (Phase 2) Road Commission for Oakland County

Performed QA/QC for transportation networks modeled and optimized through this project. Calculated clearance intervals as per RCOC accepted practice. Performed safety analysis for over 160 study intersections, performed traffic crash pattern analysis and prepared recommendations for safety improvements. Prepared red-lined traffic signal timing plans. Also assisted with field checks of installed signal timing plans and prepared recommendations for revised signal timing.

#### 26 Mile Road Environmental Assessment Road Commission of Macomb County

Collected turning movement counts and geometric information for 27 intersections along 26 Mile Road in Macomb County. Performed traffic crash analysis for intersections and segments in the study area. Modeled the 19 mile long corridor using Synchro software for Build and No Build scenarios.

## Williams Lake Road Environmental Assessment Waterford Township

Conducted a traffic and safety analysis to better determine appropriate termini of the project and provide the necessary justification for the preferred alternative for a realigned Williams Lake Road. Conducted traffic crash analysis and license plate survey to determine the safety and traffic flow impacts of the proposed realignment. Conducted air quality analysis for microscale carbon monoxide pollution using CAL3QHC, Version 2.0. CO concentrations were all below NAAQS for 1-hour and 8-hour exposures.

#### State Farm Intersection Safety Studies Road Commission for Oakland County

Reviewed geometrics, traffic volume, traffic crash and traffic conflict characteristics for three high crash intersections. Evaluated existing safety issues, recommended potential traffic safety engineering countermeasures, and developed an implementation plan of action.

# M-15 Access Management Plan

#### **Michigan Department of Transportation**

Performed driveway spacing analysis using MDOT, Oakland and Genesee County Standards. Responsible for performing traffic crash analysis for driveways and intersections along the M-15 corridor over its 20 mile length between I-75 and I-69.





# Colleen Hill, P.E., PTOE

Transportation Project Engineer

#### Rochester Road and South Boulevard Traffic Signal Design City of Troy

Prepared plans and special provisions per RCOC standards for construction and installation of a redesigned traffic signal. Configured traffic signal contact height and sag using SIGSPAN.

#### *Opdyke Road Traffic Signal Design* Bloomfield Township/City of Bloomfield Hills

Prepared plans and special provisions per RCOC standards for the construction and installation of two traffic signals, one of which was incorporated into the adjacent rail-highway grade crossing. Plans were prepared in accordance with the Michigan Manual of Uniform Traffic Control Devices. Coordinated construction activities with Canadian National Railroad.

# Acacia Park Drain Relief- Traffic Signal Removal Village of Beverly Hills

Prepared traffic signal and overhead sign removal plans and specifications/special provisions for the removal from service of a SCATS traffic signal. Coordinated permit approval from RCOC for traffic signal removal. Plans were prepared in accordance with RCOC Standards, the Michigan Manual of Traffic Control Devices, or as modified by the Engineer to meet site specific requirements.

# **Presentations/Publications**

"Intersection Safety within a Signal Optimization Project," Institute of Transportation Engineers 2004 Technical Conference and Exhibit Compendium of Technical Papers, March 2004 (with Stephen B. Dearing, P.E.).

"Intersection Safety within a Signal Optimization Project," Presented Institute of Transportation Engineers 2004 Technical Conference and Exhibit, March 31, 2004.

"Intersection Safety within a Signal Optimization Project," Presented Institute of Transportation Engineers Michigan Section Technical Session, February 12, 2004.

"Michigan ITE Website Update," Presented Institute of Transportation Engineers Michigan Section Technical Session, February 12, 2004.

"Change and Clearance Interval Design on Red-Light Running and Late Exits," Transportation Research Record, No. 1856 (p. 193-201), Washington D.C., 2003 (with Kerrie L. Schattler and Tapan K. Datta).



Appendix A

Intersection Turning Volumes

#### Pinckney and Pulford

AM PEAK

#### City of Howell 2005 Counts

|   |   | N  |  |   |   | S   |   |   |  | W  | В  |   | 1  |
|---|---|--|--|---|---|---|---|---|--|--|--|---|--|
|   |   | Ή  | R  |   |   | Т   | Т   | Н   | L  | Т  | F  | RT  | Total  |
|   | PC  | Т  | PC   | Т   | PC  | Т   | PC  | Т   | PC   | Т  | PC   | Т   |  |
| 7:00-7:15   | 103   | 10   | 3  | 0   | 1   | 0   | 163   | 6   | 0  | 0  | 3  |   | 289  |
| 7:15-7:30   | 146   | 3  | 13   | 0   | 0   | 0   | 153   | 10  | 3  | 0  | 0  | 0   | 328  |
| 7:30-7:45   | 180   | 14   | 6  | 0   | 0   | 0   | 162   | 9   | 2  | 0  | 1  | 0   | 374  |
| 7:45-8:00   | 208   | 8  | 9  | 0   | 0   | 0   | 169   | 7   | 1  | 0  | 2  | 0   | 404  |
| 8:00-8:15   | 244   | 19   | 13   | 0   | 2   | 0   | 164   | 16  | 1  | 0  | 2  | 0   |  |
| 8:15-8:30   | 137   | 9  | 6  | 0   | 0   | 0   | 141   | 10  | 0  | 0  | 1  | 0   |  |
| 8:30-8:45   | 168   | 3  | 4  | 0   | 1   | 0   | 166   | 12  | 3  | 0  | 2  | 0   |  |
| 8:45-9:00   | 171   | 10   | 23   | 0   | 1   | 0   | 148   | 11  | 0  | 0  | 1  | 1   | 366  |
| Peak Hour   | 778   |  | 41   |   | 2   |   | 648   |   | 7  |  | 5  |   | 1481   |
| Study Peak Hour   | 637   | 35   | 31   | D   | 1   | 0   | 647   | 32  | 6  | 0  | 6  | 0   | Conclusion of a reliance of                                  |
| Study Peak Hour Truck %   |   | 5%   |  | 0%  |   | 0%  |   | 5%  |  | 0%   |  | 0%  |  |
|   |   |  |  | 0.781111  |   |   |   | 0.965909  |  |  |  | 4   | 4  |
|   |   |  |  | V.701111  |   | PM PEAK   |   | 0.905909  |  |  |  | 1   |  |
|   |   | N  | в  | 0.781111  |   | PM PEAK   | B   | 0.905909  |  | w  | B  | 1   | 1  |
|   | T   |  | B<br>R'  |   |   | S   | B<br>Ti   |   | L`   | w<br>r   |  | 1   | Total  |
|   | TI<br>PC  |  |  |   |   | S   |   |   | PC   |  |  | т<br>1<br>1<br>Т  | Total  |
| 4:00-4:15   |   | H  | R  | T   | L   | S<br>T  | T   |   |  | Г  | <br>न  | Т   |  |
|   | PC  | H<br>T   | R<br>PC  | T<br>T  | L<br>PC   | S<br>T<br>T   | Tł<br>PC  | H<br>T  | PC   | r<br>T   | PC<br>0  | T<br>0  | 451  |
| 4:15-4:30   | PC 238  | H<br>T<br>9  | R<br>PC<br>2   | T<br>T<br>O   | L<br>PC<br>0  | T<br>T<br>O   | TF<br>PC<br>191   | H<br>T<br>8   | PC 2   | Г<br>Т1  | PC   | T<br>0<br>0   | 451<br>511   |
| 4:15-4:30<br>4:30-4:45  | PC<br>238<br>282  | H<br>T<br>9<br>8                                     | R<br>PC<br>2<br>8  | T<br>T<br>0<br>0  | L<br>PC<br>0<br>0   | Si<br>T   | TF<br>PC<br>191<br>206  | H<br>T<br>8<br>4  | PC 2   | Г<br>Т<br>0  | PC<br>0<br>2   | T<br>0<br>0   | 451<br>511<br>485  |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00   | PC<br>238<br>282<br>233   | H<br>T<br>9<br>8<br>9                                | R <sup>-</sup><br>PC<br>2<br>8<br>13                             | T<br>T<br>0<br>0<br>0   | L<br>PC<br>0<br>0   | S<br>T<br>T<br>0<br>0<br>0  | TF<br>PC<br>191<br>206<br>219   | H<br>T<br>8<br>4<br>5   | PC 2<br>1<br>3   | Г<br>Т<br>1<br>О<br>0                                    | PC<br>0<br>2<br>1  | T<br>0<br>0<br>0  | 451<br>511<br>485<br>410                                     |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15  | PC<br>238<br>282<br>233<br>201                                    | H T<br>9<br>8<br>9<br>4                              | R<br>PC<br>2<br>8<br>13<br>3                                     | T<br>T<br>0<br>0<br>0<br>0  | PC<br>0<br>0<br>2<br>1                                    | S<br>T<br>T<br>0<br>0<br>0<br>0   | TF<br>PC<br>191<br>206<br>219<br>196                                    | H<br>T<br>8<br>4<br>5<br>5                                    | PC 2<br>1<br>3<br>0                                    | T<br>T<br>1<br>0<br>0<br>0                               | F<br>PC<br>0<br>2<br>1<br>0  | T<br>0<br>0<br>0<br>0   | 451<br>511<br>485<br>410<br>464                              |
| 4:00-4:15<br>4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45                                 | PC<br>238<br>282<br>233<br>201<br>191                             | H<br>T<br>9<br>8<br>9<br>4<br>16                     | R<br>PC<br>2<br>8<br>13<br>3<br>14                               | T<br>T<br>0<br>0<br>0<br>0  | L<br>PC<br>0<br>0<br>2<br>1<br>3                          | S<br>T<br>0<br>0<br>0<br>0<br>0   | TF<br>PC<br>191<br>206<br>219<br>196<br>235                             | H<br>T<br>8<br>4<br>5<br>5<br>5<br>3                          | PC 2<br>1<br>3<br>0<br>2                               | T<br>T<br>1<br>0<br>0<br>0<br>0                          | FC<br>PC<br>2<br>1<br>0<br>0   | T<br>0<br>0<br>0<br>0<br>0<br>0   | 451<br>511<br>485<br>410<br>464<br>436                       |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30   | PC<br>238<br>282<br>233<br>201<br>191<br>190                      | H<br>T<br>9<br>8<br>9<br>4<br>16<br>6                | R<br>PC<br>2<br>8<br>13<br>3<br>14<br>14                         | T<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | L<br>PC<br>0<br>2<br>1<br>3<br>0                          | S<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | TF<br>PC<br>191<br>206<br>219<br>196<br>235<br>217                      | H<br>T<br>8<br>4<br>5<br>5<br>5<br>3                          | PC 2<br>1<br>3<br>0<br>2<br>2<br>2                     | T<br>T<br>1<br>0<br>0<br>0<br>0<br>0<br>0                | FC<br>PC<br>0<br>2<br>1<br>0<br>0<br>0   | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | 451<br>511<br>485<br>410<br>464<br>436<br>315                |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45  | PC<br>238<br>282<br>233<br>201<br>191<br>190<br>143               | H<br>T<br>9<br>8<br>9<br>4<br>16<br>6<br>4           | R<br>PC<br>2<br>8<br>13<br>3<br>14<br>14<br>17<br>17             | T<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | L<br>PC<br>0<br>0<br>2<br>1<br>3<br>3<br>0<br>0           | S<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0           | TF<br>PC<br>191<br>206<br>219<br>196<br>235<br>217<br>148               | H<br>T<br>8<br>4<br>5<br>5<br>5<br>3<br>4<br>1                | PC 2<br>1<br>3<br>0<br>2<br>2<br>2<br>2<br>2           | T T 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0                  | FC<br>PC<br>0<br>2<br>1<br>0<br>0<br>0<br>0<br>0   | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 451<br>511<br>485<br>410<br>464<br>436<br>315<br>383         |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:05-5:15<br>5:30-5:45<br>5:45-6:00<br>Peak Hour<br>Study Peak Hour | PC<br>238<br>282<br>233<br>201<br>191<br>190<br>143<br>190        | H<br>T<br>9<br>8<br>9<br>4<br>16<br>6<br>4           | R<br>PC<br>2<br>8<br>13<br>3<br>14<br>17<br>17<br>17<br>13       | T<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | L<br>PC<br>0<br>0<br>2<br>1<br>3<br>0<br>0<br>0<br>0<br>0 | S<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0           | Tr<br>PC<br>191<br>206<br>219<br>196<br>235<br>217<br>148<br>169        | H<br>T<br>8<br>4<br>5<br>5<br>5<br>3<br>4<br>1                | PC 2<br>1<br>3<br>0<br>2<br>2<br>2<br>2<br>2<br>0<br>6 | T T 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0                  | FC<br>PC<br>0<br>2<br>1<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 451<br>511<br>485<br>410<br>464<br>436<br>315<br>383<br>1816 |
| 4:15-4:30<br>4:30-4:45<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-8:00<br>Peak Hour                                 | PC<br>238<br>282<br>233<br>201<br>191<br>190<br>143<br>190<br>907 | H<br>T<br>9<br>8<br>9<br>4<br>16<br>6<br>4<br>7<br>7 | R<br>PC<br>2<br>8<br>13<br>3<br>14<br>17<br>17<br>17<br>13<br>38 | T<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | L<br>PC<br>0<br>2<br>1<br>3<br>0<br>0<br>0<br>0<br>6      | S<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TF<br>PC<br>191<br>206<br>219<br>196<br>235<br>217<br>148<br>169<br>856 | H<br>T<br>8<br>4<br>5<br>5<br>5<br>3<br>4<br>4<br>1<br>1<br>4 | PC 2<br>1<br>3<br>0<br>2<br>2<br>2<br>2<br>2<br>0<br>6 | T<br>T<br>1<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | FC<br>PC<br>0<br>2<br>1<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | 451<br>511<br>485<br>410<br>464<br>436<br>315<br>383         |

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#### Pinkney and Marion

#### AM PEAK

City of Howell September, 2005 Counts

|   |   |   | N   |   |   |                                      |   |  | SE   |   |  |  |   |   |  | в   |   |  |   |   | W   |   |   |                 |  |
|---|---|---|---|---|---|--------------------------------------|---|--|--|---|--|--|---|---|--|---|---|--|---|---|---|---|---|-----------------|--|
|   | PC L  | т <u> </u>                                | T   | <u>H</u>                                  | R   | T                                    | L   | T  | T  | 1   | R  | T  | L   | T   | T  | Н   | R   | T  | L   | ſ   | T   | H   |   | ۲ <u>۲</u>      | Total  |
| 7:00-7:15   | 18  | 1 7                                       | PC<br>64  | 2   | PC<br>8   |                                      | PC  | 1  | PC<br>100  |   | PC   |  | PC  | <u> </u>  | PG   | 1   | PC  | T  | PC  | T   | PC  |   | PC  | T               |  |
| 7:15-7:30   | 33  |   | 86  | - 2                                       | 10  | 0                                    |   | 0  | 95   | 3   | 2  | 0  | 34<br>33  | 0   | 34<br>10   |   | 35<br>27  | 3  | 25<br>23  | 0   | 3<br>15   | 2   | 2   | 0               |  |
| 7:30-7:45   | 29  |   | 99  | 0   | 20  | 1                                    |   | 0  | 125  | 2   | 14   |  | 33  | 0   |  | 2   | 40  |  | 38  | 2   | 26  | 2   |   |                 | 479  |
| 7:45-8:00   | 41  | 8   | 136   | 3   | 20  | 1                                    | o   | 0  | 120  | 2   | 7  | 0  | 42  |   | 39   | 2   | 40  | 4  | 33  | - 2                                       | 20  | 0   | 4   |                 | 519  |
| 8:00-8:15   | 31  | 11  | 127   | 4   | 15  | n                                    |   | 0  | 102  | 6   | 7  |  | 27  | 0   |  |   | 36  | 7  | 23  | 2   | 17  | 1   |   |                 | 459  |
| 8:15-8:30   | 27  | 9   | 112   | 2   | 15  | 0                                    | 2   | 0  | 102  | 4   | 8  | '<br>0   | 37  | 3   | 30   | ,<br>O  | 45  | 10   | 28  | 0   | 18  | 2   | 0   |                 | 457  |
| 8:30-8:45   | 32  | 3   | 118   | 0   | 14  | 0                                    | 1   | 0  | 96   | 5   | 15   | 0  | 37  | 0   | 41   | 3   | 41  | 7  | 25  | 1   | 15  | 2   | 2   | 1               | 459  |
| 8:45-9:00   | 33  | 5   | 119   | 2   | 25  | 0                                    | 1   | 0  | 99   | 5   | 9  | 0  | 41  | Ō   | 36   | 0   | 25  | 3  | 22  | Ö   | 19  | 0   |   |                 | 447  |
| Peak Hour   | 128   |   | 474   |   | 58  | -                                    | 3   |  | 452  |   | 36   |  | 139   |   | 140  |   | 164   |  | 122   | -   | 83  |   | 10  |                 | 1809   |
| Control Lange Control Control   | 121   | 22  | 385   | 8   | 46  | 2                                    | 2,2   | Ö  | 440  | 7   | 28   | 8827   | 142   |   | 118  | 5   | 145   | 22   | 119   | 2   | 66  | 2   |   | 2               | 1694   |
|   |   |   |   |   |   |                                      |   |  | ~********** <b>*</b> **  | -Cellencedial C                                     | ana ana ana ang ang ang ang ang ang ang                      | Note dataset.                                  | And the state of B  | - A Constantial School of                           | urrendendiarena.   | LO SOMORAN  | er e ciabata da esta esta esta esta esta esta esta est    | of the ball is a gran                          | ala's we share i 🖷 a  | , fillenter                               | na ( dan 163 ana a  | al halpopting a cor   |   | otronal dia war | 74.660 autority  |
| Study Peak Hour Truck %   |   | 15%                                       |   | 2%  |   | 4%                                   |   | 0%   |  | 2%  |  | 3%   |   | 1%  |  | 4%  |   | 13%  |   | 2%  |   | 3%  |   | 20%             |  |
|   |   |   |   |   | 0.741   | 11675                                |   |  |  |   | 0.841  |  |   |   |  |   | 0,807   | 83582  |   |   |   |   | 0.731   | 61765           | •  |
|   |   |   |   |   |   |                                      |   |  |  |   | PM PE4   | ۵ĸ   |   |   |  |   |   |  |   |   |   |   |   |                 |  |
|   |   |   |   |   |   |                                      |   |  |  |   |  | -11  |   |   |  |   |   |  |   |   |   |   |   |                 |  |
|   |   |   |   |   |   |                                      |   |  |  |   |  |  |   |   |  | _   |   |  |   |   |   |   |   |                 |  |
|   |   | -   | NE  |   |   | <u>т</u>                             |   | <del>-</del>                                   | SE   | 3   |  |  |   |   | Ē  |   |   |  |   |   | W   |   |   | +               | <b></b>  |
|   |   | Г<br>Т                                    | TH  |   | R   | T<br>T                               | L   | T  | TH   | 3   | RT   |  | L   | r<br>T  | T  |   | R   | T  |   | ·   | TI  |   | R   | T               | Total  |
| 4:00-4:15   | PC  | Т   | TH<br>PC  |   | PC  | Т                                    | PC  | Т  | TH<br>PC   | 3   | RT<br>PC   | г<br>Т   | PC  | T   | T<br>PC  | H<br>T  | PC  | Т  | PC  | т   | TI<br>PC  | H<br>T  | R<br>PC   | T               |  |
| 4:00-4:15   | PC<br>43  | T<br>6                                    | TH<br>PC<br>166   | 1<br>T<br>1                               | PC<br>16  | T<br>O                               |   | T<br>0   | TH<br>PC  <br>117  | B<br>I<br>T<br>4                                    | RT<br>PC  <br>40   |  | PC<br>27  | T<br>O  | T<br>PC<br>28  | H<br>T<br>0   | PC<br>54  | T<br>T<br>3                                    | PC 42   | Т<br>0                                    | TI<br>PC<br>47  |   |   | T<br>0          | 598  |
| 4:15-4:30   | PC<br>43<br>38  | T<br>6                                    | TH<br>PC<br>166<br>147  | H<br>T<br>1<br>2                          | PC<br>16<br>12  | Т                                    | PC 2  | Т  | TH<br>PC<br>117<br>144   | 3<br>T<br>4<br>3                                    | RT<br>PC  <br>40<br>34                                       | г<br>Т   | PC<br>27<br>22  | T<br>0<br>3   | PC<br>28<br>31   | H<br>T  | PC<br>54<br>37  | T<br>3   | PC<br>42<br>34  | T<br>0<br>1                               | PC<br>47<br>49  | H<br>T  |   | T               | 598<br>573   |
|   | PC<br>43<br>38<br>45                                      | T<br>6                                    | TH<br>PC<br>166   | 1<br>T<br>1                               | PC<br>16  | Т<br>0<br>0                          | PC  | T<br>0<br>0                                    | TH<br>PC<br>117<br>144<br>137  | B<br>I<br>T<br>4                                    | RT<br>PC 40<br>34<br>43                                      | г<br>Т   | PC<br>27<br>22<br>26                                      | T<br>O  | T<br>PC<br>28<br>31<br>29                                      | H<br>T<br>0   | PC<br>54<br>37<br>50                                      | T<br>3<br>1<br>4                               | PC<br>42<br>34<br>31  | T<br>0<br>1<br>0                          | PC<br>47<br>49<br>61  | H<br>T<br>0<br>1  |   | T<br>0          | 598<br>573<br>596  |
| 4:15-4:30<br>4:30-4:45  | PC<br>43<br>38  | T<br>6<br>6<br>3                          | TH<br>PC<br>166<br>147<br>140   | H<br>T<br>1<br>2<br>3                     | PC<br>16<br>12<br>14                                    | Т<br>0<br>0                          | PC<br>2<br>1<br>3   | T<br>0<br>0                                    | TH<br>PC<br>117<br>144   | B<br>T<br>4<br>3<br>2                               | RT<br>PC  <br>40<br>34                                       | г<br>Т   | PC<br>27<br>22  | T<br>0<br>3<br>0                                    | PC<br>28<br>31   | H<br>T<br>0<br>0<br>1                               | PC<br>54<br>37  | T<br>3   | PC<br>42<br>34  | T<br>0<br>1                               | PC<br>47<br>49  | H<br>T  |   | T<br>0          | 598<br>573<br>596<br>596                                     |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00   | PC<br>43<br>38<br>45<br>38                                | T<br>6<br>6<br>3<br>4                     | TH<br>PC<br>166<br>147<br>140<br>162                                    | H<br>T<br>1<br>2<br>3<br>1                | PC<br>16<br>12<br>14<br>17                              | T<br>0<br>0<br>0<br>1                | PC<br>2<br>1<br>3<br>6  | T<br>0<br>0<br>0                               | TH<br>PC<br>117<br>144<br>137<br>137   | B<br>T<br>4<br>3<br>2                               | RT<br>PC 40<br>34<br>43<br>37                                | г<br>Т   | PC<br>27<br>22<br>26<br>36                                | T<br>0<br>3<br>0<br>0                               | T<br>PC<br>28<br>31<br>29<br>22                                | H<br>T<br>0<br>0<br>1<br>0                          | PC<br>54<br>37<br>50<br>47                                | T<br>3<br>1<br>4<br>3                          | PC<br>42<br>34<br>31<br>26  | T<br>0<br>1<br>0                          | TI<br>PC<br>47<br>49<br>61<br>53                                | H<br>T<br>0<br>1<br>1<br>2                                    |   | T<br>0          | 598<br>573<br>596  |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45  | PC<br>43<br>38<br>45<br>38<br>37<br>45<br>59              | T<br>6<br>3<br>4<br>8                     | TH<br>PC<br>166<br>147<br>140<br>162<br>144                             | H<br>T<br>2<br>3<br>1<br>4<br>4<br>0      | PC<br>16<br>12<br>14<br>17<br>15                        | T<br>0<br>0<br>0<br>1<br>2           | PC<br>2<br>1<br>3<br>6  | T<br>0<br>0<br>0<br>0                          | TH<br>PC<br>117<br>144<br>137<br>137<br>122                                    | 3<br>T<br>4<br>3<br>2<br>2<br>2<br>1                | RT<br>PC<br>40<br>34<br>43<br>37<br>41                       | г<br>Т   | PC<br>27<br>22<br>26<br>36<br>19                          | T<br>0<br>3<br>0<br>0<br>0                          | T<br>PC<br>28<br>31<br>29<br>22<br>60                          | H<br>T<br>0<br>1<br>0<br>0                          | PC<br>54<br>37<br>50<br>47<br>61                          | T<br>3<br>1<br>4<br>3                          | PC<br>42<br>34<br>31<br>26<br>35                                      | T<br>0<br>1<br>0                          | TI<br>PC<br>47<br>49<br>61<br>53<br>77                          | H<br>T<br>0<br>1<br>1<br>2<br>3                               | PC<br>2<br>5<br>2<br>1                                    | T<br>0          | 598<br>573<br>596<br>596<br>639                              |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00                           | PC<br>43<br>38<br>45<br>38<br>37<br>45<br>59<br>63        | T<br>6<br>3<br>4<br>8<br>5                | TH<br>PC<br>166<br>147<br>140<br>162<br>144<br>144                      | 1<br>T<br>2<br>3<br>1<br>4<br>4           | PC<br>16<br>12<br>14<br>17<br>15<br>14                  | T<br>0<br>0<br>1<br>2<br>2           | PC<br>2<br>1<br>3<br>6<br>0                                     | T<br>0<br>0<br>0<br>0<br>0                     | TH<br>PC<br>117<br>144<br>137<br>137<br>122<br>128                             | 8<br>T<br>4<br>3<br>2<br>2<br>2<br>1<br>3           | RT<br>PC<br>40<br>34<br>43<br>37<br>41<br>44                 | г<br>Т   | PC<br>27<br>22<br>26<br>36<br>19<br>30                    | T<br>0<br>3<br>0<br>0<br>0                          | T<br>PC<br>28<br>31<br>29<br>22<br>60<br>32                    | H<br>T<br>0<br>1<br>0<br>0<br>0                     | PC<br>54<br>37<br>50<br>47<br>61<br>64                    | T<br>3<br>1<br>4<br>3<br>4<br>1                | PC<br>42<br>34<br>31<br>26<br>35<br>29                                | T<br>0<br>1<br>0<br>0<br>1<br>1           | TI<br>PC<br>47<br>49<br>61<br>53<br>77<br>66                    | H<br>T<br>0<br>1<br>1<br>2<br>3<br>1                          | PC<br>2<br>5<br>2<br>1                                    | T<br>0          | 598<br>573<br>596<br>596<br>639<br>615                       |
| 4:15-4:30<br>4:30-4:45<br>5:00-5:15<br>5:15-5:30<br>5:30-5:15<br>5:30-5:45<br>5:30-5:45<br>5:45-6:00<br>Peak Hour | PC<br>43<br>38<br>45<br>38<br>37<br>45<br>59<br>63<br>165 | T<br>6<br>3<br>4<br>8<br>5<br>4<br>4<br>4 | TH<br>PC<br>166<br>147<br>140<br>162<br>144<br>144<br>159<br>170<br>590 | H<br>T<br>2<br>3<br>1<br>4<br>4<br>0<br>3 | PC<br>16<br>12<br>14<br>17<br>15<br>14<br>9<br>11<br>60 | T<br>0<br>0<br>1<br>2<br>2<br>0<br>1 | PC<br>2<br>1<br>3<br>6<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>10 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TH<br>PC<br>117<br>144<br>137<br>137<br>122<br>128<br>124<br>124<br>119<br>524 | B<br>T<br>4<br>3<br>2<br>2<br>2<br>1<br>1<br>3<br>0 | RT<br>PC 40<br>34<br>43<br>37<br>41<br>44<br>42<br>39<br>165 | F<br>T<br>2<br>1<br>1<br>1<br>4<br>1<br>0<br>0 | PC<br>27<br>22<br>26<br>36<br>19<br>30<br>31              | T<br>0<br>3<br>0<br>0<br>0<br>0<br>0                | T<br>PC<br>28<br>31<br>29<br>22<br>60<br>32<br>18              | H<br>T<br>0<br>0<br>1<br>0<br>0<br>0<br>0           | PC<br>54<br>37<br>50<br>47<br>61<br>64<br>50<br>33<br>222 | T<br>3<br>1<br>4<br>3<br>4<br>1<br>4           | PC<br>42<br>34<br>31<br>26<br>35<br>29<br>35<br>29<br>35<br>28<br>121 | T<br>0<br>1<br>0<br>1<br>1<br>1<br>0<br>0 | TI<br>PC<br>47<br>49<br>61<br>53<br>77<br>66<br>56<br>37<br>257 | H<br>T<br>0<br>1<br>1<br>2<br>3<br>1<br>2<br>1<br>1<br>2<br>1 | PC<br>2<br>5<br>2<br>1<br>1<br>1<br>0<br>2<br>1<br>1<br>4 |                 | 598<br>573<br>596<br>596<br>639<br>615<br>597<br>566<br>2372 |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:345-6:00                          | PC<br>43<br>38<br>45<br>38<br>37<br>45<br>59<br>63        | T<br>6<br>3<br>4<br>8<br>5<br>4           | TH<br>PC<br>166<br>147<br>140<br>162<br>144<br>144<br>159<br>170        | H<br>T<br>2<br>3<br>1<br>4<br>4<br>0      | PC<br>16<br>12<br>14<br>17<br>15<br>14<br>9<br>11       | T<br>0<br>0<br>1<br>2<br>2<br>0<br>1 | PC<br>2<br>1<br>3<br>6<br>0<br>1<br>1<br>1                      | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TH<br>PC<br>117<br>144<br>137<br>137<br>122<br>128<br>124<br>124<br>119        | B<br>T<br>4<br>3<br>2<br>2<br>2<br>1<br>1<br>3<br>0 | RT<br>PC 40<br>34<br>43<br>37<br>41<br>44<br>42<br>39<br>165 | г<br>Т   | PC<br>27<br>22<br>26<br>36<br>19<br>30<br>31<br>19        | T<br>0<br>3<br>0<br>0<br>0<br>0<br>0<br>1<br>1<br>0 | T<br>PC<br>28<br>31<br>29<br>22<br>60<br>32<br>18<br>33        | H<br>T<br>0<br>1<br>0<br>0<br>0<br>0<br>0           | PC<br>54<br>37<br>50<br>47<br>61<br>64<br>50<br>33        | T<br>3<br>1<br>4<br>3<br>4<br>1<br>4           | PC<br>42<br>34<br>31<br>26<br>35<br>29<br>35<br>29<br>35<br>28<br>121 | T<br>0<br>1<br>0<br>0<br>1<br>1<br>1<br>0 | TI<br>PC<br>47<br>49<br>61<br>53<br>77<br>66<br>56<br>37<br>257 | H<br>T<br>0<br>1<br>1<br>2<br>3<br>1<br>2                     | PC<br>2<br>5<br>2<br>1<br>1<br>1<br>0<br>2<br>1<br>1<br>4 | T<br>0          | 598<br>573<br>596<br>596<br>639<br>615<br>597<br>566<br>2372 |
| 4:15-4:30<br>4:30-4:45<br>5:00-5:15<br>5:15-5:30<br>5:30-5:15<br>5:30-5:45<br>5:30-5:45<br>5:45-6:00<br>Peak Hour | PC<br>43<br>38<br>45<br>38<br>37<br>45<br>59<br>63<br>165 | T<br>6<br>3<br>4<br>8<br>5<br>4<br>4<br>4 | TH<br>PC<br>166<br>147<br>140<br>162<br>144<br>144<br>159<br>170<br>590 | H<br>T<br>2<br>3<br>1<br>4<br>4<br>0<br>3 | PC<br>16<br>12<br>14<br>17<br>15<br>14<br>9<br>11<br>60 | T<br>0<br>0<br>1<br>2<br>2<br>0<br>1 | PC<br>2<br>1<br>3<br>6<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>10 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TH<br>PC<br>117<br>144<br>137<br>137<br>122<br>128<br>124<br>124<br>119<br>524 | 3<br>T<br>4<br>3<br>2<br>2<br>2<br>1<br>3<br>0<br>0 | RT<br>PC 40<br>34<br>43<br>37<br>41<br>44<br>42<br>39<br>165 | F<br>T<br>2<br>1<br>1<br>1<br>4<br>1<br>0<br>0 | PC<br>27<br>22<br>26<br>36<br>19<br>30<br>31<br>19<br>111 | T<br>0<br>3<br>0<br>0<br>0<br>0<br>0<br>1<br>1<br>0 | T<br>PC<br>28<br>31<br>29<br>22<br>60<br>32<br>18<br>33<br>143 | H<br>T<br>0<br>0<br>1<br>0<br>0<br>0<br>0<br>0<br>0 | PC<br>54<br>37<br>50<br>47<br>61<br>64<br>50<br>33<br>222 | T<br>3<br>1<br>4<br>3<br>4<br>1<br>1<br>4<br>3 | PC<br>42<br>34<br>31<br>26<br>35<br>29<br>35<br>29<br>35<br>28<br>121 | T<br>0<br>1<br>0<br>1<br>1<br>1<br>0<br>0 | TI<br>PC<br>47<br>49<br>61<br>53<br>77<br>66<br>56<br>37<br>257 | H<br>T<br>0<br>1<br>1<br>2<br>3<br>1<br>2<br>1<br>1<br>2<br>1 | PC<br>2<br>5<br>2<br>1<br>1<br>1<br>0<br>2<br>1<br>1<br>4 |                 | 598<br>573<br>596<br>596<br>639<br>615<br>597<br>566<br>2372 |

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|-------------------------|----|----|-------------|----|-------|--------|----|-----|--------------------|----|-----------------------------------|-------|----|-----|----|---------|--------|-------|---------------|------|----|---------|----|-------|----------|
|                         |    |    |             |    | 0.733 | 309179 |    |     |                    |    | 0,848<br>PM PE                    |       |    |     |    |         | 0.7272 | 27273 |               |      |    |         |    | 0.75  |          |
|                         |    |    |             |    |       |        |    |     |                    |    | PMPE                              | AN    |    |     |    |         |        |       |               |      |    |         |    |       |          |
|                         |    |    | N           | B  | ~     |        |    |     | s                  | в  |                                   |       | r  |     |    | EB      | ·      |       | 1             |      | W  | /B      |    | T     | <u> </u> |
|                         |    | Т  |             | 'H |       | T      | L  | T   | Т                  | H  | R                                 | T     | L  | T   |    | TH      | RT     | •     | L             | .T   | Т  | H       | RT |       | Tota     |
|                         | PC | Ŧ  | PC          | Т  | PC    | Т      | PC | Т   | PC                 | Т  | PC                                | Т     | PC | T   | PC | Т       | PC     | Т     | PC            | Т    | PC | Т       | PC | Т     |          |
| 4:00-4:15               | 31 | 1  | 173         | 4  | 14    | 0      | 3  | 0   | 161                | 1  | 5                                 | 0     | 2  | 0   | 0  | 0       | 0      | 0     | 1             | 0    | 0  | 0       | 0  | 0     | 396      |
| 4:15-4:30               | 10 | 0  |             | 1  | 2     | 0      | 3  | 0   | 166                | 1  | 9                                 | 0     | 1  | 0   | 1  | 0       | 0      | 0     | 0             | 0    | 2  | 0       | 1  | 0     | 344      |
| 4:30-4:45               | 7  | 0  | 185         | 1  | 9     | 0      | 0  | 0   | 160                | 3  | 5                                 | 0     | 0  | 0   | 0  | 0       | 0      | 0     | 1             | 0    | 1  | 0       | 1  | 0     |          |
| 4:45-5:00               | 10 | 0  | 192         | 2  | 2     | 0      | 4  | 0   | 170                | 3  | 10                                | 0     | 1  | 0   | 2  | 0       | 0      | 0     | 2             | 0    | 1  | 0       | 1  | ō     |          |
| 5:00-5:15               | 7  | 0  | 188         | 1  | 2     | 0      | 2  | 0   | 213                | 3  | 18                                | 0     | 0  | 0   | 0  | 0       | 0      | 0     | 3             | 0    | 0  | 0       | 3  | Ō     |          |
| 5:15-5:30               | 13 | 0  | 170         | 1  | 2     | 0      | 2  | 1   | 171                | 3  | 6                                 | 0     | 3  | 0   | 0  | 0       | 2      | 0     | 1             | 0    | 0  | 0       | 1  | 0     |          |
| 5:30-5:45               | 20 | 2  | 188         | 1  | 6     | 0      | 2  | 1   | 133                | 3  | 34                                | 0     | 0  | 0   | 0  | 0       | 0      | 0     | 0             | 0    | 0  | 0       | 0  | 0     |          |
| 5:45-6:00               | 10 | 0  | 171         | 1  | 3     | 0      | 4  | 0   | 88                 | 2  | 5                                 | 0     | 0  | 0   | 7  | 0       | 2      | Ó     | 1             | Ū    | 0  | 0       | 0  | 0     |          |
| Peak Hour               | 50 |    | 738         |    | 12    |        | 10 |     | 687                |    | 68                                |       | 4  |     | 2  |         | 2      |       | 6             |      | 1  |         | 5  |       | 1585     |
| Study Peak Hour         | 50 | 2  | 717         | 4  | 13    | 2 · 0  | 10 | 2   | 605                | 11 | 63                                | 0     | 3  | 0   | 7  | 0       | 4      | 0     | 5             | 0    | 0  | 0       | 4  | i n   | 1500     |
| Study Peak Hour Truck % |    | 4% | 11110110110 | 1% |       | 0%     |    | 17% | renance particular | 2% | Contractor of the Second Concerns | 0%    |    | 0%  | A  | 0%      |        | 0%    | activitation. | 0%   |    | ####### |    | 0%    | 611.12   |
|                         |    |    |             | ·· |       | 0.906  |    |     |                    |    | 0.7319                            | 99153 |    |     |    |         | 0.3888 | 8889  |               |      |    |         |    | 0.375 | i .      |
|                         |    |    |             |    |       |        |    |     |                    |    |                                   |       |    |     |    |         |        |       |               |      |    |         |    |       |          |
|                         |    |    |             |    |       |        |    |     |                    |    |                                   |       |    |     |    |         |        |       |               |      |    |         |    |       |          |

NB TH WB TH T PC T SB TH EB TH LT PC LT RT LT RT RT T PC Total RT PC PC PC | PC PC T т PC PC PC PC Т T т Т 7:00-7:15 7:15-7:30 7:30-7:45 7:45-8:00 8:00-8:15 8:15-8:30 8:30-8:45 8:45-9:00 0 223 0 234 0 336 0 357 0 343 0 280 0 275 0 310 89 137 135 112 102 105 118 113 162 195 194 161 142 165 D C Ö 9 7 0 0 0 n Ō Ó з Ö Ó A B n Peak Hour Sludy Peak Hour Sludy Peak Hour Truck % \_\_\_\_19\_\_\_\_2 10% 564 10 12 0 2% 0% 9 0 468 16 6 0 0% 3% 0% 6 0 3 0 3 0 1150 0% 0% 0% 2 0 0 0 29 1 0% #D!V/0! 3%

City of Howell September, 2005 Counts

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Michigan and Livingston

AM PEAK

#### Michigan and Washington

#### City of Howell September 2005 Counts

AM PEAK

|   |  | NB   |  |  | 1   |                                      | SE  | 3  |  |     |  | E  | в  |  |                                      | 1   |                                      | W  | /B   |   |                                      |  | 1                            |
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|   | LT   | ТН   |  | RT   | Ľ   | Т                                    | Th  | 1  | RT   |     | LT   |  | н  |  | T                                    |   | T                                    | Т  | H  | R   | T                                    | Total  | 1                            |
|   | PC T   | PC   | Т  | PC T   | PC  | T                                    | PC  | T  | PC T   | PC  | <u> </u>   | PC   | <u> </u>                                       | PC   | Т                                    | PC  | Т                                    | PC   | Т  | PC  | T                                    |  | 1                            |
| 7:00-7:15   |  | 0 53   | 2  | 10 0   | ·   | 0                                    | 83  | 2  | 0  | 0   | · ·  |  |  |  | 0                                    | 1   | 0                                    | 1  | 0  | 0   | 0                                    | 167  | ]                            |
| 7:15-7:30   |  | 0 82   | 1  | 26 (   | ) 3   | 0                                    | 110   | 4  | 0  | 0   | / <u> </u>   | -  |  |  | 0                                    | 1   | 0                                    | 0  |  | 0   | 0                                    | 251  |                              |
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| 7:45-8:00   |  | 0 112  | 5  | 31 (   |   | 0                                    | 130   | 6  | 1  | 0   | 0  |  | 0  |  | 0                                    | 5   | 0                                    | 0  | 0  | 6   | 0                                    | 339  | 1068                         |
| 8:00-8:15   |  | D 96   | 3  | 32 0   |   | 0                                    | 125   | 6  | 2  | 0   | , U  |  | 0  | 3  | 0                                    | 2   | 0                                    | 1  | 0  | 2   | 0                                    | 303  | 1204                         |
| 8:15-8:30   |  | D 100  | 1  | 24 (   |   | 0                                    | 90  | 4  | 0  | 0   | 0  | 0  | 0  | 5  | 0                                    | 0   | 0                                    | 3  | 0  | 6   | 0                                    | 255  | 1208                         |
| 8:30-8:45   |  | J 96   | 5  | 29 (   |   | 0                                    | 92  | 3  | 2  | 0   | 0 0  | 0  | 0  | 4  | 0                                    | 3   | D                                    | 1  | 0  | 4   | 0                                    | 256  | 1153                         |
| 8:45-9:00   | 17   | J 115  | 4  | 29 (   | 15  | 0                                    | 87  | 4  | 3  | 0   | 0 0  | 3  | 0  | 6  | 0                                    | 2   | Ó                                    | 0  | 0  | 6   | 0                                    | 291  | 1105                         |
| Peak Hour   |  | J 416  | 13   | 119 0  | 29  | 0                                    | 468   | 27   | 3  | 0   |  |  | 0  | 23   | 0                                    |   | Ö                                    | 6  | 0  | 18  | 0                                    | 1208   | 1                            |
| Sludy Peak Hour   | 55   | 355  | 12   | 99 (   | 20  | Ö                                    | 446   | 23   | 强度 <b>的</b> 部领   | 0   | 0  | 3  | 0  | 30   | 0                                    | <b>9</b>                                    | 0                                    | 3  | 0  | 10  | 0                                    | 1068   | 997 SM                       |
| Study Peak Hour Truck %   | 0%   | 6  | 3%   | 0%   |   | 0%                                   |   | 5%   | C  | %   | 0%   | AND LANSING COLD   | 0%   | - Callery and a star                                       | 0%                                   | 222.629421.229                              | 0%                                   | Contractor State   | 0%   | 0.0000000000000000000000000000000000000     | 0%                                   | Allow Lowers   | 200120220                    |
|   |  |  |  | 0.75289017   |   |                                      |   |  | 0.83904  | 1   |  |  |  |  | 0.875                                |   |                                      |  |  |   | 0.5                                  | 1  |                              |
|   |  |  |  |  |   |                                      |   |  | PM PEAK  |     |  |  |  |  |                                      |   |                                      |  |  |   |                                      |  |                              |
|   |  |  |  |  |   |                                      |   |  |  |     |  |  |  |  |                                      |   |                                      |  |  |   |                                      |  |                              |
|   |  | NB   |  |  |   |                                      | SB  |  |  |     |  |  | в  |  |                                      |   |                                      | W  | в  |   |                                      | [  |                              |
|   | LT   | TH   |  | RT   | Lī  | г                                    | TH  |  | RT   |     | ĻT   | Т  | B<br>H   | R  | т                                    | L   | т                                    | T  |  | RT  | ſ                                    |  | ]                            |
|   | PC T   | TH<br>PC   | т  | PC T   | PC  | T                                    | TH<br>PC  | I<br>T   |  | PC  | T  | PC   | H<br>T   | R<br>PC  | T<br>T                               | PC  | T<br>T                               |  |  | RT<br>PC                                    | г<br>Т                               | Total  | ]                            |
|   | PC T<br>11 (   | PC 96  | T<br>2   | PC T<br>20 C   | PC 13   | T<br>0                               | TH<br>PC<br>159   | T<br>4   | RT   | 0   | T<br>0   | PC<br>0  | H<br>T   | PC<br>5  | T<br>T<br>0                          |   | T<br>T<br>0                          | T<br>PC<br>1   |  |   | г<br>Т<br>О                          | Total<br>327   |                              |
| 4:15-4:30   | PC T<br>11 (<br>24 (   | TH<br>PC<br>96<br>123  | 2  | PC T<br>20 C<br>29 C   | PC<br>13<br>11  | T<br>0<br>0                          | TH<br>PC<br>159<br>173  | T<br>4<br>2  | RT   | 0 0 | T<br>0<br>0  | PC<br>0  | H<br>T<br>0                                    | PC   | T<br>T<br>0                          | PC  | Т                                    | T  | H<br>T   | PC  | T<br>T<br>O                          |  |                              |
| 4:15-4:30<br>4:30-4:45  | PC T<br>11 (<br>24 (<br>10 (   | TH<br>PC<br>96<br>123<br>100   | 1<br>2<br>1<br>0                               | PC T<br>20 C<br>29 C<br>18 C   | PC<br>13<br>11<br>13  | T<br>0<br>0                          | TH<br>PC<br>159<br>173<br>143   | T<br>4<br>2<br>5                                     | RT<br>PC   T<br>7<br>1<br>1  | 0 0 | T<br>0<br>0  | PC<br>0<br>1   | H<br>T<br>0<br>0                               | PC<br>5<br>5<br>4  | T<br>T<br>0<br>0                     | PC<br>3<br>3                                | T<br>O                               | T<br>PC<br>1   | H<br>T<br>O                                    | PC  | T<br>T<br>O<br>O                     | 327  |                              |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00   | PC T<br>11 (<br>24 (<br>10 (<br>16 (   | TH           PC           96           123           100           150   | 2  | PC         T           20         0           29         0           18         0           37         0   | PC<br>13<br>11<br>13<br>23                                    | T<br>0<br>0<br>0                     | TH<br>PC<br>159<br>173<br>143<br>167                                    | T<br>4<br>2<br>5<br>4                                | RT<br>PC T<br>7<br>1<br>1<br>7                                     | 0 0 | T<br>0<br>0<br>0   | PC<br>0<br>1<br>0<br>3   | H<br>T<br>0<br>0<br>0                          | PC<br>5<br>5<br>4<br>5                                     | T<br>0<br>0                          | PC<br>3<br>3<br>5                           | T<br>0                               | T<br>PC<br>1<br>0  | H<br>T<br>O                                    | PC 5  | T<br>0<br>0<br>0                     | 327<br>377<br>305  | 1425                         |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15  | PC T<br>11 (<br>24 (<br>10 (<br>16 (<br>21 (   | TH           PC           96           123           100           150           107   | 1<br>2<br>1<br>0                               | PC T<br>20 C<br>29 C<br>18 C<br>37 C<br>22 C   | PC<br>13<br>11<br>13<br>23<br>16                              | T<br>0<br>0<br>0<br>0                | TH<br>PC<br>159<br>173<br>143<br>167<br>190                             | T<br>41<br>2<br>5<br>4<br>5                          | RT<br>PC   T<br>7<br>1<br>1  |     | T<br>0<br>0<br>0   | PC<br>0<br>1<br>0<br>3   | H<br>T<br>0<br>0                               | PC<br>5<br>5<br>4  | T<br>0<br>0                          | PC<br>3<br>3<br>5                           | T<br>0<br>0                          | T<br>PC<br>1<br>0  | H<br>T<br>0<br>0                               | PC<br>5<br>4<br>4                           | T<br>0<br>0<br>0                     | 327<br>377<br>305  | 1425                         |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30   | PC T<br>11 (<br>24 (<br>10 (<br>16 (<br>21 (<br>25 ()  | TH           PC           0         96           0         123           0         100           0         150           0         107           0         105   | 1<br>2<br>1<br>0                               | PC         T           20         0           29         0           18         0           37         0           22         0           21         0   | PC<br>13<br>11<br>13<br>23<br>16<br>17                        | T<br>0<br>0<br>0<br>0<br>0           | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145                      | T<br>4<br>2<br>5<br>4<br>5<br>6                      | RT<br>PC T<br>7<br>1<br>1<br>7                                     |     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0                               | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1                          | H<br>T<br>0<br>0<br>0                          | PC<br>5<br>4<br>5<br>2                                     | T<br>0<br>0<br>0                     | PC<br>3<br>3<br>5<br>1<br>5                 | T<br>0<br>0<br>0                     | T<br>PC<br>1<br>0  | H<br>T<br>0<br>0<br>0                          | PC<br>5<br>4<br>4<br>2                      | T<br>0<br>0<br>0<br>0                | 327<br>377<br>305<br>416                                     |                              |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45  | PC         T           11         0           24         0           10         0           16         0           21         0           25         0           17         0                                | TH           PC           96           123           100           150           107           105           105   | 2<br>1<br>0<br>0                               | PC         T           20         0           29         0           18         0           37         0           22         0           21         0   | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13                  | T<br>0<br>0<br>0<br>0                | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145<br>160               | T<br>41<br>2<br>5<br>4<br>5                          | RT<br>PC T<br>7<br>1<br>1<br>7                                     |     | T<br>0<br>0<br>0<br>0  | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1                          | H<br>T<br>0<br>0<br>0                          | PC<br>5<br>5<br>4<br>5<br>2<br>7                           | T<br>0<br>0<br>0<br>0                | PC<br>3<br>5<br>1<br>5<br>3                 | T<br>0<br>0<br>0<br>0                | T1<br>PC<br>1<br>0<br>1<br>1<br>1                          | H<br>T<br>0<br>0<br>0<br>0                     | PC<br>5<br>4<br>4<br>2<br>6                 |                                      | 327<br>377<br>305<br>416<br>379                              | 1477                         |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45  | PC T<br>11 (<br>24 (<br>10 (<br>16 (<br>21 (<br>25 (<br>17 (   | TH           PC           0         96           0         123           0         100           0         150           0         107           0         105   | 2<br>1<br>0<br>0                               | PC         T           20         0           29         0           18         0           37         0           22         0           21         0   | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13                  | T<br>0<br>0<br>0<br>0<br>0           | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145                      | T<br>4<br>2<br>5<br>4<br>5<br>6                      | RT<br>PC T<br>7<br>1<br>1<br>7                                     |     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0                          | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1<br>0                     | H<br>T<br>0<br>0<br>0<br>0                     | PC<br>5<br>4<br>5<br>2<br>7<br>2                           | T<br>0<br>0<br>0<br>0<br>0           | PC<br>3<br>5<br>1<br>5<br>3<br>0            | T<br>0<br>0<br>0<br>0                | T1<br>PC<br>1<br>0<br>1<br>1<br>1<br>1<br>1                | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0           | PC<br>5<br>4<br>4<br>2<br>6                 | T<br>0<br>0<br>0<br>0<br>0           | 327<br>377<br>305<br>416<br>379<br>340                       | <b>1477</b><br>1440          |
| 4:15-4:30<br>4:30-4:45<br>5:00-5:15<br>5:15-5:30<br>5:30-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00<br>Peak Hour       | PC         T           11         0           24         0           10         0           16         0           21         0           25         0           17         0                                | TH           PC           96           123           100           150           107           105           105   | 2<br>1<br>0<br>0                               | PC         T           20         0           29         0           18         0           37         0           22         0           21         0   | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13                  | T<br>0<br>0<br>0<br>0<br>0<br>0      | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145<br>160               | T<br>4<br>2<br>5<br>4<br>5<br>6                      | RT<br>PC   T<br>7<br>1<br>1<br>7<br>3<br>1<br>1<br>1<br>0<br>12    |     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1<br>0                     | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>5<br>4<br>5<br>2<br>7<br>7<br>2<br>2<br>2<br>16 | T<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>3<br>5<br>1<br>5<br>3<br>0            | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TI<br>PC<br>1<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>2<br>3 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>4<br>4<br>2<br>6                 | T<br>0<br>0<br>0<br>0<br>0           | 327<br>377<br>305<br>416<br>379<br>340<br>329                | 1477<br>1440<br>1464         |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00<br>Peak Hour<br>Study Peak Hour | PC         T           11         0           24         0           10         0           16         0           21         0           17         0           12         0           71         12        | TH           PC           96           0           123           100           150           150           107           105           105           105           105           117   | 2<br>1<br>0<br>0                               | PC         T           20         C           29         C           18         C           37         C           22         C           21         C           35         C                          | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13<br>9<br>63       | T<br>0<br>0<br>0<br>0<br>0<br>0      | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145<br>160<br>141        | T<br>4<br>2<br>5<br>4<br>5<br>6<br>3<br>1            | RT<br>PC T<br>7<br>1<br>7<br>3<br>1<br>1<br>1<br>0<br>12           |     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1<br>0<br>1<br>4           | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>5<br>4<br>5<br>2<br>7<br>2<br>2<br>16           | T<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>3<br>5<br>1<br>5<br>3<br>0<br>4<br>14 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TI<br>PC<br>1<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>2<br>3 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>4<br>2<br>6<br>5<br>4<br>1<br>16 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 327<br>377<br>305<br>416<br>379<br>340<br>329<br>326<br>1459 | 1477<br>1440<br>1464<br>1374 |
| 4:15-4:30<br>4:30-4:45<br>5:00-5:15<br>5:15-5:30<br>5:30-5:15<br>5:15-5:30<br>5:45-6:00<br>Peak Hour                    | PC         T           11         0           24         0           10         0           16         0           25         0           17         0           12         0           71         71        | TH           PC           0         96           0         123           0         100           0         150           0         105           0         105           0         105           0         117           480         434 | 1<br>2<br>1<br>0<br>0<br>1<br>3<br>1<br>1<br>1 | PC         T           20         C           29         C           18         C           37         C           22         C           21         C           35         C           106         C  | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13<br>9<br>63<br>55 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145<br>160<br>141<br>673 | T<br>4<br>2<br>5<br>4<br>5<br>6                      | RT<br>PC   T<br>7<br>1<br>1<br>7<br>3<br>1<br>1<br>1<br>0<br>12    |     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1<br>0<br>1<br>0<br>1<br>4 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | PC<br>5<br>5<br>4<br>5<br>2<br>7<br>7<br>2<br>2<br>2<br>16 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | PC<br>3<br>5<br>1<br>5<br>3<br>0<br>4<br>14 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TI<br>PC<br>1<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>2<br>3 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | PC 5<br>4<br>4<br>2<br>6<br>5<br>4<br>1     | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 327<br>377<br>305<br>416<br>379<br>340<br>329<br>326<br>1459 | 1477<br>1440<br>1464         |
| 4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00<br>Peak Hour<br>Study Peak Hour              | PC         T           11         ()           24         ()           10         ()           16         ()           21         ()           25         ()           12         ()           71         75 | TH           PC           0         96           0         123           0         100           0         150           0         105           0         105           0         105           0         117           480         434 | 1<br>1<br>0<br>0<br>1<br>3<br>1<br>1<br>1      | PC         T           20         C           29         C           18         C           37         C           21         C           21         C           35         C           106         99 | PC<br>13<br>11<br>13<br>23<br>16<br>17<br>13<br>9<br>63<br>55 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | TH<br>PC<br>159<br>173<br>143<br>167<br>190<br>145<br>160<br>141<br>673 | T<br>4<br>2<br>5<br>4<br>5<br>6<br>3<br>1<br>1<br>15 | RT<br>PC T<br>7<br>1<br>7<br>3<br>1<br>7<br>3<br>1<br>0<br>12<br>5 |     |  | T<br>PC<br>0<br>1<br>0<br>3<br>0<br>1<br>0<br>1<br>0<br>1<br>4 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>5<br>4<br>5<br>2<br>7<br>7<br>2<br>2<br>2<br>16 | T<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>3<br>5<br>1<br>5<br>3<br>0<br>4<br>14 | T<br>0<br>0<br>0<br>0<br>0<br>0      | TI<br>PC<br>1<br>0<br>1<br>1<br>1<br>1<br>1<br>1<br>2<br>3 | H<br>T<br>0<br>0<br>0<br>0<br>0<br>0<br>0      | PC<br>5<br>4<br>2<br>6<br>5<br>4<br>1<br>16 | T<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 327<br>377<br>305<br>416<br>379<br>340<br>329<br>326<br>1459 | 14<br>14<br>14<br>13         |

### Grand River and Court

# City of Howell September 2005 Counts

#### AM PEAK

|                         |   | N  | B                      |       |     | E  | В                               |       |                                  | N  | /B                                       | dit/d/-deals/science. |                     | 1              |
|-------------------------|---|----|------------------------|-------|-----|----|---------------------------------|-------|----------------------------------|----|--|-----------------------|---------------------|----------------|
|                         | L   | Т  | R                      | Т     | Т   | H  | R                               | ιT.   | L                                | Т  | Т  | Н                     |                     |                |
|                         | PC  | Т  | PC                     | Т     | PC  | Т  | PC                              | Т     | PC                               | Т  | PC                                       | Т                     | Total               |                |
| 7:00-7:15               | 0   | 0  | 18                     | 0     | 96  | 1  | 1                               | 0     | 10                               | 0  | 89                                       | 6                     | 221                 |                |
| 7:15-7:30               | 0   | 0  | 5                      | 0     | 139 | 8  | 2                               | 0     | 5                                | 0  | 173                                      | 5                     | 337                 |                |
| 7:30-7:45               | 1   | 0  | 20                     | 0     | 138 | 3  | 1                               | 0     | 9                                | 0  | 104                                      | 10                    | 286                 | 1              |
| 7:45-8:00               | 0   | 0  | 18                     | 0     | 141 | 5  | 4                               | 0     | 10                               | 0  | 101                                      | 5                     | 284                 | 1128           |
| 8:00-8:15               | 0   | 0  | 10                     | 0     | 123 | 3  | 1                               | 0     | 16                               | 0  | 96                                       | 8                     | 257                 | 1164           |
| 8:15-8:30               | 0   | Ö  | 13                     | 1     | 104 | 5  | 2                               | 0     | 6                                | 0  | 97                                       | 15                    | 243                 | 1070           |
| 8:30-8:45               | 0   | 0  | 14                     | 0     | 145 | 5  | 2                               | 0     | 15                               | 0  | 130                                      | 6                     | 317                 | 1101           |
| 8:45-9:00               | 1   | 0  | 16                     | 0     | 170 | 5  | 0                               | 0     | 7                                | 0  | 120                                      | 11                    | 330                 | 1147           |
| Peak Hour               | 1   |    | 53                     |       | 541 |    | 8                               |       | 40                               |    | 474                                      |                       | 1117                |                |
| Study Peak Hour         | 1   | 0  | 61                     | 0     | 514 | 17 |                                 | 0     | 34                               | 0  | 467                                      | 26                    | 1128                |                |
| Study Peak Hour Truck % |   | 0% | and the ansatz distant | 0%    |     | 3% | ana tan di kuruk (gel del talit | 0%    | - 1999 Average (2004), 965 Avera | 0% | unterstanden bei der der der             | 5%                    | 2109-2203 2203 2003 | anationelesses |
|                         | kunaa aa ahaa ahaa ahaa ahaa ahaa ahaa ah |    |                        | 0.738 |     |    |                                 | 0.898 |                                  |    | 2020/00/00/00/00/00/00/00/00/00/00/00/00 | 0.72                  |                     |                |

PM PEAK

|                         |    | N  | IB |       |     | Е    | В                              |       |      | W  | /B  |       |               |      |
|-------------------------|----|----|----|-------|-----|------|--------------------------------|-------|------|----|---|-------|---------------|------|
|                         | L  | Т  | R  | Т     | Т   | Ή    | R                              | Т     | L    | Т  | Т   | Н     |               |      |
|                         | PC | Т  | PC | Т     | PC  | Т    | PC                             | Т     | PC   | Т  | PC  | Т     | Total         |      |
| 4:00-4:15               | 1  | 0  | 9  | 0     | 200 | 7    | 5                              | 0     | 23   | 0  | 170   | 8     | 423           |      |
| 4:15-4:30               | 1  | 0  | 12 | 0     | 166 | 3    | 0                              | 0     | 27   | 0  | 155   | 8     | 372           |      |
| 4:30-4:45               | 1  | 0  | 16 | 0     | 183 | 4    | 4                              | 0     | 30   | 0  | 185   | 12    | 435           |      |
| 4:45-5:00               | 0  | 0  | 6  | 1     | 215 | 2    | 4                              | 0     | 18   | 0  | 200   | 10    | 456           | 1686 |
| 5:00-5:15               | 1  | 0  | 14 | 0     | 176 | 2    | 6                              | 1     | 28   | 0  | 195   | 3     | 426           | 1689 |
| 5:15-5:30               | 0  | 0  | 6  | 0     | 212 | 4    | 7                              | 0     | 37   | 0  | 197   | 1     | 464           | 1781 |
| 5:30-5:45               | 2  | 0  | 13 | 0     | 167 | 11   | 7                              | 0     | 19   | 0  | 195   | 1     | 415           | 1761 |
| 5:45-6:00               | 0  | 0  | 14 | 0     | 178 | 1    | 3                              | 0     | 20   | 0  | 180   | 0     | 396           | 1701 |
| Peak Hour               | 2  |    | 42 |       | 786 |      | 21                             |       | 113  |    | 777   |       | 1741          |      |
| Study Peak Hour         | 3  | 0  | 47 | 0     | 733 | . 18 | 23                             | 1     | 104  | 0  | 767   | 5     | 1701          |      |
| Study Peak Hour Truck % |    | 0% |    | 0%    |     | 2%   | n tana yang dika 2003 yang dik | 4%    | anan | 0% | na entre superior de la constante de la constan<br>Constante de la constante de la<br>Constante de la constante de la | 1%    | waradzidzieli |      |
| •                       |    |    |    | 0.833 |     |      |                                | 0.869 |      |    |   | 0.932 |               |      |

Y:\200408\20040841\Design\ProjectData\Traffic\Synchro\transfer\March2007\ssheets\CityProvided\_TrafCounts\_Truck. xis GR\_Court

#### Grand River and Barnard

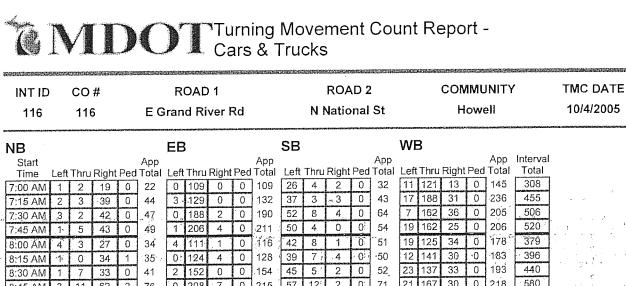
| N<br>PC<br>0 0<br>0 0<br>0 1<br>0 1<br>0 0<br>0 1<br>0 1<br>0 1<br>0 1<br>0 2  | LT<br>PC T<br>2 0<br>0 0<br>1 0<br>1 0<br>1 0<br>0 0<br>1 0<br>1 0<br>1  | 0 0<br>0 0<br>1 0<br>0 0<br>1 0<br>1 0<br>1 0  | 2 0<br>9 0<br>9 0<br>12 0   | 0 1<br>0 3<br>0 2                | SE<br>TF<br>0 1<br>0 0 |                             | τ<br>T<br>O                         | AM PEAM  | г рс   | ЕВ<br>ГН  <br>  Т                                     | RT<br>PC T   | PC   | LT<br>T  | WE<br>TH<br>PC   |  | RT<br>PC 1  | Total  |
|--|--|--|---|----------------------------------|------------------------|-----------------------------|-------------------------------------|--|--|---|--|--|--|--|--|---|--|
| T           PC           0           0           0           0           0           1           0           1           0           1           0           1           0   | PC         T           2         0           0         0           0         0           1         0           0         0 | TH           PC         T           0         0           0         0           1         0           1         0           1         0           1         0           1         0          | PC         T           6         0           2         0           9         0           9         0           12         0 | PC 1<br>0 7<br>0 1<br>0 3<br>0 2 | T PC<br>0 1<br>0 0     | I F<br>T PC<br>0 3          | T<br>O                              |  | г рс   | тн  |  |  | .T   | TH   |  |   | Total  |
| PC           0         0           0         0           0         1           0         0           0         1           0         1           0         1           0         1           0         1           0         2 | PC         T           2         0           0         0           0         0           1         0           0         0 | PC         T           0         0           0         0           1         0           0         0           1         0           1         0           1         0           1         0 | PC         T           6         0           2         0           9         0           9         0           12         0 | PC 1<br>0 7<br>0 1<br>0 3<br>0 2 | T PC<br>0 1<br>0 0     | T PC<br>0 3                 | T<br>O                              |  | г рс   |   |  |  | T  |  | -  |   | Total  |
| 0 0<br>0 0<br>0 1<br>0 0<br>0 1<br>0 1<br>0 1<br>0 1<br>0 2  | 2 0<br>0 0<br>0 0<br>1 0<br>1 0<br>1 0<br>0 0  | 0 0<br>0 0<br>1 0<br>0 0<br>1 0<br>1 0<br>1 0  | 6 0<br>2 0<br>9 0<br>9 0<br>12 0  | 0 7<br>0 1<br>0 3<br>0 2         | 0 1                    | 0 3                         |                                     | PC 1   |  | T   | PC T   | PC   | T  | DO   | 7 1  | DC 7  |  |
| 0 0<br>0 1<br>0 0<br>0 1<br>0 1<br>0 1<br>0 1<br>0 2   | 0 0<br>0 0<br>1 0<br>1 0<br>0 0  | 0 0<br>1 0<br>0 0<br>1 0<br>1 0<br>1 0   | 2 0<br>9 0<br>9 0<br>12 0   | 0 1<br>0 3<br>0 2                | 0 0                    |                             |                                     | 1  | 01 07  |   |  |  | 1  | PU   |  | PC I I  |  |
| 0 1<br>0 0<br>0 1<br>0 1<br>0 1<br>0 2   | 0 0<br>1 0<br>1 0<br>0 0   | 1 0<br>0 0<br>1 0<br>1 0   | 9 (<br>9 (<br>12 (  | 0 3                              |                        | 0 1                         |                                     |  | 0 95   | 7   | 4  | 0 10   | 0  | 120  | 7  | 0   | 0 263  |
| D 0<br>D 1<br>D 1<br>D 1<br>D 2  | 1 0<br>1 0<br>0 0  | 0 0<br>1 0<br>1 0  | 9 (<br>12 (   | 2                                | 0 1                    |                             | 0                                   | 2  | 0 136  | 7   | 1  | 0 7  | 0  | 200  | 7  | 0   | 0 364  |
| D 1<br>D 1<br>D 2  | 1 0  | 1 0  | 12 0  |                                  |                        | 0 4                         | 0                                   | 1  | 0 153  | 3   | 4  | 0 14   | 0  | 112  | 10   | 1   | 0 316  |
| 0 1<br>0 2   | 0 0  | 1 0  |   |                                  | 0 1                    | 0 2                         | 0                                   | 1  | 0 166  | 12  | 4  | 0 10   | 0  | 110  | 6  | 0   | 0 324  |
| 5 2  |  |  | 12 1  | ) 1                              | 0 1                    | 0 2                         | 0                                   | 1  | 0 114  |   | 4  | 0 9  | 0  | 115  | 5  | 0   | 0 270  |
|  |  |  |   | 5                                | 0 3                    | 0 2                         | 0                                   | 1  | 0 107  | 6   | 4  | 0 8  | 0  | 95   | 9  | 0   | 0 254  |
| ) 1  | 1 1 0  | 2 U  |   | 3                                | 0 1                    | 0 3                         | 0                                   | 3  | 0 135  | 3   | 2  | 0 4  | 0  | 105  | 5  | 3   | 0 283  |
|  | 1 0  | 1 0  | 15 0  | 2                                | 0 0                    | 0 3                         | 0                                   | 0  | 0 162  | 8   | 4  | 0 7  | 0  | 130  | 5  | 0   | 0 338  |
| 2  | 2  | 2  | 32  | 7                                | 3                      | 9                           |                                     | 5  | 569  |   | 13   | 40   |  | 537  |  | 1   | 1220   |
| ) 1  | 3 0  | 1 0  | 26  | 13                               | 0 3                    | 0 10                        | 0                                   | 5  | 0 . 550  | 29  | 13   | 0 41   | 0  | 542  | 30   | . 1   | 0 1267   |
| i.   | 0%   | 0%   | 0%  |                                  | 0%                     | 0%                          | 0%                                  |  | 0%   | 5%  | C  | 0%   | 0%   |  | 5%   | C   | %  |
|  |  |  | 0.75  | i                                |                        | 0.590                       | 90909                               |  |  |   | 0.815573   | 77   |  |  |  | 0.717289  | 12   |
|  |  |  |   |                                  |                        | PM PE                       | EAK                                 |  |  |   |  |  |  |  |  |   |  |
|  |  | NB   |   |                                  | SB                     |                             |                                     |  |  | ЕB  |  |  |  | WE   | l  |   |  |
|  | LT   | TH   | RT  | LT                               | TH                     |                             | RT .                                | LT   |  | ГН  | RT   |  | .T   | ŤΗ   |  | RT  | Total  |
| PC   | PC T   | PC T   | PC T  | PC T                             | r PC                   | T PC                        | Т                                   | PC   | PC   | Т   | PC T   | PC   | Т  | PC   | Т  | PC T  |  |
|  | 1 0  | 2 0  |   |                                  | 0 0                    | 0 4                         | 0                                   | 8  | 0 203  | 7   | 4  | 0 12   |  | 226  | 5  | 1   | 0 485  |
|  | 3 0  | 1  | 13 0  |                                  | 0 4                    | 0 7                         | 0                                   | 4  | 0 187  | 3   | 2  | 0 17   | 0  | 186  | 10   | 3   | 0 440  |
|  | 1 0  | 2 0  |   |                                  | 0 0                    | 0 4                         |                                     | 2  | 0 169  | 1   | 1  | 0 11   | 0  | 192  | 19   | 6   | 0 419  |
|  | 1 0  | 1 0  |   | 2                                | 0 1                    | 0 9                         |                                     | 6  | 0 161  | 4   | 2  | 0 16   | 0  | 190  | 10   | 6   | 0 418  |
| ) 1  | 1 0  | 1 0  | 16 0  |                                  | 0 1                    | 0 5                         |                                     | 4  | 0 184  | 7   | 3  | 0 11   |  | 225  | 4  | 4   | 0 470  |
| D 1<br>D 1   |  | 1 0  | 9 0   | 3                                | 0 1                    | 0 3                         | 0                                   | 4  | 0 166  |   | 1  | 0 15   |  | 180  | 2  | 2   | 0 390  |
| D 1<br>D 1   | 0 0  | 1 0  |   |                                  | 0 0                    | 0 4                         | 0                                   | 8  | 0 170  |   | 6  | 0 6  |  | 200  | 2  | 4   | 0 419  |
| D 1<br>D 1<br>D 1<br>D 1   |  | 7 0  | 20 0  | 1                                | 0 0                    | 0 8                         | 0                                   | 16   | 0 160  | 3   | 3  | 0 6  | 0  | 105  | 0  | 3   | 0 333  |
| D 1<br>D 1<br>D 1<br>D 1   |  |  | 41  | 6                                | 5                      | 24                          |                                     | 20   | 720  |   | 9  | 56   |  | 794  |  | 16  | 1703   |
| D 1<br>D 1<br>D 1<br>D 1   | 1 0<br>1 0<br>6  | 6  | CONTRACTOR OF THE OWNER OF THE  | 9                                | 0 2                    | 0 20                        | 0                                   | 32   | 0 680  | 16  | 13   | 0 38   |  | 710  | 8  | - 13  | 0 1612   |
| 0 1<br>0 1<br>0 1<br>0 1<br>0 1<br>0 7<br>6  | 1 0<br>1 0   |  |   | 1                                | 196                    | 0%                          | 0%                                  |  | DPL  | 20/   | 0  | A 1  | 094  |  | 1%   | C   | %  |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 1 0<br>1 0<br>6  |  |   | 1 .                              |                        | 0.00                        |                                     |  | 1 /0   | 2%  | 0  | 1%5  | 0.70   |  |  |   |  |
|  | 1 0  |  | 6   | 6 41<br>10 0 58 0                | 6 41 6<br>10 0 58 0 9  | 6 41 6 5<br>10 0 58 0 9 0 2 | 6 41 6 5 24<br>10 0 58 0 9 0 2 0 20 | 6         41         6         5         24           10         0         58         0         9         0         2         0         20         0 | 6         41         6         5         24         20           10         0         58         0         9         0         2         0         20         0         32 | 6 41 6 5 24 20 720<br>10 0 58 0 9 0 2 0 20 0 32 0 680 | 6         41         6         5         24         20         720           10         0         58         0         9         0         2         0         0         32         0         680         16 | 6         41         6         5         24         20         720         9           10         0         58         0         9         0         2         0         20         32         0         680         16         13 | 6         41         6         5         24         20         720         9         56           10         0         58         0         9         0         2         0         20         32         0         680         16         13         0         38 | 6         41         6         5         24         20         720         9         56           10         0         58         0         9         0         2         0         20         32         0         680         16         13         0         36         0 | 6         41         6         5         24         20         720         9         56         794           10         0         58         0         9         0         2         0         20         32         0         680         16         13         0         36         0         710 | 6         41         6         5         24         20         720         9         56         794           10         0         58         0         9         0         2         0         0         32         0         680         16         13         0         38         0         710         8 | 6         41         6         5         24         20         720         9         56         794         16           10         0         58         0         9         2         0         20         0         32         0         680         16         13         0         38         0         710         8         13 |

# City of Howell September 2005 Counts

# Grand River and Fowler

AM PEAK

|  |                                 | N                          | B  |                                 |  | E                               | B                                    |                            |  | N                          | /B   |                                    |
|--|---------------------------------|----------------------------|--|---------------------------------|--|---------------------------------|--------------------------------------|----------------------------|--|----------------------------|--|------------------------------------|
|  | L                               | Т                          | R  |                                 | T  | H                               | R                                    | Т                          | LT   |                            | TH   |                                    |
|  | PC                              | Т                          | PC   | Т                               | PC   | Т                               | PC                                   | Т                          | PC   | Т                          | PC   | Т                                  |
| 7:00-7:15  | 1                               | 0                          | 16   | 0                               | 114  | 1                               | 1                                    | 0                          | 9  | 0                          | 111  | 6                                  |
| 7:15-7:30  | 1                               | 0                          | 20   | 1                               | 145  | 9                               | 7                                    | 0                          | 21   | 1                          | 190  | 7                                  |
| 7:30-7:45  | 3                               | 0                          | 26   | 0                               | 143  | 4                               | 7                                    | 0                          | 27   | 0                          | 95   | 8                                  |
| 7:45-8:00  | 1                               | 0                          | 41   | 0                               | 166  | 7                               | 4                                    | 0                          | 31   | 2                          | 125  | 4                                  |
| 8:00-8:15  | 1                               | 0                          | 27   | 1                               | 141  | 3                               | 4                                    | 0                          | 20   | 0                          | 103  | 7                                  |
| 8:15-8:30  | 0                               | 0                          | 25   | 1                               | 131  | 6                               | 1                                    | 0                          | 15   | 0                          | 110  | 18                                 |
| 8:30-8:45  | 1                               | 0                          | 25   | 1                               | 160  | 5                               | 4                                    | 0                          | 25   | 0                          | 122  | 5                                  |
| 8:45-9:00  | 6                               | 0                          | 39   | 4                               | 157  | 8                               | 16                                   | 0                          | 29   | 2                          | 126  | 12                                 |
| Peak Hour  | 6                               |                            | 114  |                                 | 595  |                                 | 22                                   |                            | 99   |                            | 513  |                                    |
| Study Peak Hour  | 6                               | 0                          | 103  | 1                               | 568  | 21                              | 19                                   | 0                          | 88   | 3                          | 521  | 25                                 |
| Study Peak Hour Truck %  |                                 | 0%                         |  | 1%                              |  | 4%                              |                                      | 0%                         |  | 3%                         |  | 5%                                 |
|  |                                 |                            |  | 0.655                           |  |                                 |                                      | 0.859                      |  |                            |  | 0.727                              |
|  |                                 |                            |  |                                 |  | ]                               | PM PE/                               | ٩K                         |  |                            |  |                                    |
|  |                                 | NI                         | 3  | 1                               |  | EE                              | 3                                    | l                          |  | w                          | B  | 1                                  |
|  | L.                              | r I                        | R  | Г                               | Tł   | 4                               | R                                    | Г                          | LT   |                            | TH   |                                    |
|  | PC                              | T                          | PC   | Т                               |  |                                 | -                                    |                            |  |                            |  | 1                                  |
| 4:00-4:15  | 4                               |                            |  | 1                               | PC   | Т                               | PC                                   | Т                          | PC   | T                          | PC   | т                                  |
|  | 1                               | 0                          | 29   | 2                               | PC<br>192  | <b>T</b>                        | PC 2                                 | <u>т</u><br>0              | PC<br>32                                     | <u> </u>                   | PC<br>184  | <u>т</u><br>9                      |
| 4:15-4:30  | 1<br>2                          | 0<br>0                     |  |                                 |  |                                 |                                      |                            |  |                            |  |                                    |
|  | 1<br>2<br>1                     |                            | 29   | 2                               | 192  | 7                               | 2                                    | 0                          | 32   |                            | 184  | 9                                  |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00  |                                 | 0                          | 29<br>40                                     | 2<br>0                          | 192<br>180   | 7                               | 2<br>5                               | 0                          | 32<br>25                                     | 1                          | 184<br>195   | 9<br>10                            |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15   | 1                               | 0                          | 29<br>40<br>41                               | 2<br>0<br>1                     | 192<br>180<br>208                                    | 7<br>3<br>5                     | 2<br>5<br>3                          | 0<br>0<br>0                | 32<br>25<br>32                               | 1                          | 184<br>195<br>201                                    | 9<br>10<br>14                      |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00  | 1<br>2                          | 0<br>0<br>0                | 29<br>40<br>41<br>41                         | 2<br>0<br>1<br>0                | 192<br>180<br>208<br>222                             | 7<br>3<br>5<br>3                | 2<br>5<br>3<br>1                     | 0<br>0<br>0                | 32<br>25<br>32<br>47                         | 1<br>1<br>1                | 184<br>195<br>201<br>178                             | 9<br>10<br>14<br>11<br>3           |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45                           | 1<br>2<br>1<br>3<br>2           | 0<br>0<br>0                | 29<br>40<br>41<br>41<br>38<br>40<br>27       | 2<br>0<br>1<br>0<br>0<br>0<br>0 | 192<br>180<br>208<br>222<br>200                      | 7<br>3<br>5<br>3<br>5           | 2<br>5<br>3<br>1<br>3                | 0<br>0<br>0<br>0           | 32<br>25<br>32<br>47<br>39                   | 1<br>1<br>1<br>1<br>0      | 184<br>195<br>201<br>178<br>185                      | 9<br>10<br>14<br>11                |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00              | 1<br>2<br>1<br>3                | 0<br>0<br>0<br>0           | 29<br>40<br>41<br>41<br>38<br>40             | 2<br>0<br>1<br>0<br>0<br>0      | 192<br>180<br>208<br>222<br>200<br>212               | 7<br>3<br>5<br>3<br>5<br>4      | 2<br>5<br>3<br>1<br>3<br>4           | 0<br>0<br>0<br>0<br>0      | 32<br>25<br>32<br>47<br>39<br>43             | 1<br>1<br>1<br>0<br>0      | 184<br>195<br>201<br>178<br>185<br>198               | 9<br>10<br>14<br>11<br>3<br>2      |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00<br>Peak Hour | 1<br>2<br>1<br>3<br>2<br>1<br>7 | 0<br>0<br>0<br>0<br>0<br>0 | 29<br>40<br>41<br>41<br>38<br>40<br>27       | 2<br>0<br>1<br>0<br>0<br>0<br>0 | 192<br>180<br>208<br>222<br>200<br>212<br>201        | 7<br>3<br>5<br>3<br>5<br>4<br>2 | 2<br>5<br>3<br>1<br>3<br>4<br>2      | 0<br>0<br>0<br>0<br>0<br>0 | 32<br>25<br>32<br>47<br>39<br>43<br>32       | 1<br>1<br>1<br>0<br>0<br>0 | 184<br>195<br>201<br>178<br>185<br>198<br>200        | 9<br>10<br>14<br>11<br>3<br>2<br>3 |
| 4:15-4:30<br>4:30-4:45<br>4:45-5:00<br>5:00-5:15<br>5:15-5:30<br>5:30-5:45<br>5:45-6:00              | 1<br>2<br>1<br>3<br>2<br>1      | 0<br>0<br>0<br>0<br>0<br>0 | 29<br>40<br>41<br>41<br>38<br>40<br>27<br>33 | 2<br>0<br>1<br>0<br>0<br>0<br>0 | 192<br>180<br>208<br>222<br>200<br>212<br>201<br>200 | 7<br>3<br>5<br>3<br>5<br>4<br>2 | 2<br>5<br>3<br>1<br>3<br>4<br>2<br>6 | 0<br>0<br>0<br>0<br>0<br>0 | 32<br>25<br>32<br>47<br>39<br>43<br>32<br>37 | 1<br>1<br>1<br>0<br>0<br>0 | 184<br>195<br>201<br>178<br>185<br>198<br>200<br>155 | 9<br>10<br>14<br>11<br>3<br>2<br>3 |



|       | 1.00 MINI       | 1 1      |          | 10       | 1 4 | 1 44 | 1.0      | 100       | <u> </u> |   | 1100 |          |                 |          | Lunning        |      | harmon  | -             |                 |    |      |       | and the second se |
|-------|-----------------|----------|----------|----------|-----|------|----------|-----------|----------|---|------|----------|-----------------|----------|----------------|------|---|---------------|-----------------|----|------|-------|---|
|       | 7:15 AM         | 2        | 3        | -39      | 0   | 44   | 3 -      | .129      | 0        | 0 | 132  | 37       | 3               | 3        | 0              | 43   | 17  | 188           | 31              | 0  | 236  | 455   | a second de la companya de  |
|       | 7:30 AM         | 3        | 2        | 42.      | 0   | 47   | 0        | 188       | 2        | 0 | 190  | 52       | 8               | 4        | 0              | 64   | (mannan)                                      | 162           | 36              | 0  | 205  | 50,6  | and the second second   |
|       | 7:45 AM         | 1        | 5        | 43       | 0   | 49   | 1        | 206       | 4        | 0 | 211  | 50       | 4               | 0.       | 0              | 54   | 19  | 162           | 25              | 0  | 206  | 520   | and a second  |
|       | 8:00 ÅM         | 4        | 3        | 27       | 0   | 34   | 4        | 111       | . 1      | 0 | 116  | 42       | 8               | 1        | 0              | 51   | 19  | 125           | 34              | 0  | 178  | 379   |   |
| مەسىي | 8:15 AM         | 11:      | 0        | 34       | 1   | 35   | 0 :      | 124       | 4        | 0 | 128  | 39       | 77              | . 4      | 0              | ·50  | 12  | 141           | -30             | ٠O | 183  | 396   |   |
|       | 8:30 AM         | 1        | 7        | 33       | 0   | 41   | 2        | 152       | 0        | 0 | .154 | 45       | 5               | 2        | 0              | 52_  | 23  | 137           | 33              | 0  | 193  | 440   |   |
|       | 8:45 AM         | 3        | 11       | 62       | 2   | 76   | 0        | 208       | 7        | 0 | 215  | 57       | 12 <sup>:</sup> | 2        | 0 <sup>.</sup> | 71   | 21  | 167           | 30              | 0  | 218  | 580   | and a second s  |
|       | 11:00 AM        | 4        | 11       | 30       | Ó   | 45   | 4        | 196       | 4        | 0 | 204  | 47       | 11              | 5        | 0              | 63   | 19  | 167           | 34              | 0  | 220  | 532   |   |
| •     | 11:15 AM        | 4        | 7        | 37       | 0   | 48   | 3        | 182       | 5        | 0 | 190  | 40       | 14              | 11       | 0              | 65   | 15  | 176           | 44              | 0  | 235  | -538  |   |
|       | 11:30 AM        | 6        | . 7      | 38       | 0   | 51   | 0        | 1,96      | . 8.     | 0 | 204  | 48       | 4               | 4        | 0              | 56   | 15  | 172           | 41              | 1  | 228  | 539   | na an a  |
|       | 11:45 AM        | 4        | 3        | 57       | 0   | 64   | 3        | 187       | 6        | 1 | 196  | 66       | 13              | 4        | 1              | 83   | 28  | 191           | 54              | 1  | 273  | 616   |   |
|       | 12:00 PM        | 8        | 13       | 57       | 0   | 78   | 2        | 239       | 2        | 0 | 243  | 71       | 14              | 8        | 0              | 93   | 25  | 208           | 62              | 1  | 295  | 709   | a and a star was a set of the   |
| ····  | 12:15 PM        | 12       | 5        | 35       | 0   | - 52 | 6        | 213       | 6        | 1 | 225  | 58       | 13              | 1.       | 0.             | 72   | -   | 209           | 55              | 1  | 285  | 634   | a second s |
|       | 12:30 PM        | 12       | 6        | 53,      | 0   | 71   | 1        | 189       | 5        | 0 | 195  | 59       | 11              | 8        | 0              | 78   | annam   | 221           | 57              | 0  | 297  | 641   |   |
|       | 12:45 PM        | 13       | 10       | 46       | 0   | 69   | 1        | 178       | 7        | 1 | 186  | 55       | 15              | 8        | 0              | 78   | 000007876                                     | 222           | 50              | 0  | 291  | 624   |   |
|       | 4:00 PM         | 10       | 14       | 40       | 0   | 64   | 4        | 229       | 4        | 0 | 237  | 58       | 12              | 10       | 1              | 80   | 21  | 210           | 77              | 1  | 308  | 689   |   |
|       | 4:15 PM         | 4        | 13       | 50       | 2   | 67   | 5        | 182       | 6        | 0 | 193  | 45       | 13              | 7        | 0              | 65   | answere S                                     | 220           | ******          | 0  | 307  | 632   |   |
|       | 4:30 PM         | 5        | 13       | 43       | 4   | 61   | 4        | 206       | 1        | 1 | 211  | 72       | 18              | 12       | 0              | 102  | Samones                                       | 209           | ****            | 0  | 303  | 677   |   |
|       | 4:45 PM         | 5        | 6        | 51       | 2   | 62   | 2        | 197       | 5        | 0 | 204  | 71       | 18              | 9        | 0              | 98   | and the second second                         | 234           | CARLE COMPANY   | 0  | 353  | 717   |   |
|       | 5:00 PM         | 12       | 18       | 39       | 0   | 69   | 2        | 214       | 3        | 2 | 219  | 78       | 22              | 12       | 0              | 112  | (manual data data data data data data data da | www.www.water | 100             | 0  | 343  | 743   |   |
|       | 5:15 PM         | 17       | 13       | 37       | 1   | 67   | 6        | 238       | 6        | 2 | 250  | 47       | 40              | 11       | 2              | 98   | immen 6                                       | 182           | และเมพาะจุ้     | 0  | 294  | 709   |   |
|       | 5:30 PM         | 9        | 8        | 41       | 1   | 58   | 1        | 220       | 4        | 0 | 225  | 52       | 28              | 7        | 0              | 87   |   | 185           |                 | 1  | 267  | 637   | ,   |
|       | 5:45 PM         | 5        | 12       | 43       | 0   | 60   | 4        | 198       | 4        | 0 | 206  | 76       | 18              | 5        | 0              | 99   | in the second second                          | 214           | near the second | 1  | 353  | 718   |   |
|       |                 |          |          | 996      | 13  | 1334 |          | 4491      | 94       | 8 |      |          | 315             | 140      | 4              | 1746 |   |               | 1313            | 7  | 6216 | 13939 |   |
|       | App %           |          |          |          |     |      |          | 96.7      |          |   |      | 73.9     |                 |          |                | 12.5 |   | 71.6          |                 |    | 44.6 |       |   |
|       | Total %<br>HV % | 1.0<br>9 | 1.4<br>4 | 7.1<br>3 |     | 9.6  | 0.4<br>9 | 32.2<br>5 | 0.7<br>9 |   | 33.3 | 9.3<br>2 | 2.3             | 1.0<br>4 |                | 12.0 | 3.2<br>2                                      | ง 1.9<br>5    | 9.4<br>2        |    | 44.0 |       |   |
|       | ⊡v %o           | 9        | 4        | J        |     |      | 3        | J         | Э        |   |      | ~        | 0               | · e      |                |      | ~   | 5             | -               |    |      |       |   |

Appendix B

Intersection Level of Service Without National Street Extension

|                               | ٨                            | ~     | *     | Î    | Ļ          | 4          |
|-------------------------------|------------------------------|-------|-------|------|------------|------------|
| Movement                      | EBL                          | EBR   | NBL   | NBT  | SBT        | SBR        |
| Lane Configurations           | ሻ                            | 7     |       | 4¢   | ተ          | ŕ          |
| Volume (vph)                  | 214                          | 75    | 120   | 417  | 678        | 127        |
| Ideal Flow (vphpl)            | 2000                         | 2000  | 2000  | 2000 | 2000       | 2000       |
| Total Lost time (s)           | 6.0                          | 6.0   |       | 6.6  | 6.6        | 6.6        |
| Lane Util. Factor             | 1.00                         | 1.00  |       | 0.95 | 1.00       | 1.00       |
| Frt                           | 1.00                         | 0.85  |       | 1.00 | 1.00       | 0,85       |
| Fit Protected                 | 0.95                         | 1.00  |       | 0.99 | 1.00       | 1.00       |
| Satd. Flow (prot)             | 1863                         | 1667  |       | 3684 | 1961       | 1667       |
| Flt Permitted                 | 0.95                         | 1.00  |       | 0.61 | 1.00       | 1.00       |
| Satd. Flow (perm)             | 1863                         | 1667  |       | 2287 | 1961       | 1667       |
| Peak-hour factor, PHF         | 0.92                         | 0.92  | 0.92  | 0.92 | 0.92       | 0.92       |
| Adj. Flow (vph)               | 233                          | 82    | 130   | 453  | 737        | 138        |
| RTOR Reduction (vph)          | 0                            | 67    | 0     | 0    | 0          | 45         |
| Lane Group Flow (vph)         | 233                          | 15    | 0     | 583  | 737        | 93         |
| Turn Type                     |                              | Perm  | Perm  |      |            | Perm       |
| Protected Phases              | 4                            |       |       | 2    | 6          |            |
| Permitted Phases              |                              | 4     | 2     |      |            | 6          |
| Actuated Green, G (s)         | 16.5                         | 16.5  |       | 60.9 | 60.9       | 60.9       |
| Effective Green, g (s)        | 16.5                         | 16.5  |       | 60.9 | 60.9       | 60.9       |
| Actuated g/C Ratio            | 0,18                         | 0.18  |       | 0.68 | 0.68       | 0.68       |
| Clearance Time (s)            | 6.0                          | 6.0   |       | 6.6  | 6.6        | 6.6        |
| Vehicle Extension (s)         | 3.0                          | 3.0   |       | 3.0  | 3.0        | 3.0        |
| Lane Grp Cap (vph)            | 342                          | 306   |       | 1548 | 1327       | 1128       |
| v/s Ratio Prot                | c0.13                        | un da |       |      | c0.38      |            |
| v/s Ratio Perm                | an a china a sa a sainta b   | 0.01  |       | 0.25 |            | 0.06       |
| v/c Ratio                     | 0.68                         | 0.05  |       | 0.38 | 0.56       | 0.08       |
| Uniform Delay, d1             | 34.3                         | 30.3  |       | 6.3  | 7.5        | 5.0        |
| Progression Factor            | 1.00                         | 1.00  |       | 1.00 | 0.98       | 1.39       |
| Incremental Delay, d2         | 5.5                          | 0.1   |       | 0.7  | 1.5        | 0.1        |
| Delay (s)                     | 39.8                         | 30.4  |       | 7.0  | 8.8        | 7.1        |
| Level of Service              | D                            | С     |       | Α    | А          | А          |
| Approach Delay (s)            | 37.3                         |       |       | 7.0  | 8.6        |            |
| Approach LOS                  | D                            |       |       | А    | А          |            |
| Intersection Summary          |                              |       |       |      | -          |            |
| HCM Average Control Dela      | V                            |       | 13.2  | H    | CM Level   | of Service |
| HCM Volume to Capacity ra     |                              |       | 0.58  |      |            |            |
| Actuated Cycle Length (s)     | 7777.<br>Alexandria (N. A. A |       | 90.0  | Sı   | um of lost | time (s)   |
| Intersection Capacity Utiliza | ation                        |       | 75.4% |      |            | of Service |
| Analysis Period (min)         | 977113333333333              |       | 15    |      |            |            |
| c Critical Lane Group         |                              |       |       |      |            |            |
|                               |                              |       |       |      |            |            |

|  | Å    |      | $\mathbf{i}$ | 1     |            | Ł          | ٩     | Î    | p    | \$             | Ļ    | 4    |
|--|------|------|--------------|-------|------------|------------|-------|------|------|----------------|------|------|
| Movement   | EBL  | EBT  | EBR          | WBL   | WBT        | WBR        | NBL   | NBT  | NBR  | SBL            | SBT  | SBR  |
| Lane Configurations  | ሻ    | ₽    |              | ሻ     | ₽          |            | ካ     | ₽    |      | ۳ <sub>۱</sub> | 个    | ٦    |
| Volume (vph)   | 143  | 153  | 167          | 121   | 68         | 10         | 143   | 393  | 48   | 2              | 447  | 29   |
| Ideal Flow (vphpl)   | 2000 | 2000 | 2000         | 2000  | 2000       | 2000       | 2000  | 2000 | 2000 | 2000           | 2000 | 2000 |
| Total Lost time (s)  | 6.1  | 6.1  |              | 6.1   | 6.1        |            | 5.9   | 5.9  |      | 5.9            | 5.9  | 5.9  |
| Lane Util. Factor  | 1.00 | 1.00 |              | 1.00  | 1.00       |            | 1.00  | 1.00 |      | 1.00           | 1.00 | 1.00 |
| Frt  | 1.00 | 0.92 |              | 1.00  | 0.98       |            | 1.00  | 0.98 |      | 1,00           | 1.00 | 0.85 |
| Flt Protected  | 0.95 | 1.00 |              | 0.95  | 1.00       |            | 0.95  | 1.00 |      | 0.95           | 1.00 | 1.00 |
| Satd. Flow (prot)  | 1881 | 1696 |              | 1845  | 1879       |            | 1652  | 1925 |      | 1900           | 1961 | 1650 |
| Flt Permitted  | 0.69 | 1.00 |              | 0.33  | 1.00       |            | 0.36  | 1.00 |      | 0.31           | 1.00 | 1.00 |
| Satd. Flow (perm)  | 1362 | 1696 |              | 633   | 1879       |            | 625   | 1925 |      | 622            | 1961 | 1650 |
| Peak-hour factor, PHF                                      | 0.81 | 0.81 | 0.81         | 0.73  | 0.73       | 0.73       | 0.74  | 0.74 | 0.74 | 0.84           | 0.84 | 0.84 |
| Adj. Flow (vph)  | 177  | 189  | 206          | 166   | 93         | 14         | 193   | 531  | 65   | 2              | 532  | 35   |
| RTOR Reduction (vph)                                       | 0    | 43   | 0            | 0     | 6          | 0          | 0     | 5    | 0    | 0              | 0    | 10   |
| Lane Group Flow (vph)                                      | 177  | 352  | 0            | 166   | 101        | 0          | 193   | 591  | 0    | 2              | 532  | 25   |
| Heavy Vehicles (%)   | 1%   | 4%   | 13%          | 3%    | 2%         | 20%        | 15%   | 2%   | 4%   | 0%             | 2%   | 3%   |
| Turn Type  | Perm |      |              | Perm  |            |            | Perm  |      |      | Perm           |      | Perm |
| Protected Phases   |      | 4    |              |       | 8          |            |       | 2    |      |                | 6    |      |
| Permitted Phases   | 4    |      |              | 8     |            |            | 2     |      |      | 6              |      | 6    |
| Actuated Green, G (s)                                      | 28.9 | 28.9 |              | 28.9  | 28.9       |            | 49.1  | 49.1 |      | 49.1           | 49.1 | 49.1 |
| Effective Green, g (s)                                     | 28.9 | 28.9 |              | 28.9  | 28.9       |            | 49.1  | 49.1 |      | 49.1           | 49.1 | 49.1 |
| Actuated g/C Ratio   | 0.32 | 0.32 |              | 0.32  | 0.32       |            | 0.55  | 0.55 |      | 0.55           | 0.55 | 0.55 |
| Clearance Time (s)   | 6.1  | 6.1  |              | 6.1   | 6.1        |            | 5.9   | 5.9  |      | 5.9            | 5.9  | 5.9  |
| Lane Grp Cap (vph)   | 437  | 545  |              | 203   | 603        |            | 341   | 1050 |      | 339            | 1070 | 900  |
| v/s Ratio Prot   |      | 0.21 |              |       | 0.05       |            |       | 0.31 |      |                | 0.27 |      |
| v/s Ratio Perm   | 0.13 |      |              | c0.26 |            |            | c0.31 |      |      | 0.00           |      | 0.02 |
| v/c Ratio  | 0.41 | 0.65 |              | 0.82  | 0.17       |            | 0.57  | 0.56 |      | 0.01           | 0.50 | 0.03 |
| Uniform Delay, d1  | 23.8 | 26.2 |              | 28.1  | 21.9       |            | 13.4  | 13.4 |      | 9.3            | 12.8 | 9.4  |
| Progression Factor   | 1.00 | 1.00 |              | 1.00  | 1.00       |            | 1.23  | 1.26 |      | 1.15           | 1.22 | 1.36 |
| Incremental Delay, d2                                      | 2.8  | 5.8  |              | 29.3  | 0.6        |            | 6.5   | 2.1  |      | 0.0            | 1.6  | 0.1  |
| Delay (s)  | 26.6 | 32.0 |              | 57.4  | 22.5       |            | 23.0  | 19.0 |      | 10.8           | 17.2 | 12.9 |
| Level of Service   | С    | С    |              | E     | С          |            | С     | В    |      | В              | В    | В    |
| Approach Delay (s)   |      | 30.3 |              |       | 43.7       |            |       | 20.0 |      |                | 16.9 |      |
| Approach LOS   |      | С    |              |       | D          |            |       | В    |      |                | В    |      |
| Intersection Summary                                       |      |      |              |       |            |            |       |      |      |                |      |      |
| HCM Average Control Delay                                  |      |      | 24.8         | H     | CM Level   | of Service | Э     |      | С    |                |      |      |
| HCM Volume to Capacity ratio                               |      |      | 0.66         |       |            |            |       |      |      |                |      |      |
| Actuated Cycle Length (s)                                  |      |      | 90.0         | Sı    | um of lost | time (s)   |       |      | 12.0 |                |      |      |
| Intersection Capacity Utilizatior<br>Analysis Period (min) |      |      | 76.4%<br>15  |       |            | of Service |       |      | D    |                |      |      |
| c Critical Lane Group                                      |      |      |              |       |            |            |       |      |      |                |      |      |

|   | ٨        | >    | $\mathbf{i}$ | *     | -          | ×.        | 1    | Ť    | p    | 1    | Ļ               | 4    |
|---|----------|------|--------------|-------|------------|-----------|------|------|------|------|-----------------|------|
| Movement  | EBL      | EBT  | EBR          | WBL   | WBT        | WBR       | NBL  | NBT  | NBR  | SBL  | SBT             | SBR  |
| Lane Configurations                                       | <b>P</b> | 个    |              | ሻ     | 个          |           | ×,   | 个    |      | ኻ    | 个               | ሾ    |
| Volume (vph)  | 10       | 10   | 81           | 40    | 10         | 10        | 20   | 279  | 60   | 10   | 349             | 10   |
| Ideal Flow (vphpi)  | 1900     | 1900 | 1900         | 1900  | 1900       | 1900      | 1900 | 1900 | 1900 | 1900 | 1900            | 1900 |
| Total Lost time (s)                                       | 5.8      | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8  |      | 5.8  | 5.8             | 5.8  |
| Lane Util. Factor   | 1.00     | 1.00 |              | 1.00  | 1.00       |           | 1.00 | 1.00 |      | 1.00 | 1.00            | 1.00 |
| Frt   | 1.00     | 0.87 |              | 1.00  | 0.92       |           | 1.00 | 0.97 |      | 1.00 | 1.00            | 0.85 |
| Flt Protected   | 0.95     | 1.00 |              | 0.95  | 1.00       |           | 0.95 | 1.00 |      | 0.95 | 1.00            | 1.00 |
| Satd. Flow (prot)   | 1770     | 1614 |              | 1770  | 1723       |           | 1770 | 1813 |      | 1770 | 1863            | 1583 |
| Flt Permitted   | 0.74     | 1.00 |              | 0.69  | 1.00       |           | 0.47 | 1.00 |      | 0.48 | 1.00            | 1.00 |
| Satd. Flow (perm)   | 1384     | 1614 |              | 1291  | 1723       |           | 881  | 1813 |      | 899  | 1863            | 1583 |
| Peak-hour factor, PHF                                     | 0.92     | 0.92 | 0.92         | 0.92  | 0.92       | 0.92      | 0.92 | 0.92 | 0.92 | 0.92 | 0.92            | 0.92 |
| Adj. Flow (vph)   | 11       | 11   | 88           | 43    | 11         | 11        | 22   | 303  | 65   | 11   | 379             | 11   |
| RTOR Reduction (vph)                                      | 0        | 57   | 0            | 0     | 7          | 0         | 0    | 9    | 0    | 0    | 0               | 5    |
| Lane Group Flow (vph)                                     | 11       | 42   | 0            | 43    | 15         | 0         | 22   | 359  | 0    | 11   | 379             | 6    |
| Turn Type   | Perm     |      |              | Perm  |            |           | Perm |      |      | Perm |                 | Perm |
| Protected Phases  |          | 4    |              |       | 8          |           |      | 2    |      |      | 6               |      |
| Permitted Phases  | 4        |      |              | 8     |            |           | 2    |      |      | 6    | NAR STRATEGICAL | 6    |
| Actuated Green, G (s)                                     | 31.2     | 31.2 |              | 31.2  | 31.2       |           | 47.2 | 47.2 |      | 47.2 | 47.2            | 47.2 |
| Effective Green, g (s)                                    | 31.2     | 31.2 |              | 31.2  | 31.2       |           | 47.2 | 47.2 |      | 47.2 | 47.2            | 47.2 |
| Actuated g/C Ratio  | 0.35     | 0.35 |              | 0.35  | 0.35       |           | 0.52 | 0.52 |      | 0.52 | 0.52            | 0.52 |
| Clearance Time (s)  | 5.8      | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8  |      | 5.8  | 5.8             | 5.8  |
| Lane Grp Cap (vph)  | 480      | 560  |              | 448   | 597        |           | 462  | 951  |      | 471  | 977             | 830  |
| v/s Ratio Prot  |          | 0.03 |              |       | 0.01       |           |      | 0.20 |      |      | c0.20           |      |
| v/s Ratio Perm  | 0.01     |      |              | c0.03 |            |           | 0.02 |      |      | 0.01 |                 | 0.00 |
| v/c Ratio   | 0.02     | 0.07 |              | 0.10  | 0.02       |           | 0.05 | 0.38 |      | 0.02 | 0.39            | 0.01 |
| Uniform Delay, d1   | 19.4     | 19.7 |              | 19.9  | 19.4       |           | 10.4 | 12.7 |      | 10.3 | 12.8            | 10.2 |
| Progression Factor  | 1.00     | 1.00 |              | 1.00  | 1.00       |           | 0.72 | 0.68 |      | 1.03 | 0.81            | 1.19 |
| Incremental Delay, d2                                     | 0.1      | 0.3  |              | 0.4   | 0,1        |           | 0.2  | 1.1  |      | 0.1  | 0.9             | 0.0  |
| Delay (s)   | 19.4     | 20.0 |              | 20.3  | 19.5       |           | 7.7  | 9.7  |      | 10.6 | 11.3            | 12.2 |
| Level of Service  | В        | В    |              | С     | В          |           | Α    | Α    |      | В    | В               | В    |
| Approach Delay (s)  |          | 19.9 |              |       | 20.0       |           |      | 9.6  |      |      | 11.3            |      |
| Approach LOS  |          | В    |              |       | С          |           |      | Α    |      |      | В               |      |
| Intersection Summary                                      |          |      |              |       |            |           |      |      |      |      |                 |      |
| HCM Average Control Delay<br>HCM Volume to Capacity ratio |          |      | 12.2<br>0.27 | H     | CM Level   | of Servic | e    |      | В    |      |                 |      |
| Actuated Cycle Length (s)                                 |          |      | 90.0         | SI    | um of lost | time (s)  |      |      | 11.6 |      |                 |      |
| Intersection Capacity Utilization                         |          |      | 37.0%        |       | U Level c  |           |      |      | A    |      |                 |      |
| Analysis Period (min)                                     |          |      | 15           |       |            |           |      |      |      |      |                 |      |

|                                   | ٨    |            | $\mathbf{k}$ | 1     | 4          | ×.        |       | Ť    | p    | 1    | w.    | ~    |
|-----------------------------------|------|------------|--------------|-------|------------|-----------|-------|------|------|------|-------|------|
| Movement                          | EBL  | EBT        | EBR          | WBL   | WBT        | WBR       | NBL   | NBT  | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | ٣    | <b>ተ</b> ጮ |              | ሻ     | <b>≜</b> ₽ |           | ሻ     | ₿    |      | ٦Ť   | 4     |      |
| Volume (vph)                      | 17   | 396        | 59           | 58    | 413        | 11        | 56    | 137  | 86   | 40   | 242   | 9    |
| Ideal Flow (vphpl)                | 2000 | 2000       | 2000         | 2000  | 2000       | 2000      | 2000  | 2000 | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)               | 6.0  | 6.0        |              | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |      |
| Lane Util. Factor                 | 1.00 | 0.95       |              | 1.00  | 0.95       |           | 1.00  | 1.00 |      | 1.00 | 1.00  |      |
| Frt                               | 1.00 | 0.98       |              | 1.00  | 1.00       |           | 1.00  | 0.94 |      | 1.00 | 0.99  |      |
| Flt Protected                     | 0.95 | 1.00       |              | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (prot)                 | 1863 | 3653       |              | 1863  | 3711       |           | 1863  | 1847 |      | 1863 | 1950  |      |
| Flt Permitted                     | 0.95 | 1.00       |              | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (perm)                 | 1863 | 3653       |              | 1863  | 3711       |           | 1863  | 1847 |      | 1863 | 1950  |      |
| Peak-hour factor, PHF             | 0.79 | 0.79       | 0.79         | 0.70  | 0.70       | 0.70      | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81 |
| Adj. Flow (vph)                   | 22   | 501        | 75           | 83    | 590        | 16        | 59    | 144  | 91   | 49   | 299   | 11   |
| RTOR Reduction (vph)              | 0    | 12         | 0            | 0     | 2          | 0         | 0     | 25   | 0    | 0    | 2     | 0    |
| Lane Group Flow (vph)             | 22   | 564        | 0            | 83    | 604        | 0         | 59    | 210  | 0    | 49   | 308   | 0    |
| Turn Type                         | Prot |            |              | Prot  |            |           | Prot  |      |      | Prot |       |      |
| Protected Phases                  | 5    | 2          |              | 1     | 6          |           | 3     | 8    |      | 7    | 4     |      |
| Permitted Phases                  |      |            |              |       |            |           |       |      |      |      | h     |      |
| Actuated Green, G (s)             | 3.0  | 32.1       |              | 7.0   | 36.1       |           | 7.1   | 21.5 |      | 5.4  | 19.8  |      |
| Effective Green, g (s)            | 3.0  | 32.1       |              | 7.0   | 36.1       |           | 7.1   | 21.5 |      | 5.4  | 19.8  |      |
| Actuated g/C Ratio                | 0.03 | 0.36       |              | 0.08  | 0.40       |           | 0.08  | 0.24 |      | 0.06 | 0.22  |      |
| Clearance Time (s)                | 6.0  | 6.0        |              | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |      |
| Vehicle Extension (s)             | 3.0  | 3.0        |              | 3.0   | 3.0        |           | 3.0   | 3.0  |      | 3.0  | 3.0   |      |
| Lane Grp Cap (vph)                | 62   | 1303       |              | 145   | 1489       |           | 147   | 441  |      | 112  | 429   |      |
| v/s Ratio Prot                    | 0.01 | 0.15       |              | c0.04 | c0.16      |           | c0.03 | 0.11 |      | 0.03 | c0.16 |      |
| v/s Ratio Perm                    |      |            |              |       |            |           |       |      |      |      |       |      |
| v/c Ratio                         | 0.35 | 0.43       |              | 0.57  | 0.41       |           | 0.40  | 0,48 |      | 0.44 | 0.72  |      |
| Uniform Delay, d1                 | 42.6 | 22.0       |              | 40.1  | 19.3       |           | 39.4  | 29.4 |      | 40.8 | 32.5  |      |
| Progression Factor                | 1.00 | 1.00       |              | 0.88  | 0.67       |           | 1.27  | 0.61 |      | 1.00 | 1.00  |      |
| Incremental Delay, d2             | 3.5  | 1.1        |              | 4.5   | 0.7        |           | 1.7   | 0.8  |      | 2.7  | 5.7   |      |
| Delay (s)                         | 46.0 | 23.1       |              | 39.7  | 13.7       |           | 51.8  | 18.7 |      | 43.6 | 38.2  |      |
| Level of Service                  | D    | С          |              | D     | В          |           | D     | В    |      | D    | D     |      |
| Approach Delay (s)                |      | 23.9       |              |       | 16.8       |           |       | 25.3 |      |      | 38.9  |      |
| Approach LOS                      |      | С          |              |       | В          |           |       | С    |      |      | D     |      |
| Intersection Summary              |      |            |              |       |            |           |       |      |      |      |       |      |
| HCM Average Control Delay         |      |            | 24.4         | H     | CM Level   | of Servic | e     |      | С    |      |       |      |
| HCM Volume to Capacity ratio      |      |            | 0.54         |       |            |           |       |      |      |      |       |      |
| Actuated Cycle Length (s)         |      |            | 90.0         |       | um of lost |           |       |      | 24.0 |      |       |      |
| Intersection Capacity Utilization | 1    |            | 56.5%        | IC    | U Level o  | f Service |       |      | В    |      |       |      |
| Analysis Period (min)             |      |            | 15           |       |            |           |       |      |      |      |       |      |
| c Critical Lane Group             |      |            |              |       |            |           |       |      |      |      |       |      |

|                                | ٨                                     |                         | ¥     | 1    |            | Ł.        | ٩    | Â    | p    | 6     | Ļ    | 4    |
|--------------------------------|---------------------------------------|-------------------------|-------|------|------------|-----------|------|------|------|-------|------|------|
| Movement                       | EBL                                   | EBT                     | EBR   | WBL  | WBT        | WBR       | NBL  | NBT  | NBR  | SBL   | SBT  | SBR  |
| Lane Configurations            | Ĩ                                     | <b>ት</b> ፞ ኡ            |       | ሻ    | 个          | ሻ         | ٣    | ĵ≽   |      | ሻ     | ¢Î   |      |
| Volume (vph)                   | 4                                     | 632                     | 6     | 54   | 633        | 105       | 7    | 12   | 143  | 165   | 19   | 9    |
| Ideal Flow (vphpl)             | 2000                                  | 2000                    | 2000  | 2000 | 2000       | 2000      | 2000 | 2000 | 2000 | 2000  | 2000 | 2000 |
| Total Lost time (s)            | 6.1                                   | 6.1                     |       | 6.1  | 6.1        | 6.1       | 6.0  | 6.0  |      | 6.0   | 6.0  |      |
| Lane Util. Factor              | 1.00                                  | 0.95                    |       | 1.00 | 1.00       | 1.00      | 1.00 | 1.00 |      | 1.00  | 1.00 |      |
| Frt                            | 1.00                                  | 1.00                    |       | 1.00 | 1.00       | 0.85      | 1.00 | 0.86 |      | 1.00  | 0.95 |      |
| Flt Protected                  | 0.95                                  | 1.00                    |       | 0.95 | 1.00       | 1.00      | 0.95 | 1.00 |      | 0.95  | 1.00 |      |
| Satd. Flow (prot)              | 1863                                  | 3720                    |       | 1863 | 1961       | 1500      | 1863 | 1689 |      | 1863  | 1865 |      |
| Flt Permitted                  | 0.16                                  | 1.00                    |       | 0.28 | 1.00       | 1.00      | 0.73 | 1.00 |      | 0.63  | 1.00 |      |
| Satd. Flow (perm)              | 314                                   | 3720                    |       | 540  | 1961       | 1500      | 1437 | 1689 |      | 1229  | 1865 |      |
| Peak-hour factor, PHF          | 0.76                                  | 0.76                    | 0.76  | 0.83 | 0.83       | 0.83      | 0.83 | 0.83 | 0.83 | 0.75  | 0.75 | 0.75 |
| Adj. Flow (vph)                | 5                                     | 832                     | 8     | 65   | 763        | 127       | 8    | 14   | 172  | 220   | 25   | 12   |
| RTOR Reduction (vph)           | 0                                     | 1                       | 0     | 0    | 0          | 62        | 0    | 0    | 0    | 0     | 8    | 0    |
| Lane Group Flow (vph)          | 5                                     | 839                     | 0     | 65   | 763        | 65        | 8    | 186  | 0    | 220   | 29   | 0    |
| Parking (#/hr)                 | · · · · · · · · · · · · · · · · · · · | en Teda Merez d'Arres a | 0     |      |            | 0         |      |      |      |       |      |      |
| Turn Type                      | Perm                                  |                         |       | Perm |            | Perm      | Perm |      |      | Perm  |      |      |
| Protected Phases               |                                       | 2                       |       |      | 6          |           |      | 8    |      |       | 4    |      |
| Permitted Phases               | 2                                     |                         |       | 6    |            | 6         | 8    |      |      | 4     |      |      |
| Actuated Green, G (s)          | 45.9                                  | 45.9                    |       | 45.9 | 45.9       | 45.9      | 32.0 | 32.0 |      | 32.0  | 32.0 |      |
| Effective Green, g (s)         | 45.9                                  | 45.9                    |       | 45.9 | 45.9       | 45.9      | 32.0 | 32.0 |      | 32.0  | 32.0 |      |
| Actuated g/C Ratio             | 0.51                                  | 0.51                    |       | 0.51 | 0.51       | 0.51      | 0.36 | 0.36 |      | 0.36  | 0.36 |      |
| Clearance Time (s)             | 6.1                                   | 6.1                     |       | 6.1  | 6.1        | 6.1       | 6.0  | 6.0  |      | 6.0   | 6.0  |      |
| Lane Grp Cap (vph)             | 160                                   | 1897                    |       | 275  | 1000       | 765       | 511  | 601  |      | 437   | 663  |      |
| v/s Ratio Prot                 |                                       | 0.23                    |       |      | c0.39      |           |      | 0.11 |      |       | 0.02 |      |
| v/s Ratio Perm                 | 0.02                                  |                         |       | 0.12 |            | 0.04      | 0.01 |      |      | c0.18 |      |      |
| v/c Ratio                      | 0.03                                  | 0.44                    |       | 0.24 | 0.76       | 0.08      | 0.02 | 0.31 |      | 0.50  | 0.04 |      |
| Uniform Delay, d1              | 11.0                                  | 14.0                    |       | 12.3 | 17.7       | 11.3      | 18.8 | 21.0 |      | 22.8  | 19.0 |      |
| Progression Factor             | 0.75                                  | 0.97                    |       | 1.00 | 1.00       | 1.00      | 1.00 | 1.00 |      | 1.00  | 1.00 |      |
| Incremental Delay, d2          | 0.4                                   | 0.7                     |       | 2.0  | 5.5        | 0.2       | 0.1  | 1.3  |      | 4.1   | 0.1  |      |
| Delay (s)                      | 8.6                                   | 14.3                    |       | 14.3 | 23.2       | 11.5      | 18.8 | 22.3 |      | 26.9  | 19.1 |      |
| Level of Service               | А                                     | В                       |       | В    | С          | В         | В    | С    |      | С     | В    |      |
| Approach Delay (s)             |                                       | 14.3                    |       |      | 21.0       |           |      | 22.2 |      |       | 25.7 |      |
| Approach LOS                   |                                       | В                       |       |      | С          |           |      | С    |      |       | С    |      |
| Intersection Summary           |                                       |                         |       |      |            |           |      |      |      |       |      |      |
| HCM Average Control Delay      |                                       |                         | 19.1  | H    | CM Level   | of Servic | e    |      | В    |       |      |      |
| HCM Volume to Capacity rat     | tio                                   |                         | 0.66  |      |            |           |      |      |      |       |      |      |
| Actuated Cycle Length (s)      |                                       |                         | 90.0  |      | um of lost |           |      |      | 12.1 |       |      |      |
| Intersection Capacity Utilizat | ion                                   |                         | 75.4% | IC   | U Level c  | f Service |      |      | D    |       |      |      |
| Analysis Period (min)          |                                       |                         | 15    |      |            |           |      |      |      |       |      |      |
| c Critical Lane Group          |                                       |                         |       |      |            |           |      |      |      |       |      |      |

|                              | ٨                             | V    | 4     | Î                | Ļ                         | 1          |   |
|------------------------------|-------------------------------|------|-------|------------------|---------------------------|------------|---|
| Movement                     | EBL                           | EBR  | NBL   | NBT              | SBT                       | SBR        |   |
| Lane Configurations          | ሻ                             | 7    |       | ት <mark>`</mark> | 个                         | 7          |   |
| Volume (vph)                 | 520                           | 240  | 84    | 408              | 650                       | 191        |   |
| Ideal Flow (vphpl)           | 2000                          | 2000 | 2000  | 2000             | 2000                      | 2000       |   |
| Total Lost time (s)          | 6.0                           | 6.0  |       | 6.6              | 6.6                       | 6.6        |   |
| Lane Util. Factor            | 1.00                          | 1.00 |       | 0.95             | 1.00                      | 1.00       |   |
| Frt                          | 1.00                          | 0.85 |       | 1.00             | 1.00                      | 0.85       |   |
| -It Protected                | 0.95                          | 1.00 |       | 0.99             | 1.00                      | 1.00       |   |
| Satd. Flow (prot)            | 1863                          | 1667 |       | 3694             | 1961                      | 1667       |   |
| -It Permitted                | 0.95                          | 1.00 |       | 0.63             | 1.00                      | 1.00       |   |
| Satd. Flow (perm)            | 1863                          | 1667 |       | 2332             | 1961                      | 1667       |   |
| Peak-hour factor, PHF        | 0.92                          | 0.92 | 0.92  | 0.92             | 0.92                      | 0.92       |   |
| Adj. Flow (vph)              | 565                           | 261  | 91    | 443              | 707                       | 208        |   |
| RTOR Reduction (vph)         | 0                             | 133  | 0     | 0                | 0                         | 95         |   |
| _ane Group Flow (vph)        | 565                           | 128  | 0     | 534              | 707                       | 113        |   |
| Turn Type                    |                               | Perm | Perm  |                  |                           | Perm       | <b></b>   |
| Protected Phases             | 4                             |      |       | 2                | 6                         |            |   |
| Permitted Phases             |                               | 4    | 2     |                  | er e dinê tê din mê te te | 6          |   |
| Actuated Green, G (s)        | 28.6                          | 28.6 |       | 48.8             | 48.8                      | 48.8       |   |
| Effective Green, g (s)       | 28.6                          | 28.6 |       | 48.8             | 48.8                      | 48.8       |   |
| Actuated g/C Ratio           | 0.32                          | 0.32 |       | 0.54             | 0.54                      | 0.54       |   |
| Clearance Time (s)           | 6.0                           | 6.0  |       | 6.6              | 6.6                       | 6.6        | en eine deue alle eine eine deue deut mehr deut weiten bei um eine eine deut deut eine deut eine eine eine eine |
| /ehicle Extension (s)        | 3.0                           | 3.0  |       | 3.0              | 3.0                       | 3.0        |   |
| ane Grp Cap (vph)            | 592                           | 530  |       | 1264             | 1063                      | 904        |   |
| //s Ratio Prot               | c0.30                         |      |       |                  | c0.36                     |            |   |
| /s Ratio Perm                |                               | 0.08 |       | 0.23             |                           | 0.07       |   |
| //c Ratio                    | 0.95                          | 0.24 |       | 0.42             | 0.67                      | 0.12       |   |
| Jniform Delay, d1            | 30.1                          | 22.7 |       | 12.2             | 14.7                      | 10.1       |   |
| Progression Factor           | 1.00                          | 1.00 |       | 1.00             | 1.40                      | 2.59       |   |
| ncremental Delay, d2         | 25.9                          | 0.2  |       | 1.0              | 2.5                       | 0.2        |   |
| )elay (s)                    | 55.9                          | 22.9 |       | 13.3             | 23.1                      | 26.4       |   |
| evel of Service              | E                             | С    |       | В                | С                         | С          |   |
| Approach Delay (s)           | 45.5                          |      |       | 13.3             | 23.9                      |            |   |
| Approach LOS                 | D                             |      |       | В                | С                         |            |   |
| ntersection Summary          |                               |      |       |                  |                           |            |   |
| ICM Average Control Dela     | Ŋ                             |      | 29.2  | H                | CM Level                  | of Service | С   |
| ICM Volume to Capacity ra    |                               |      | 0.77  |                  |                           |            |   |
| Actuated Cycle Length (s)    |                               |      | 90.0  | Sı               | um of lost                | time (s)   | 12.6  |
| ntersection Capacity Utiliza | ation                         |      | 88.9% |                  |                           | of Service | E CARACTERIA  |
| Analysis Period (min)        | errend et el batelle el litte |      | 15    | n an chuidheadh. |                           |            | nin oli urbul ing bolin u curven fran effektion i Bergelen (m. 2005).<br>19                                     |
| Critical Lane Group          |                               |      |       |                  |                           |            |   |

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|---|------|------|-------------|-------|------------|------------|------|-------|------|--------------------------|------|------|
| Movement  | EBL  | EBT  | EBR         | WBL   | WBT        | WBR        | NBL  | NBT   | NBR  | SBL                      | SBT  | SBF  |
| Lane Configurations                                       | ኻ    | \$   |             | ሻ     | ₽          |            | ሻ    | ۴,    |      | Ϋ́ς                      | Ŷ    | 5    |
| Volume (vph)  | 100  | 143  | 220         | 129   | 243        | 4          | 225  | 628   | 54   | 3                        | 497  | 130  |
| Ideal Flow (vphpl)  | 2000 | 2000 | 2000        | 2000  | 2000       | 2000       | 2000 | 2000  | 2000 | 2000                     | 2000 | 2000 |
| Total Lost time (s)                                       | 6.1  | 6.1  |             | 6.1   | 6.1        |            | 5.9  | 5.9   |      | 5.9                      | 5.9  | 5.9  |
| Lane Util. Factor   | 1.00 | 1.00 |             | 1.00  | 1.00       |            | 1.00 | 1.00  |      | 1.00                     | 1.00 | 1.00 |
| Frt   | 1.00 | 0.91 |             | 1.00  | 1.00       |            | 1.00 | 0.99  |      | 1.00                     | 1.00 | 0.85 |
| Fit Protected   | 0.95 | 1.00 |             | 0.95  | 1.00       |            | 0.95 | 1.00  |      | 0.95                     | 1.00 | 1.00 |
| Satd. Flow (prot)   | 1881 | 1765 |             | 1863  | 1938       |            | 1743 | 1927  |      | 1900                     | 1980 | 1650 |
| Flt Permitted   | 0.42 | 1.00 |             | 0.24  | 1.00       |            | 0.38 | 1.00  |      | 0.21                     | 1.00 | 1.00 |
| Satd. Flow (perm)   | 839  | 1765 |             | 474   | 1938       |            | 693  | 1927  |      | 425                      | 1980 | 1650 |
| Peak-hour factor, PHF                                     | 0.83 | 0.83 | 0.83        | 0.80  | 0.80       | 0.80       | 0.90 | 0.90  | 0.90 | 0.95                     | 0.95 | 0.95 |
| Adj. Flow (vph)   | 120  | 172  | 265         | 161   | 304        | 5          | 250  | 698   | 60   | 3                        | 523  | 137  |
| RTOR Reduction (vph)                                      | 0    | 62   | 0           | 0     | 1          | 0          | 0    | 3     | 0    | 0                        | 0    | 38   |
| Lane Group Flow (vph)                                     | 120  | 375  | 0           | 161   | 308        | 0          | 250  | 755   | 0    | 3                        | 523  | 99   |
| Heavy Vehicles (%)  | 1%   | 0%   | 5%          | 2%    | 3%         | 0%         | 9%   | 2%    | 9%   | 0%                       | 1%   | 3%   |
| Turn Type   | Perm |      |             | Perm  |            | 6NE9.5     | Perm |       |      | Perm                     |      | Perm |
| Protected Phases  |      | 4    |             |       | 8          |            |      | 2     |      | ala da Bernara Parataka. | 6    |      |
| Permitted Phases  | 4    |      |             | 8     |            |            | 2    |       |      | 6                        |      | 6    |
| Actuated Green, G (s)                                     | 26.9 | 26.9 |             | 26.9  | 26.9       |            | 51.1 | 51.1  |      | 51.1                     | 51.1 | 51.1 |
| Effective Green, g (s)                                    | 26.9 | 26.9 |             | 26.9  | 26.9       |            | 51.1 | 51.1  |      | 51.1                     | 51.1 | 51.1 |
| Actuated g/C Ratio  | 0.30 | 0.30 |             | 0.30  | 0.30       |            | 0.57 | 0.57  |      | 0.57                     | 0.57 | 0.57 |
| Clearance Time (s)  | 6.1  | 6.1  |             | 6.1   | 6.1        |            | 5.9  | 5.9   |      | 5.9                      | 5.9  | 5.9  |
| Lane Grp Cap (vph)  | 251  | 528  |             | 142   | 579        |            | 393  | 1094  |      | 241                      | 1124 | 937  |
| v/s Ratio Prot  |      | 0.21 |             |       | 0.16       |            |      | c0.39 |      |                          | 0.26 |      |
| v/s Ratio Perm  | 0.14 |      |             | c0.34 |            |            | 0.36 |       |      | 0.01                     |      | 0.06 |
| v/c Ratio   | 0.48 | 0.71 |             | 1.13  | 0.53       |            | 0.64 | 0.69  |      | 0.01                     | 0.47 | 0.11 |
| Uniform Delay, d1   | 25.8 | 28.1 |             | 31.6  | 26.3       |            | 13.2 | 13.8  |      | 8.5                      | 11.4 | 8.9  |
| Progression Factor  | 1.00 | 1.00 |             | 1.00  | 1.00       |            | 1.21 | 1.24  |      | 0.95                     | 1.05 | 1.18 |
| Incremental Delay, d2                                     | 6.4  | 7.9  |             | 116.0 | 3.5        |            | 6.3  | 2.9   |      | 0.1                      | 1.3  | 0.2  |
| Delay (s)   | 32.2 | 36.0 |             | 147.5 | 29.8       |            | 22.3 | 20.1  |      | 8.2                      | 13.4 | 10.8 |
| Level of Service  | С    | D    |             | F     | С          |            | С    | С     |      | А                        | В    | В    |
| Approach Delay (s)  |      | 35.2 |             |       | 70.1       |            |      | 20.7  |      |                          | 12.8 |      |
| Approach LOS  |      | D    |             |       | Е          |            |      | С     |      |                          | В    |      |
| Intersection Summary                                      |      |      |             |       |            |            |      |       |      |                          |      |      |
| HCM Average Control Delay                                 |      |      | 30.3        | НС    | CM Level   | of Service | )    |       | С    |                          |      |      |
| HCM Volume to Capacity ration                             | )    |      | 0.84        |       |            |            |      |       |      |                          |      |      |
| Actuated Cycle Length (s)                                 |      |      | 90.0        |       | im of lost |            |      |       | 12.0 |                          |      |      |
| Intersection Capacity Utilizatic<br>Analysis Period (min) | n    |      | 91.1%<br>15 | IC    | U Level o  | f Service  |      |       | F    |                          |      |      |
| Analysis Period (min)<br>c Critical Lane Group            |      |      | 15          |       |            |            |      |       |      |                          |      |      |

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|-----------------------------------|--|------|------------------------------------|-------|-------------------------|------------|------|-------|------|------|------------------------|------------------|
| Movement                          | EBL  | EBT  | EBR                                | WBL   | WBT                     | WBR        | NBL  | NBT   | NBR  | SBL  | SBT                    | SBR              |
| Lane Configurations               | ሻ  | ĥ    |                                    | ሻ     | ef.                     |            | ሻ    | ¢ĵ    |      | ሻ    | Ŷ                      | ľ                |
| Volume (vph)                      | 27   | 20   | 105                                | 190   | 25                      | 66         | 24   | 345   | 88   | 13   | 416                    | 32               |
| Ideal Flow (vphpi)                | 2000   | 2000 | 2000                               | 2000  | 2000                    | 2000       | 2000 | 2000  | 2000 | 2000 | 2000                   | 2000             |
| Total Lost time (s)               | 5.8  | 5.8  |                                    | 5.8   | 5.8                     |            | 5.8  | 5.8   |      | 5.8  | 5.8                    | 5.8              |
| Lane Util. Factor                 | 1.00   | 1.00 |                                    | 1.00  | 1.00                    |            | 1.00 | 1.00  |      | 1.00 | 1.00                   | 1.00             |
| Ert                               | 1.00   | 0.87 |                                    | 1.00  | 0.89                    |            | 1.00 | 0.97  |      | 1.00 | 1.00                   | 0.85             |
| Flt Protected                     | 0.95   | 1.00 |                                    | 0.95  | 1.00                    |            | 0.95 | 1.00  |      | 0.95 | 1.00                   | 1.00             |
| Satd. Flow (prot)                 | 1863   | 1714 |                                    | 1863  | 1747                    |            | 1863 | 1901  |      | 1863 | 1961                   | 1667             |
| Flt Permitted                     | 0.69   | 1.00 |                                    | 0.67  | 1.00                    |            | 0.41 | 1.00  |      | 0.40 | 1.00                   | 1.00             |
| Satd. Flow (perm)                 | 1359   | 1714 |                                    | 1314  | 1747                    |            | 806  | 1901  |      | 775  | 1961                   | 1667             |
| Peak-hour factor, PHF             | 0.92   | 0.92 | 0.92                               | 0.92  | 0.92                    | 0.92       | 0.92 | 0.92  | 0.92 | 0.92 | 0.92                   | 0.92             |
| Adj. Flow (vph)                   | 29   | 22   | 114                                | 207   | 27                      | 72         | 26   | 375   | 96   | 14   | 452                    | 35               |
| RTOR Reduction (vph)              | 0  | 74   | 0                                  | 0     | 47                      | 0          | 0    | 10    | 0    | 0    | 0                      | 16               |
| Lane Group Flow (vph)             | 29   | 62   | 0                                  | 207   | 52                      | 0          | 26   | 461   | 0    | 14   | 452                    | 19               |
| Turn Type                         | Perm   |      |                                    | Perm  |                         |            | Perm |       |      | Perm |                        | Perm             |
| Protected Phases                  |  | 4    |                                    |       | 8                       |            |      | 2     |      |      | 6                      |                  |
| Permitted Phases                  | 4  |      | tool or a standard                 | 8     |                         |            | 2    |       |      | 6    |                        | 6                |
| Actuated Green, G (s)             | 31.2   | 31.2 |                                    | 31.2  | 31.2                    |            | 47.2 | 47.2  |      | 47.2 | 47.2                   | 47.2             |
| Effective Green, g (s)            | 31.2   | 31.2 |                                    | 31.2  | 31.2                    |            | 47.2 | 47.2  |      | 47.2 | 47.2                   | 47.2             |
| Actuated g/C Ratio                | 0.35   | 0,35 |                                    | 0.35  | 0.35                    |            | 0.52 | 0.52  |      | 0.52 | 0.52                   | 0.52             |
| Clearance Time (s)                | 5.8  | 5.8  |                                    | 5.8   | 5.8                     |            | 5.8  | 5.8   |      | 5.8  | 5.8                    | 5.8              |
| Lane Grp Cap (vph)                | 471  | 594  |                                    | 456   | 606                     |            | 423  | 997   |      | 406  | 1028                   | 874              |
| v/s Ratio Prot                    |  | 0.04 |                                    |       | 0.03                    |            |      | c0.24 |      |      | 0.23                   |                  |
| v/s Ratio Perm                    | 0.02   |      |                                    | c0.16 |                         |            | 0.03 |       |      | 0.02 |                        | 0.01             |
| v/c Ratio                         | 0.06   | 0.10 | a na bana na harina da da da da ba | 0.45  | 0.09                    |            | 0.06 | 0.46  |      | 0.03 | 0.44                   | 0.02             |
| Uniform Delay, d1                 | 19.6   | 19.9 |                                    | 22.8  | 19.8                    |            | 10.5 | 13.4  |      | 10.4 | 13.2                   | 10.3             |
| Progression Factor                | 1.00   | 1.00 |                                    | 1.00  | 1.00                    |            | 0.61 | 0.48  |      | 1.06 | 0.92                   | 1.40             |
| Incremental Delay, d2             | 0.3  | 0.3  |                                    | 3.2   | 0.3                     |            | 0.2  | 1.3   |      | 0.1  | 1.1                    | 0.0              |
| Delay (s)                         | 19.9   | 20.3 |                                    | 26.0  | 20.1                    |            | 6.6  | 7.7   |      | 11.1 | 13.2                   | 14.5             |
| Level of Service                  | В  | С    |                                    | С     | С                       |            | Α    | Α     |      | В    | В                      | В                |
| Approach Delay (s)                |  | 20.2 |                                    |       | 24.1                    |            |      | 7.7   |      |      | 13.2                   |                  |
| Approach LOS                      |  | С    |                                    |       | С                       |            |      | Α     |      |      | В                      |                  |
| Intersection Summary              |  |      |                                    |       |                         |            |      |       |      |      |                        |                  |
| HCM Average Control Delay         |  |      | 14.4                               | H     | CM Level                | of Servic  | е    |       | В    |      |                        | and a set of the |
| HCM Volume to Capacity ratio      | n shinin manakiri  |      | 0.46                               |       | listel fil for an entre |            |      |       |      |      | enne Yn dryf yn dir ei | nn (rennik) ()   |
| Actuated Cycle Length (s)         |  |      | 90.0                               | Sı    | im of lost              | time (s)   |      |       | 11.6 |      |                        |                  |
| Intersection Capacity Utilization | 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -<br>1 |      | 54.0%                              |       |                         | of Service |      |       | А    |      |                        |                  |
| Analysis Period (min)             |  |      | 15                                 |       |                         |            |      |       |      |      |                        |                  |

| Lane ConfigurationsVolume (vph)Ideal Flow (vphpl)2Total Lost time (s)Lane Util. FactorFrtFit Protected | EBL<br>47<br>2000<br>6.0<br>1.00<br>1.00<br>0.95<br>1863 | EBT<br><b>†1</b> -<br>467<br>2000<br>6.0<br>0.95 | EBR<br>68<br>2000 | WBL   | WBT<br><b>^^</b> | WBR        | NBL   | NBT   | NBR                                 | SBL  | SBT  | SBR     |
|--|--|--|-------------------|-------|------------------|------------|-------|-------|-------------------------------------|------|------|---------|
| Volume (vph)Ideal Flow (vphpl)2Total Lost time (s)Lane Util. FactorFrtFlt Protected                    | 47<br>2000<br>6.0<br>1.00<br>1.00<br>0.95                | 467<br>2000<br>6.0<br>0.95                       |                   | 138   |                  |            | 10c   | ٠     |                                     | -    |      |         |
| Ideal Flow (vphpl)2Total Lost time (s)Lane Util. FactorFrtFlt Protected                                | 2000<br>6.0<br>1.00<br>1.00<br>0.95                      | 2000<br>6.0<br>0.95                              |                   |       |                  |            | .1    | ኈ     |                                     | ሻ    | ₽    |         |
| Total Lost time (s)<br>Lane Util. Factor<br>Frt<br>Flt Protected                                       | 6.0<br>1.00<br>1.00<br>0.95                              | 6.0<br>0.95                                      | 2000              | 0000  | 462              | 94         | 75    | 288   | 75                                  | 62   | 255  | 16      |
| Lane Util. Factor<br>Frt<br>Flt Protected (  | 1.00<br>1.00<br>0.95                                     | 0.95   |                   | 2000  | 2000             | 2000       | 2000  | 2000  | 2000                                | 2000 | 2000 | 2000    |
| Frt Fit Protected  | 1.00<br>0.95   |  |                   | 6.0   | 6.0              |            | 6.0   | 6.0   |                                     | 6.0  | 6.0  |         |
| Flt Protected (  | 0.95   | ener konzerte italiere                           |                   | 1.00  | 0.95             |            | 1.00  | 1.00  |                                     | 1.00 | 1.00 |         |
|  |  | 0.98   |                   | 1.00  | 0.97             |            | 1.00  | 0.97  |                                     | 1.00 | 0.99 |         |
| Satd. Flow (prot) 1  | 1863   | 1.00   |                   | 0.95  | 1.00             |            | 0.95  | 1.00  |                                     | 0.95 | 1.00 |         |
|  | 1000   | 3654   |                   | 1863  | 3631             |            | 1863  | 1900  |                                     | 1863 | 1943 |         |
| Flt Permitted (  | 0.95   | 1.00   |                   | 0.95  | 1.00             |            | 0.95  | 1.00  |                                     | 0.95 | 1.00 |         |
| Satd. Flow (perm) 1  | 863  | 3654   |                   | 1863  | 3631             |            | 1863  | 1900  |                                     | 1863 | 1943 |         |
| Peak-hour factor, PHF (  | 0.90   | 0.90   | 0.90              | 0.92  | 0.92             | 0.92       | 0.89  | 0.89  | 0.89                                | 0.90 | 0.90 | 0.90    |
| Adj. Flow (vph)  | 52   | 519  | 76                | 150   | 502              | 102        | 84    | 324   | 84                                  | 69   | 283  | 18      |
| RTOR Reduction (vph)   | 0  | 12   | 0                 | 0     | 17               | 0          | 0     | 11    | 0                                   | 0    | 2    | 0       |
| Lane Group Flow (vph)  | 52   | 583  | 0                 | 150   | 587              | 0          | 84    | 397   | 0                                   | 69   | 299  | 0       |
|  | Prot   |  |                   | Prot  |                  |            | Prot  |       |                                     | Prot |      | <u></u> |
| Protected Phases   | 5  | 2  |                   | 1     | 6                |            | 3     | 8     |                                     | 7    | 4    |         |
| Permitted Phases   |  |  |                   |       |                  |            |       |       | n kan serien serien serien date dar |      |      |         |
| Actuated Green, G (s)  | 5.4  | 27.7   |                   | 9.9   | 32.2             |            | 7.0   | 21.6  |                                     | 6.8  | 21.4 |         |
| Effective Green, g (s)   | 5.4  | 27.7   |                   | 9.9   | 32.2             |            | 7.0   | 21.6  |                                     | 6.8  | 21.4 |         |
| Actuated g/C Ratio (   | 0.06   | 0.31   |                   | 0.11  | 0.36             |            | 0.08  | 0.24  |                                     | 0.08 | 0.24 |         |
| Clearance Time (s)   | 6.0  | 6.0  |                   | 6.0   | 6.0              |            | 6.0   | 6.0   |                                     | 6.0  | 6.0  |         |
| Vehicle Extension (s)  | 3.0  | 3.0  |                   | 3.0   | 3.0              |            | 3.0   | 3.0   |                                     | 3.0  | 3.0  |         |
| Lane Grp Cap (vph)   | 112  | 1125   |                   | 205   | 1299             |            | 145   | 456   |                                     | 141  | 462  |         |
| v/s Ratio Prot   | 0.03   | c0.16  |                   | c0.08 | c0.16            |            | c0.05 | c0.21 |                                     | 0.04 | 0,15 |         |
| v/s Ratio Perm   |  |  |                   |       |                  |            |       |       |                                     |      |      |         |
| v/c Ratio  | 0.46   | 0.52   |                   | 0.73  | 0.45             |            | 0.58  | 0.87  |                                     | 0.49 | 0.65 |         |
| Uniform Delay, d1 4  | 40.9   | 25.7   |                   | 38.8  | 22.1             |            | 40.1  | 32.9  |                                     | 39.9 | 30.9 |         |
| Progression Factor 1   | 1.00   | 1.00   |                   | 0.88  | 0.73             |            | 1.27  | 0.85  |                                     | 1.00 | 1.00 |         |
| Incremental Delay, d2  | 3.0  | 1.7  |                   | 9.5   | 0.8              |            | 5.2   | 15.7  |                                     | 2.7  | 3.1  |         |
| Delay (s)  | 43.9   | 27.4   |                   | 43.7  | 16.9             |            | 56.1  | 43.8  |                                     | 42.6 | 34.0 |         |
| Level of Service   | D  | С  |                   | D     | В                |            | E     | D     |                                     | D    | С    |         |
| Approach Delay (s)   |  | 28.7   |                   |       | 22.3             |            |       | 45.9  |                                     |      | 35.6 |         |
| Approach LOS   |  | С  |                   |       | С                |            |       | D     |                                     |      | D    |         |
| Intersection Summary   |  |  |                   |       |                  |            |       |       |                                     |      |      |         |
| HCM Average Control Delay  |  |  | 31.4              | H     | CM Level         | of Service | Э     |       | С                                   |      |      | <u></u> |
| HCM Volume to Capacity ratio   |  |  | 0.68              |       |                  |            |       |       |                                     |      |      |         |
| Actuated Cycle Length (s)  |  |  | 90.0              | Su    | um of lost       | time (s)   |       |       | 24.0                                |      |      |         |
| Intersection Capacity Utilization  |  |  | 66.1%             | IC    | U Level o        | f Service  |       |       | С                                   |      |      |         |
| Analysis Period (min)  |  |  | 15                |       |                  |            |       |       |                                     |      |      |         |
| c Critical Lane Group  |  |  |                   |       |                  |            |       |       |                                     |      |      |         |

|  | ٨                      |         | >     | *          |           | s.               | ٦                                      | Ť        | p                           | \$             | Ť    | $\checkmark$ |
|--|------------------------|---------|-------|------------|-----------|------------------|--|----------|-----------------------------|----------------|------|--------------|
| Movement                                       | EBL                    | EBT     | EBR   | WBL        | WBT       | WBR              | NBL                                    | NBT      | NBR                         | SBL            | SBT  | SBR          |
| Lane Configurations                            | ሻ                      | <u></u> |       | ሻ          | 个         | ศั               | ሻ                                      | <b>4</b> |                             | ሻ              | \$   |              |
| Volume (vph)                                   | 14                     | 855     | 15    | 79         | 852       | 362              | 39                                     | 50       | 170                         | 268            | 98   | 44           |
| Ideal Flow (vphpl)                             | 2000                   | 2000    | 2000  | 2000       | 2000      | 2000             | 2000                                   | 2000     | 2000                        | 2000           | 2000 | 2000         |
| Total Lost time (s)                            | 6.1                    | 6.1     |       | 6.1        | 6.1       | 6.1              | 6.0                                    | 6.0      |                             | 6.0            | 6.0  |              |
| Lane Util. Factor                              | 1.00                   | 0.95    |       | 1.00       | 1.00      | 1.00             | 1.00                                   | 1.00     |                             | 1.00           | 1.00 |              |
| Frt  | 1.00                   | 1.00    |       | 1.00       | 1.00      | 0.85             | 1.00                                   | 0.88     |                             | 1.00           | 0.95 |              |
| Fit Protected                                  | 0.95                   | 1.00    |       | 0.95       | 1.00      | 1.00             | 0.95                                   | 1.00     |                             | 0.95           | 1.00 |              |
| Satd. Flow (prot)                              | 1863                   | 3716    |       | 1863       | 1961      | 1500             | 1863                                   | 1733     |                             | 1863           | 1870 |              |
| Flt Permitted                                  | 0.09                   | 1.00    |       | 0.22       | 1.00      | 1.00             | 0.66                                   | 1.00     |                             | 0.56           | 1.00 |              |
| Satd. Flow (perm)                              | 167                    | 3716    |       | 430        | 1961      | 1500             | 1291                                   | 1733     |                             | 1093           | 1870 |              |
| Peak-hour factor, PHF                          | 0.88                   | 0.88    | 0.88  | 0.92       | 0.92      | 0.92             | 0.94                                   | 0.94     | 0.94                        | 0.92           | 0.92 | 0.92         |
| Adj. Flow (vph)                                | 16                     | 972     | 17    | 86         | 926       | 393              | 41                                     | 53       | 181                         | 291            | 107  | 48           |
| RTOR Reduction (vph)                           | 0                      | 1       | 0     | 0          | 0         | 187              | 0                                      | 0        | 0                           | 0              | 18   | 0            |
| Lane Group Flow (vph)                          | 16                     | 988     | 0     | 86         | 926       | 206              | 41                                     | 234      | 0                           | 291            | 137  | 0            |
| Parking (#/hr)                                 |                        |         | 0     |            |           | 0                |  |          |                             |                |      |              |
| Turn Type                                      | Perm                   |         |       | Perm       |           | Perm             | Perm                                   |          |                             | Perm           |      |              |
| Protected Phases                               |                        | 2       |       |            | 6         | A - MARA waxaali |  | 8        |                             |                | 4    |              |
| Permitted Phases                               | 2                      |         |       | 6          |           | 6                | 8                                      |          |                             | 4              |      |              |
| Actuated Green, G (s)                          | 46.9                   | 46.9    |       | 46.9       | 46.9      | 46.9             | 31.0                                   | 31.0     |                             | 31.0           | 31.0 |              |
| Effective Green, g (s)                         | 46.9                   | 46.9    |       | 46.9       | 46.9      | 46.9             | 31.0                                   | 31.0     |                             | 31.0           | 31.0 |              |
| Actuated g/C Ratio                             | 0.52                   | 0.52    |       | 0.52       | 0.52      | 0.52             | 0.34                                   | 0.34     |                             | 0.34           | 0.34 |              |
| Clearance Time (s)                             | 6.1                    | 6.1     |       | 6.1        | 6.1       | 6.1              | 6.0                                    | 6.0      |                             | 6.0            | 6.0  |              |
| Lane Grp Cap (vph)                             | 87                     | 1936    |       | 224        | 1022      | 782              | 445                                    | 597      |                             | 376            | 644  |              |
| v/s Ratio Prot                                 |                        | 0.27    |       |            | c0.47     |                  |  | 0.14     |                             |                | 0.07 |              |
| v/s Ratio Perm                                 | 0.10                   |         |       | 0.20       |           | 0.14             | 0.03                                   |          |                             | c0.27          |      |              |
| v/c Ratio                                      | 0.18                   | 0.51    |       | 0.38       | 0.91      | 0.26             | 0.09                                   | 0.39     |                             | 0.77           | 0.21 |              |
| Uniform Delay, d1                              | 11.4                   | 14.1    |       | 12.9       | 19.6      | 12.0             | 20.0                                   | 22.4     |                             | 26.4           | 20.9 |              |
| Progression Factor                             | 0.83                   | 0.95    |       | 1.00       | 1.00      | 1.00             | 1.00                                   | 1.00     |                             | 1.00           | 1.00 |              |
| Incremental Delay, d2                          | 4.5                    | 0.9     |       | 4.9        | 13.0      | 0.8              | 0.4                                    | 1.9      |                             | 14.4           | 0.8  |              |
| Delay (s)                                      | 14.0                   | 14.3    |       | 17.8       | 32.5      | 12.8             | 20.4                                   | 24.3     |                             | 40.7           | 21.6 |              |
| Level of Service                               | В                      | В       |       | В          | С         | В                | С                                      | С        |                             | D              | С    |              |
| Approach Delay (s)                             |                        | 14.3    |       |            | 26.1      |                  |  | 23.7     |                             |                | 34.1 |              |
| Approach LOS                                   | , bé sanis da ani i da | В       |       |            | С         |                  | 1 - 11 - 11 - 11 - 11 - 11 - 11 - 11 - | С        | . 996 - Ale Versey (1997) - | s construction | С    |              |
| Intersection Summary                           |                        |         |       |            |           |                  |  |          |                             |                |      |              |
| HCM Average Control Dela                       | у                      |         | 23.2  | H          | CM Level  | of Servic        | e                                      |          | С                           |                |      |              |
| HCM Volume to Capacity ra                      | atio                   |         | 0.85  |            |           |                  |  |          |                             |                |      |              |
| ctuated Cycle Length (s) S                     |                        | 90.0    |       | um of lost |           |                  | 12.1                                   |          |                             |                |      |              |
| Intersection Capacity Utiliza                  | ntion                  |         | 97.6% | IC         | U Level o | of Service       |  |          | F                           |                |      |              |
| Analysis Period (min)<br>c Critical Lane Group |                        |         | 15    |            |           |                  |  |          |                             |                |      |              |

|                               | ≯                        | $\mathbf{i}$ | *     | Î                    | Ļ                                       | 4          |  |
|-------------------------------|--------------------------|--------------|-------|----------------------|---|------------|--|
| Movement                      | EBL                      | EBR          | NBL   | NBT                  | SBT                                     | SBR        |  |
| Lane Configurations           | k                        | 7            |       | <del>م</del> î ל     | 个                                       | ۲          |  |
| Volume (vph)                  | 276                      | 100          | 105   | 459                  | 786                                     | 118        |  |
| Ideal Flow (vphpl)            | 2000                     | 2000         | 2000  | 2000                 | 2000                                    | 2000       |  |
| Total Lost time (s)           | 6.0                      | 6.0          |       | 6.6                  | 6.6                                     | 6.6        |  |
| Lane Util. Factor             | 1.00                     | 1.00         |       | 0.95                 | 1.00                                    | 1.00       | e o estas e estas dente la decensión de la calactería de la defensión de la decensión de la defensión de la de<br>La defensión   |
| Frt                           | 1.00                     | 0.85         |       | 1.00                 | 1.00                                    | 0.85       |  |
| Flt Protected                 | 0.95                     | 1.00         |       | 0.99                 | 1.00                                    | 1.00       |  |
| Satd. Flow (prot)             | 1863                     | 1667         |       | 3691                 | 1961                                    | 1667       |  |
| Flt Permitted                 | 0.95                     | 1.00         |       | 0.59                 | 1.00                                    | 1.00       |  |
| Satd. Flow (perm)             | 1863                     | 1667         |       | 2197                 | 1961                                    | 1667       |  |
| Peak-hour factor, PHF         | 0.92                     | 0.92         | 0.92  | 0.92                 | 0.92                                    | 0.92       |  |
| Adj. Flow (vph)               | 300                      | 109          | 114   | 499                  | 854                                     | 128        |  |
| RTOR Reduction (vph)          | 0                        | 86           | 0     | 0                    | 0                                       | 45         | er en alle al alle a ser en dat definitetististe annet Verlaet Direktern titte. En atte  |
| Lane Group Flow (vph)         | 300                      | 23           | Ō     | 613                  | 854                                     | 83         |  |
| Turn Type                     |                          | Perm         | Perm  |                      | - 100 - 11 - 11 - 11 - 11 - 11 - 11 - 1 | Perm       |  |
| Protected Phases              | 4                        |              |       | 2                    | 6                                       |            |  |
| Permitted Phases              | a dha an tao bita filita | 4            | 2     | an an an an Arraight |   | 6          | aan da sa sanaa da bahan da bahan na da baba da bada da baban da yeen na baran da bada bada bada bada bada bad<br>Baban  |
| Actuated Green, G (s)         | 18.7                     | 18.7         |       | 58.7                 | 58.7                                    | 58.7       |  |
| Effective Green, g (s)        | 18.7                     | 18.7         |       | 58.7                 | 58.7                                    | 58.7       |  |
| Actuated g/C Ratio            | 0.21                     | 0.21         |       | 0.65                 | 0.65                                    | 0.65       |  |
| Clearance Time (s)            | 6.0                      | 6.0          |       | 6.6                  | 6.6                                     | 6.6        | en an de la secte de la regel de la companya de la secte de la<br>La companya de la comp   |
| Vehicle Extension (s)         | 3.0                      | 3.0          |       | 3.0                  | 3.0                                     | 3.0        |  |
| ane Grp Cap (vph)             | 387                      | 346          |       | 1433                 | 1279                                    | 1087       | an a   |
| //s Ratio Prot                | c0.16                    |              |       |                      | c0.44                                   |            |  |
| //s Ratio Perm                |                          | 0.01         |       | 0.28                 |   | 0.05       |  |
| ı/c Ratio                     | 0.78                     | 0.07         |       | 0.43                 | 0.67                                    | 0.08       |  |
| Jniform Delay, d1             | 33.7                     | 28.6         |       | 7.5                  | 9.6                                     | 5.7        |  |
| Progression Factor            | 1.00                     | 1.00         |       | 1.00                 | 1.10                                    | 1.18       |  |
| ncremental Delay, d2          | 9.4                      | 0.1          |       | 0.9                  | 2.4                                     | 0.1        |  |
| Delay (s)                     | 43.0                     | 28.7         |       | 8.5                  | 13.0                                    | 6.9        |  |
| evel of Service               | D                        | С            |       | А                    | В                                       | А          | o na sana a sana ing kana ing kana sa na sana kana kana kana kana kan  |
| Approach Delay (s)            | 39.2                     |              |       | 8.5                  | 12.2                                    |            |  |
| Approach LOS                  | D                        |              |       | А                    | В                                       |            |  |
| ntersection Summary           |                          |              |       |                      |   |            |  |
| CM Average Control Delay      | ,                        |              | 16.6  | н                    | CM Level                                | of Service | В  |
| ICM Volume to Capacity rat    |                          |              | 0.69  |                      |   |            |  |
| ctuated Cycle Length (s)      | ne state i state         |              | 90.0  | Su                   | im of lost                              | time (s)   | 12.6   |
| ntersection Capacity Utilizat | ion                      |              | 84.8% |                      | U Level o                               |            | E  |
| analysis Period (min)         |                          |              | 15    |                      |   |            | e is secondestination for the first of the f |
| Critical Lane Group           |                          |              | IJ    |                      |   |            |  |

|                               | ٨     | <b></b> > | $\mathbf{i}$  | *     | <b>4</b>   | ×.                   | ٩                   | Î     | p                     | \$               | ţ.       | 4            |
|-------------------------------|-------|-----------|---------------|-------|------------|----------------------|---------------------|-------|-----------------------|------------------|----------|--------------|
| Movement                      | EBL   | EBT       | EBR           | WBL   | WBT        | WBR                  | NBL                 | NBT   | NBR                   | SBL              | SBT      | SBR          |
| Lane Configurations           | ሻ     | 个         | ۴             | ×,    | ĥ          |                      | ሻ                   | ĥ     |                       | ሻ                | <u>م</u> | <b>آ</b> م   |
| Volume (vph)                  | 158   | 169       | 184           | 134   | 75         | 11                   | 158                 | 434   | 53                    | 2                | 494      | 32           |
| Ideal Flow (vphpl)            | 2000  | 2000      | 2000          | 2000  | 2000       | 2000                 | 2000                | 2000  | 2000                  | 2000             | 2000     | 2000         |
| Total Lost time (s)           | 4.0   | 6.1       | 6.1           | 4.0   | 6.1        |                      | 4.0                 | 5.9   |                       | 5.9              | 5.9      | 5.9          |
| Lane Util. Factor             | 1.00  | 1.00      | 1.00          | 1.00  | 1.00       |                      | 1.00                | 1.00  |                       | 1.00             | 1.00     | 1.00         |
| Frt                           | 1.00  | 1.00      | 0.85          | 1.00  | 0.98       |                      | 1.00                | 0.98  |                       | 1.00             | 1.00     | 0.85         |
| Flt Protected                 | 0.95  | 1.00      | 1.00          | 0.95  | 1.00       |                      | 0.95                | 1.00  |                       | 0.95             | 1.00     | 1.00         |
| Satd. Flow (prot)             | 1881  | 1923      | 1504          | 1845  | 1881       |                      | 1652                | 1924  |                       | 1900             | 1961     | 1650         |
| Flt Permitted                 | 0.53  | 1.00      | 1.00          | 0.59  | 1.00       |                      | 0.23                | 1.00  | is i Shirin ma'i      | 0.22             | 1.00     | 1.00         |
| Satd. Flow (perm)             | 1045  | 1923      | 1504          | 1145  | 1881       |                      | 397                 | 1924  |                       | 434              | 1961     | 1650         |
| Peak-hour factor, PHF         | 0.81  | 0.81      | 0.81          | 0.73  | 0.73       | 0.73                 | 0.74                | 0.74  | 0.74                  | 0.84             | 0.84     | 0.84         |
| Adj. Flow (vph)               | 195   | 209       | 227           | 184   | 103        | 15                   | 214                 | 586   | 72                    | 2                | 588      | 38           |
| RTOR Reduction (vph)          | 0     | 0         | 130           | 0     | 6          | 0                    | 0                   | 5     | 0                     | 0                | 0        | 18           |
| Lane Group Flow (vph)         | 195   | 209       | 97            | 184   | 112        | Ō                    | 214                 | 653   | Ō                     | 2                | 588      | 20           |
| Heavy Vehicles (%)            | 1%    | 4%        | 13%           | 3%    | 2%         | 20%                  | 15%                 | 2%    | 4%                    | 0%               | 2%       | 3%           |
| Turn Type                     | pm+pt |           | Perm          | pm+pt |            |                      | pm+pt               |       |                       | Perm             |          | Perm         |
| Protected Phases              | 7     | 4         |               | 3     | 8          |                      | 5                   | 2     |                       | And Anti-Anti-Ad | 6        | ANG GUTAANG  |
| Permitted Phases              | 4     |           | 4             | 8     |            |                      | 2                   |       |                       | 6                |          | 6            |
| Actuated Green, G (s)         | 27.2  | 14.2      | 14.2          | 20.8  | 11.0       |                      | 51.9                | 50.0  |                       | 36.0             | 36.0     | 36.0         |
| Effective Green, g (s)        | 27.2  | 14.2      | 14.2          | 20.8  | 11.0       |                      | 51.9                | 50.0  |                       | 36.0             | 36.0     | 36.0         |
| Actuated g/C Ratio            | 0.30  | 0.16      | 0.16          | 0.23  | 0.12       |                      | 0.58                | 0.56  |                       | 0.40             | 0.40     | 0.40         |
| Clearance Time (s)            | 4.0   | 6.1       | 6.1           | 4.0   | 6.1        |                      | 4.0                 | 5.9   |                       | 5.9              | 5.9      | 5.9          |
| Vehicle Extension (s)         | 3.0   | 3.0       | 3.0           | 3.0   | 3.0        |                      | 3.0                 | 3.0   |                       | 3.0              | 3.0      | 3.0          |
| Lane Grp Cap (vph)            | 437   | 303       | 237           | 341   | 230        |                      | 368                 | 1069  |                       | 174              | 784      | 660          |
| v/s Ratio Prot                | c0.06 | c0.11     |               | c0.06 | 0.06       |                      | 0.06                | c0.34 |                       | u, hi ya dhaa    | c0.30    |              |
| v/s Ratio Perm                | 0.07  |           | 0.06          | 0.07  |            |                      | 0.27                |       |                       | 0.00             |          | 0.01         |
| v/c Ratio                     | 0.45  | 0.69      | 0.41          | 0.54  | 0.49       |                      | 0.58                | 0.61  |                       | 0.01             | 0.75     | 0.03         |
| Uniform Delay, d1             | 24.5  | 35.8      | 34.1          | 29.6  | 36.9       |                      | 26.1                | 13.5  |                       | 16.3             | 23.1     | 16.4         |
| Progression Factor            | 1.00  | 1.00      | 1.00          | 1.00  | 1.00       |                      | 1.19                | 1.19  |                       | 0.76             | 0.82     | 0.62         |
| Incremental Delay, d2         | 0.7   | 6.4       | 1.2           | 1.6   | 1.6        |                      | 2.2                 | 2.4   |                       | 0.1              | 6.5      | 0.1          |
| Delay (s)                     | 25.2  | 42.2      | 35.3          | 31.2  | 38.5       |                      | 33.1                | 18.4  |                       | 12.5             | 25.4     | 10.3         |
| Level of Service              | <br>C | D         | D             | C     | D          |                      | C                   | В     |                       | В                | C        | В            |
| Approach Delay (s)            |       | 34.5      | 19. C. STELES | 1     | 34.0       |                      |                     | 22.0  |                       | ta Midala Tarra  | 24.4     | an drift.    |
| Approach LOS                  |       | C         |               |       | C          |                      |                     | C     |                       |                  | <br>C    |              |
| Intersection Summary          |       |           |               |       |            |                      |                     |       |                       |                  |          |              |
| HCM Average Control Dela      | ay    |           | 27.4          | H     | CM Level   | of Servic            | е                   |       | С                     |                  |          |              |
| HCM Volume to Capacity ra     |       |           | 0.64          |       |            | a dan basar di Tabib | er und Phile Albert |       | an an an tri Fasiliri |                  |          | energene dil |
| Actuated Cycle Length (s)     |       |           | 90.0          | Sı    | um of lost | time (s)             |                     |       | 13.9                  |                  |          |              |
| Intersection Capacity Utiliza | ation |           | 68.0%         |       | U Level o  |                      |                     |       | С                     |                  |          |              |
| Analysis Period (min)         |       |           | 15            |       |            |                      |                     |       |                       |                  |          |              |
| a Critical Lana Crown         |       |           | - 81 CAR 51 C |       |            |                      |                     |       |                       |                  |          |              |

|                                   | ٨    | <b></b> þ | $\mathbf{k}$ | ×.    | 4          | Ł          | ٩    | Î    | P    | 1    | Å.    | *    |
|-----------------------------------|------|-----------|--------------|-------|------------|------------|------|------|------|------|-------|------|
| Movement                          | EBL  | EBT       | EBR          | WBL   | WBT        | WBR        | NBL  | NBT  | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | ٣    | f         |              | ×.    | Å          |            | ሻ    | Ŷ    |      | ۲.   | ŕ     | ř    |
| Volume (vph)                      | 11   | 11        | 89           | 44    | 11         | 11         | 22   | 308  | 66   | 11   | 385   | 11   |
| Ideal Flow (vphpl)                | 1900 | 1900      | 1900         | 1900  | 1900       | 1900       | 1900 | 1900 | 1900 | 1900 | 1900  | 1900 |
| Total Lost time (s)               | 5.8  | 5.8       |              | 5.8   | 5.8        |            | 5.8  | 5.8  |      | 5.8  | 5.8   | 5.8  |
| Lane Util. Factor                 | 1.00 | 1.00      |              | 1.00  | 1.00       |            | 1.00 | 1.00 |      | 1.00 | 1.00  | 1.00 |
| Frt                               | 1.00 | 0.87      |              | 1.00  | 0.92       |            | 1.00 | 0.97 |      | 1.00 | 1.00  | 0.85 |
| Flt Protected                     | 0.95 | 1.00      |              | 0.95  | 1.00       |            | 0.95 | 1.00 |      | 0.95 | 1.00  | 1.00 |
| Satd. Flow (prot)                 | 1770 | 1614      |              | 1770  | 1723       |            | 1770 | 1813 |      | 1770 | 1863  | 1583 |
| Flt Permitted                     | 0.74 | 1.00      |              | 0.69  | 1.00       |            | 0.52 | 1.00 |      | 0.52 | 1.00  | 1.00 |
| Satd. Flow (perm)                 | 1381 | 1614      |              | 1279  | 1723       |            | 964  | 1813 |      | 974  | 1863  | 1583 |
| Peak-hour factor, PHF             | 0.92 | 0.92      | 0.92         | 0.92  | 0.92       | 0.92       | 0.92 | 0.92 | 0.92 | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)                   | 12   | 12        | 97           | 48    | 12         | 12         | 24   | 335  | 72   | 12   | 418   | 12   |
| RTOR Reduction (vph)              | 0    | 89        | 0            | 0     | 11         | 0          | 0    | 4    | 0    | 0    | 0     | 3    |
| Lane Group Flow (vph)             | 12   | 20        | 0            | 48    | 13         | 0          | 24   | 403  | 0    | 12   | 418   | 9    |
| Turn Type                         | Perm |           |              | Perm  |            |            | Perm |      |      | Perm |       | Perm |
| Protected Phases                  |      | 4         |              |       | 8          |            |      | 2    |      |      | 6     |      |
| Permitted Phases                  | 4    |           |              | 8     |            |            | 2    |      |      | 6    |       | 6    |
| Actuated Green, G (s)             | 7.8  | 7.8       |              | 7.8   | 7.8        |            | 70.6 | 70.6 |      | 70.6 | 70.6  | 70.6 |
| Effective Green, g (s)            | 7.8  | 7.8       |              | 7.8   | 7.8        |            | 70.6 | 70.6 |      | 70.6 | 70.6  | 70.6 |
| Actuated g/C Ratio                | 0.09 | 0.09      |              | 0.09  | 0.09       |            | 0.78 | 0.78 |      | 0.78 | 0.78  | 0.78 |
| Clearance Time (s)                | 5.8  | 5.8       |              | 5.8   | 5.8        |            | 5.8  | 5.8  |      | 5.8  | 5.8   | 5.8  |
| Vehicle Extension (s)             | 3.0  | 3.0       |              | 3.0   | 3.0        |            | 3.0  | 3.0  |      | 3.0  | 3.0   | 3.0  |
| Lane Grp Cap (vph)                | 120  | 140       |              | 111   | 149        |            | 756  | 1422 |      | 764  | 1461  | 1242 |
| v/s Ratio Prot                    |      | 0.01      |              |       | 0.01       |            |      | 0.22 |      |      | c0.22 |      |
| v/s Ratio Perm                    | 0.01 |           |              | c0.04 |            |            | 0.02 |      |      | 0.01 |       | 0.01 |
| v/c Ratio                         | 0.10 | 0.15      |              | 0,43  | 0.09       |            | 0.03 | 0.28 |      | 0.02 | 0.29  | 0.01 |
| Uniform Delay, d1                 | 37.9 | 38.0      |              | 39.0  | 37.8       |            | 2.1  | 2.7  |      | 2.1  | 2.7   | 2.1  |
| Progression Factor                | 1.00 | 1.00      |              | 1.00  | 1.00       |            | 0.58 | 0.67 |      | 0.72 | 0.60  | 0.76 |
| Incremental Delay, d2             | 0.4  | 0.5       |              | 2.7   | 0.3        |            | 0.1  | 0.4  |      | 0.0  | 0.4   | 0.0  |
| Delay (s)                         | 38.2 | 38.5      |              | 41.7  | 38.1       |            | 1,3  | 2.3  |      | 1.6  | 2.0   | 1.6  |
| Level of Service                  | D    | D         |              | D     | D          |            | А    | А    |      | А    | А     | А    |
| Approach Delay (s)                |      | 38.5      |              |       | 40.5       |            |      | 2.2  |      |      | 2.0   |      |
| Approach LOS                      |      | D         |              |       | D          |            |      | А    |      |      | А     |      |
| Intersection Summary              |      |           |              |       |            |            |      |      |      |      |       |      |
| HCM Average Control Delay         |      |           | 8.8          | H     | CM Level   | of Service | Э    |      | А    |      |       |      |
| HCM Volume to Capacity ratio      |      |           | 0.30         |       |            |            |      |      |      |      |       |      |
| Actuated Cycle Length (s)         |      |           | 90.0         |       | im of lost |            |      |      | 11.6 |      |       |      |
| Intersection Capacity Utilization | 1    |           | 39.0%        | IC    | U Level o  | f Service  |      |      | Α    |      |       |      |
| Analysis Period (min)             |      |           | 15           |       |            |            |      |      |      |      |       |      |
| c Critical Lane Group             |      |           |              |       |            |            |      |      |      |      |       |      |

|  | A               |            | ~           | 1                        | -¢         | *                      | ٩     | Ť            | p    | \$                    | Ť     | ~            |
|--|-----------------|------------|-------------|--------------------------|------------|------------------------|-------|--------------|------|-----------------------|-------|--------------|
| Movement   | EBL             | EBT        | EBR         | WBL                      | WBT        | WBR                    | NBL   | NBT          | NBR  | SBL                   | SBT   | SBR          |
| Lane Configurations  | ሻ               | <b>∱</b> ኈ |             | ሻ                        | <b>ሶ</b> ኈ |                        | ሻ     | ኈ            |      | 5                     | Â     |              |
| Volume (vph)   | 19              | 437        | 65          | 64                       | 456        | 12                     | 62    | 151          | 95   | 44                    | 267   | 10           |
| Ideal Flow (vphpl)   | 2000            | 2000       | 2000        | 2000                     | 2000       | 2000                   | 2000  | 2000         | 2000 | 2000                  | 2000  | 2000         |
| Total Lost time (s)  | 6.0             | 6.0        |             | 6.0                      | 6,0        |                        | 6.0   | 6.0          |      | 6.0                   | 6.0   |              |
| Lane Util. Factor  | 1.00            | 0.95       |             | 1.00                     | 0.95       |                        | 1.00  | 1.00         |      | 1.00                  | 1.00  |              |
| Frt  | 1.00            | 0.98       |             | 1.00                     | 1.00       |                        | 1.00  | 0.94         |      | 1.00                  | 0.99  |              |
| Flt Protected  | 0.95            | 1.00       |             | 0.95                     | 1.00       |                        | 0.95  | 1.00         |      | 0.95                  | 1.00  |              |
| Satd. Flow (prot)  | 1863            | 3653       |             | 1863                     | 3711       |                        | 1863  | 1847         |      | 1863                  | 1950  |              |
| FIt Permitted  | 0.95            | 1.00       |             | 0.95                     | 1.00       |                        | 0.95  | 1.00         |      | 0.95                  | 1.00  |              |
| Satd. Flow (perm)  | 1863            | 3653       |             | 1863                     | 3711       | 경망감독                   | 1863  | 1847         |      | 1863                  | 1950  |              |
| Peak-hour factor, PHF  | 0.79            | 0.79       | 0.79        | 0.70                     | 0.70       | 0.70                   | 0.95  | 0.95         | 0.95 | 0.81                  | 0.81  | 0.81         |
| Adj. Flow (vph)  | 24              | 553        | 82          | 91                       | 651        | 17                     | 65    | 159          | 100  | 54                    | 330   | 12           |
| RTOR Reduction (vph)   | 0               | 11         | 0           | 0                        | 2          | 0                      | 0     | 27           | 0    | 0                     | 2     | 0            |
| Lane Group Flow (vph)  | 24              | 624        | 0           | 91                       | 666        | 0                      | 65    | 232          | 0    | 54                    | 340   | 0            |
| Turn Type  | Prot            |            |             | Prot                     |            |                        | Prot  |              | i,,, | Prot                  |       |              |
| Protected Phases   | 5               | 2          |             | 1                        | 6          |                        | 3     | 8            |      | 7                     | 4     |              |
| Permitted Phases   |                 |            |             |                          |            |                        |       |              |      |                       |       |              |
| Actuated Green, G (s)  | 3.1             | 32.6       |             | 7.3                      | 36.8       |                        | 5.6   | 20.5         |      | 5.6                   | 20.5  |              |
| Effective Green, g (s)   | 3.1             | 32.6       |             | 7.3                      | 36.8       |                        | 5.6   | 20.5         |      | 5.6                   | 20.5  |              |
| Actuated g/C Ratio   | 0.03            | 0.36       |             | 0.08                     | 0.41       |                        | 0.06  | 0.23         |      | 0.06                  | 0.23  |              |
| Clearance Time (s)   | 6.0             | 6.0        |             | 6.0                      | 6.0        | and francisca and defi | 6.0   | 6.0          |      | 6.0                   | 6.0   |              |
| Vehicle Extension (s)  | 3.0             | 3.0        |             | 3.0                      | 3.0        |                        | 3.0   | 3.0          |      | 3.0                   | 3.0   |              |
| Lane Grp Cap (vph)   | 64              | 1323       |             | 151                      | 1517       |                        | 116   | 421          |      | 116                   | 444   |              |
| v/s Ratio Prot   | 0.01            | 0.17       |             | c0.05                    | c0.18      |                        | c0.03 | 0.13         |      | 0.03                  | c0.17 |              |
| v/s Ratio Perm   |                 |            |             | 12.177.77.27.27.77.77.47 |            |                        |       | ran Sili Car |      |                       |       |              |
| v/c Ratio  | 0.38            | 0.47       |             | 0.60                     | 0.44       |                        | 0.56  | 0.55         |      | 0.47                  | 0.77  |              |
| Uniform Delay, d1  | 42.5            | 22.1       |             | 39.9                     | 19.2       |                        | 41.0  | 30.7         |      | 40.8                  | 32.5  |              |
| Progression Factor   | 1.00            | 1.00       |             | 0.82                     | 0.87       |                        | 0.98  | 0.80         |      | 1.00                  | 1.00  |              |
| Incremental Delay, d2  | 3.7             | 1.2        |             | 5.7                      | 0.8        |                        | 5.9   | 1.5          |      | 2.9                   | 7.7   |              |
| Delay (s)  | 46.2            | 23.3       |             | 38.4                     | 17.4       |                        | 46.2  | 26.1         |      | 43.7                  | 40.3  |              |
| Level of Service   | D               | С          |             | D                        | В          |                        | D     | С            |      | D                     | D     |              |
| Approach Delay (s)   |                 | 24.1       |             |                          | 19.9       |                        |       | 30.1         |      |                       | 40.7  |              |
| Approach LOS   | A Grad Labela A | С          |             | un de structur de se     | В          | a De Nordelando.       |       | С            |      | alan ya santan alia i | D     | lite teste a |
| Intersection Summary   |                 |            |             |                          |            |                        |       |              |      |                       |       |              |
| HCM Average Control Delay  |                 |            | 26.6        | Н                        | CM Level   | of Servic              | е     |              | С    |                       |       |              |
| HCM Volume to Capacity ratio   |                 |            | 0.59        |                          |            |                        |       |              |      |                       |       |              |
| Actuated Cycle Length (s)  |                 |            | 90.0        |                          | um of lost |                        |       |              | 24.0 |                       |       |              |
| Intersection Capacity Utilizatio<br>Analysis Period (min)<br>c Critical Lane Group | n               |            | 59.0%<br>15 |                          | CU Level c |                        |       |              | В    |                       |       |              |

|                                   | <u>_</u>                                      |      | Ý                 | <b>*</b>       | <b>«</b> — | ×.                    | ٩  | Ť                 | p                     | 6                      | ↓<br>₩ | 4                                     |
|-----------------------------------|---|------|-------------------|----------------|------------|-----------------------|--|-------------------|-----------------------|------------------------|--------|---------------------------------------|
| Movement                          | EBL   | EBT  | EBR               | WBL            | WBT        | WBR                   | NBL  | NBT               | NBR                   | SBL                    | SBT    | SBR                                   |
| Lane Configurations               | ኻ   | ♠₽   |                   | ኻ              | ŕ          | 7                     | ሻ  | ¢î                |                       | ኻ                      | eî     |                                       |
| Volume (vph)                      | 4   | 698  | 7                 | 60             | 699        | 116                   | 8  | 13                | 158                   | 182                    | 21     | 10                                    |
| ldeal Flow (vphpl)                | 2000  | 2000 | 2000              | 2000           | 2000       | 2000                  | 2000   | 2000              | 2000                  | 2000                   | 2000   | 2000                                  |
| Total Lost time (s)               | 6.1   | 6.1  |                   | 6.1            | 6.1        | 6.1                   | 6.0  | 6.0               |                       | 6.0                    | 6.0    |                                       |
| Lane Util. Factor                 | 1.00  | 0.95 |                   | 1.00           | 1.00       | 1.00                  | 1.00   | 1.00              |                       | 1.00                   | 1.00   |                                       |
| Frt                               | 1.00  | 1.00 |                   | 1.00           | 1.00       | 0.85                  | 1.00   | 0.86              |                       | 1.00                   | 0.95   |                                       |
| Flt Protected                     | 0.95  | 1.00 |                   | 0.95           | 1.00       | 1.00                  | 0.95   | 1.00              |                       | 0.95                   | 1.00   |                                       |
| Satd. Flow (prot)                 | 1863  | 3720 |                   | 1863           | 1961       | 1500                  | 1863   | 1690              |                       | 1863                   | 1868   |                                       |
| Flt Permitted                     | 0.19  | 1.00 |                   | 0.27           | 1.00       | 1.00                  | 0.73   | 1.00              |                       | 0.56                   | 1.00   |                                       |
| Satd. Flow (perm)                 | 366   | 3720 |                   | 524            | 1961       | 1500                  | 1432   | 1690              |                       | 1098                   | 1868   |                                       |
| Peak-hour factor, PHF             | 0.76  | 0.76 | 0.76              | 0.83           | 0.83       | 0.83                  | 0.83   | 0.83              | 0.83                  | 0.75                   | 0.75   | 0.75                                  |
| Adj. Flow (vph)                   | 5   | 918  | 9                 | 72             | 842        | 140                   | 10   | 16                | 190                   | 243                    | 28     | 13                                    |
| RTOR Reduction (vph)              | 0   | 1    | 0                 | 0              | 0          | 56                    | 0  | 0                 | 0                     | 0                      | 10     | 0                                     |
| Lane Group Flow (vph)             | 5   | 926  | 0                 | 72             | 842        | 84                    | 10   | 206               | 0                     | 243                    | 31     | 0                                     |
| Parking (#/hr)                    |   |      | 0                 |                |            | 0                     |  |                   |                       | n dangan sajar kabudan |        |                                       |
| Turn Type                         | Perm  |      |                   | Perm           |            | Perm                  | Perm   |                   |                       | Perm                   |        |                                       |
| Protected Phases                  |   | 2    |                   |                | 6          |                       | ardan Arranalan a                                | 8                 |                       |                        | 4      |                                       |
| Permitted Phases                  | 2   |      |                   | 6              |            | 6                     | 8  |                   |                       | 4                      |        |                                       |
| Actuated Green, G (s)             | 54.3  | 54.3 |                   | 54.3           | 54.3       | 54.3                  | 23.6   | 23.6              |                       | 23.6                   | 23.6   |                                       |
| Effective Green, g (s)            | 54.3  | 54.3 |                   | 54.3           | 54.3       | 54.3                  | 23.6   | 23.6              |                       | 23.6                   | 23.6   |                                       |
| Actuated g/C Ratio                | 0.60  | 0.60 |                   | 0.60           | 0.60       | 0.60                  | 0.26   | 0.26              |                       | 0.26                   | 0.26   |                                       |
| Clearance Time (s)                | 6.1   | 6.1  |                   | 6.1            | 6.1        | 6.1                   | 6.0  | 6.0               |                       | 6.0                    | 6.0    |                                       |
| Vehicle Extension (s)             | 3.0   | 3.0  |                   | 3.0            | 3.0        | 3.0                   | 3.0  | 3.0               |                       | 3.0                    | 3.0    |                                       |
| Lane Grp Cap (vph)                | 221   | 2244 |                   | 316            | 1183       | 905                   | 376  | 443               |                       | 288                    | 490    |                                       |
| v/s Ratio Prot                    | na dhe ta | 0.25 |                   |                | c0.43      |                       |  | 0.12              |                       |                        | 0.02   |                                       |
| v/s Ratio Perm                    | 0.01  |      |                   | 0.14           |            | 0.06                  | 0.01   |                   |                       | c0.22                  |        |                                       |
| v/c Ratio                         | 0.02  | 0.41 |                   | 0.23           | 0.71       | 0.09                  | 0.03   | 0.47              |                       | 0.84                   | 0.06   |                                       |
| Uniform Delay, d1                 | 7.2   | 9.4  |                   | 8.2            | 12.4       | 7.5                   | 24.7   | 27.9              |                       | 31.5                   | 24.9   |                                       |
| Progression Factor                | 0.59  | 0.80 |                   | 1.00           | 1.00       | 1.00                  | 1.00   | 1.00              | e e c'h de dé de te e | 1.00                   | 1.00   |                                       |
| Incremental Delay, d2             | 0.2   | 0.5  |                   | 1.7            | 3.7        | 0.2                   | 0.0  | 0.8               |                       | 19.6                   | 0.1    |                                       |
| Delay (s)                         | 4.4   | 8.1  |                   | 9.9            | 16.1       | 7.7                   | 24.7   | 28.7              |                       | 51.1                   | 25.0   | · · · · · · · · · · · · · · · · · · · |
| Level of Service                  | Α   | Α    |                   | Α              | В          | Α                     | С  | С                 |                       | D                      | С      |                                       |
| Approach Delay (s)                |   | 8.0  |                   |                | 14.5       |                       |  | 28.5              |                       |                        | 47.3   |                                       |
| Approach LOS                      |   | Α    |                   |                | В          |                       |  | С                 |                       |                        | D      |                                       |
| Intersection Summary              |   |      |                   |                |            |                       |  |                   |                       |                        |        |                                       |
| HCM Average Control Delay         |   |      | 17.1              | Н              | CM Leve    | l of Servic           | е  |                   | В                     |                        |        |                                       |
| HCM Volume to Capacity ratio      |   |      | 0.75              | ti na isandili | 1          | na na kaominin'i Gera | a shekara ka | aan sa wala dhaha | ana ing ing hini ka   |                        |        |                                       |
| Actuated Cycle Length (s)         |   |      | 90.0              | Si             | um of los  | t time (s)            |  |                   | 12.1                  |                        |        |                                       |
| Intersection Capacity Utilization |   |      | 82.0%             |                |            | of Service            |  |                   | D                     |                        |        |                                       |
| Analysis Period (min)             |   |      | 15                |                |            |                       |  |                   |                       |                        |        |                                       |
| c Critical Lano Group             |   |      | 5. S. 1. 1. 17. 1 |                |            |                       |  |                   |                       |                        |        |                                       |

|                                     |   |  | -   | -   |   |  |
|-------------------------------------|---|--|---|---|---|--|
| EBL                                 | EBR   | NBL  | NBT   | SBT   | SBR   |  |
| ኻ                                   | *   |  | <del>ሳ</del> ት  | ዯ   | 7   |  |
| 676                                 | 329   | 75   | 448   | 755   | 178   |  |
| 2000                                | 2000  | 2000   | 2000  | 2000  |   |  |
| 6.0                                 | 6.0   |  | 6.6   | 6.6   | and the second second second second second            |  |
| 1.00                                | 1.00  |  | 0.95  | 1.00  | 1.00  |  |
| 1.00                                | 0.85  |  | 1.00  | 1.00  | 0.85  |  |
| 0.95                                | 1.00  |  | 0.99  | 1.00  | 1.00  |  |
| 1863                                | 1667  |  | 3699  | 1961  | 1667  |  |
| 0.95                                | 1.00  | 1. (A. ) & (A. )   | 0.51  | 1.00  | 1.00  |  |
| 1863                                | 1667  |  | 1895  | 1961  | The second second second second second                |  |
| 0.92                                | 0.92  | 0.92   | 0.92  | 0.92  |   |  |
|                                     |   |  |   |   |   |  |
|                                     |   |  | 0   |   |   |  |
|                                     |   | 0  |   |   |   |  |
|                                     |   | Perm   |   |   |   | Anno ann an an Arthree an Anna |
| 4                                   |   |  | 2   | 6   |   |  |
|                                     | 4   | 2  |   | arehart, i. dik.  | 6   |  |
| 37.3                                | 37.3  |  | 40.1  | 40.1  |   |  |
| and a set of a second second second |   |  |   |   |   |  |
| 0.41                                | 0.41  |  | 0.45  | 0.45  |   |  |
| 6.0                                 | 6.0   |  | 6.6   | 6.6   | 6.6   |  |
| 3.0                                 | 3.0   |  | 3.0   | 3.0   | 3.0   |  |
| 772                                 | 691   |  | 844   | 874   | 743   |  |
| c0.39                               |   |  |   | c0.42   |   |  |
|                                     | 0.18  |  | 0.30  |   | 0.05  |  |
| 0.95                                | 0.44  |  | 0.94dl  | 0.94  | 0.12  |  |
| 25.5                                | 18.9  |  | 19.8  | 23.8  |   |  |
| 1.00                                | 1.00  |  | 1.00  | 0.91  |   |  |
| 21.4                                | 0.5   |  | 4.3   | 14.7  | 0.2   | an easta an sui dheasha anna an an an shear an an anna an an an an an an an an an a                            |
| 46.9                                | 19.3  |  | 24.1  | 36.3  |   |  |
| D                                   | В   |  | С   | D   | В   |  |
| 37.9                                |   |  | 24.1  | 31.5  |   |  |
| D                                   |   |  | С   | С   |   |  |
|                                     |   |  |   |   |   |  |
| ateria di stati di sene da si si    |   | 32.5   | НС  | CM Level  | of Service  | С  |
| )                                   |   | and there is the second of   |   |   |   |  |
| tean. Né teréfei                    |   |  | Su  | m of lost   | time (s)  | 12.6   |
| 'n                                  | 1   |  |   |   |   | G  |
| •••• A 199 199 19                   | an tao kisini<br>T  |  |   |   |   | an an an tha ann an tha an tha tha 1960 an tha                             |
| )                                   | 676<br>2000<br>6.0<br>1.00<br>1.00<br>0.95<br>1863<br>0.95<br>1863<br>0.95<br>1863<br>0.92<br>735<br>0<br>735<br>0<br>735<br>4<br>37.3<br>0.41<br>6.0<br>3.0<br>772<br>c0.39<br>0.95<br>25.5<br>1.00<br>21.4<br>46.9<br>D<br>37.9<br>D<br>37.9<br>D | 676       329         2000       2000         6.0       6.0         1.00       1.00         1.00       0.85         0.95       1.00         1863       1667         0.95       1.00         1863       1667         0.95       1.00         1863       1667         0.92       0.92         735       358         0       53         735       305         Perm       4         4       4         37.3       37.3         37.3       37.3         37.3       37.3         0.41       0.41         6.0       6.0         3.0       3.0         772       691         c0.39       0.18         0.95       0.44         25.5       18.9         1.00       1.00         21.4       0.5         46.9       19.3         D       B         37.9       D         0       3         0       1         0       1 | 676         329         75           2000         2000         2000           6.0         6.0         1.00           1.00         1.00         1.00           1.00         0.85         0.95         1.00           1863         1667         0.95         1.00           1863         1667         0.92         0.92           0.95         1.00         1863         1667           0.95         1.00         1863         1667           0.92         0.92         0.92         0.92           735         358         82         0         53         0           735         305         0         0         735         0           735         305         0         0         10         0         10           4         4         2         37.3         37.3         37.3         37.3         37.3         37.3         37.3         37.3         37.3         37.4         0.41         6.0         6.0         30         30         10         10         100         10.0         1.0         1.0         1.0         1.0         1.0         1.0         1.0 | 676 $329$ $75$ $448$ $2000$ $2000$ $2000$ $2000$ $6.0$ $6.0$ $6.6$ $1.00$ $1.00$ $0.95$ $1.00$ $0.85$ $1.00$ $0.95$ $1.00$ $0.99$ $1863$ $1667$ $3699$ $0.95$ $1.00$ $0.51$ $1863$ $1667$ $1895$ $0.95$ $1.00$ $0.51$ $1863$ $1667$ $1895$ $0.92$ $0.92$ $0.92$ $0.92$ $735$ $358$ $82$ $487$ $0$ $53$ $0$ $0$ $735$ $358$ $82$ $487$ $0$ $53$ $0$ $0$ $735$ $358$ $82$ $487$ $0$ $53$ $0$ $0$ $735$ $37.3$ $40.1$ $0.45$ $6.0$ $6.0$ $6.6$ $3.0$ <td< td=""><td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td><td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td></td<> | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |

| Lane Configurations         T  |   | ٨  |                                    | $\mathbf{i}$                          | 1                           | 4                                 | Ł          | ٩                                     | f    | p                       | 1  | Ļ                                      | 4                                       |
|--|---|--|------------------------------------|---------------------------------------|-----------------------------|-----------------------------------|------------|---------------------------------------|------|-------------------------|--|--|---|
| Volume (vph)         110         158         243         142         268         4         249         694         60         3         549         1           Ideal Flow (vphpl)         2000         1.00 <td< th=""><th>Movement</th><th>EBL</th><th>EBT</th><th>EBR</th><th>WBL</th><th>WBT</th><th>WBR</th><th>NBL</th><th>NBT</th><th>NBR</th><th>SBL</th><th>SBT</th><th>SBR</th></td<>                                       | Movement  | EBL  | EBT                                | EBR                                   | WBL                         | WBT                               | WBR        | NBL                                   | NBT  | NBR                     | SBL  | SBT                                    | SBR                                     |
| Ideal Flow (vphpl)         2000         100         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         0.95         1.00         0.05         1.00         0.05         1.00         0.05         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         0.016         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00         1.00 <t< td=""><td>Lane Configurations</td><td>٢</td><td>ŕ</td><td>٦</td><td>ሻ</td><td>eî.</td><td></td><td>ħ</td><td>4Î</td><td></td><td>ħ</td><td>个</td><td>ក៏</td></t<>                                  | Lane Configurations   | ٢  | ŕ                                  | ٦                                     | ሻ                           | eî.                               |            | ħ                                     | 4Î   |                         | ħ  | 个                                      | ក៏                                      |
| Total Lost time (s)       4.0       6.1       6.1       5.9<   | Volume (vph)  | 110  | 158                                | 243                                   | 142                         | 268                               | 4          | 249                                   | 694  | 60                      | 3  | 549                                    | 144                                     |
| Lane Util, Factor         1.00         0.00         0.01         0.00         0.09         1.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.01         0.00         0.01         0.00         0.01         0.00         0.01         0.00         0.01         0.00         0.01 <td>Ideal Flow (vphpl)</td> <td>2000</td> | Ideal Flow (vphpl)  | 2000   | 2000                               | 2000                                  | 2000                        | 2000                              | 2000       | 2000                                  | 2000 | 2000                    | 2000   | 2000                                   | 2000                                    |
| Frt       1.00       1.00       0.85       1.00       1.00       0.99       1.00       1.00       0.07         FIL Protected       0.95       1.00       0.95       1.00       0.95       1.00       0.99       1.00       0.95       1.00       0.95       1.00       0.95       1.00       0.95       1.00       0.95       1.00       1.00       0.95       1.00       0.95       1.00       1.00       1.00       1.00       0.95       1.00       1.00       1.00       1.00       1.00       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.01 <td>Total Lost time (s)</td> <td>4.0</td> <td>6.1</td> <td>6.1</td> <td>4.0</td> <td>6.1</td> <td></td> <td>5.9</td> <td>5.9</td> <td></td> <td>5.9</td> <td>5.9</td> <td>5.9</td>   | Total Lost time (s)   | 4.0  | 6.1                                | 6.1                                   | 4.0                         | 6.1                               |            | 5.9                                   | 5.9  |                         | 5.9  | 5.9                                    | 5.9                                     |
| Fit Protected       0.95       1.00       1.00       0.95       1.00       0.95       1.00       1.00       1.10         Satu. Flow (port)       181       2000       1619       1863       1938       1743       1927       1900       1980       16         Fil Permitted       0.24       1.00       0.055       1.00       0.16       1.00       0.14       1000       1.01         Satu. Flow (ptm)       483       2000       1619       1079       1938       296       1927       270       1980       16         Peak-hour factor, PHF       0.83       0.83       0.80       0.80       0.90       0.90       0.95 </td <td>Lane Util. Factor</td> <td>1.00</td> <td>1.00</td> <td>1.00</td> <td>1.00</td> <td>1.00</td> <td>*. **</td> <td>1.00</td> <td>1.00</td> <td></td> <td>1.00</td> <td>1.00</td> <td>1.00</td>   | Lane Util. Factor   | 1.00   | 1.00                               | 1.00                                  | 1.00                        | 1.00                              | *. **      | 1.00                                  | 1.00 |                         | 1.00   | 1.00                                   | 1.00                                    |
| Satd. Flow (prot)       1881       2000       1619       1863       1938       1743       1927       1900       1980       16         FIP Fermitted       0.24       1.00       0.55       1.00       0.16       1.00       0.14       1.00       1.10       1.01       0.14       1.00       1.01       1.01       1.01       1.01       1.01       1.01       1.01       1.01       1.01       1.01       1.01       1.00       1.01       1.00       1.01       1.00       1.01       1.00       1.00       0.55       0.00       0.01   | Frt   | 1.00   | 1.00                               | 0.85                                  | 1.00                        | 1.00                              |            | 1.00                                  | 0.99 |                         | 1.00   | 1.00                                   | 0.85                                    |
| Fit Permitted       0.24       1.00       1.00       0.55       1.00       0.16       1.00       0.14       1.00       1.1         Satd. Flow (perm)       483       2000       1619       1079       1938       296       1927       270       1980       16         Peak-hour factor, PHF       0.83       0.83       0.80       0.80       0.80       0.90       0.90       0.95       0.95       0.95       0.44       1.00       1.1       Satd. Flow (ph)       133       190       293       178       335       5       277       771       67       3       578       1.1         RTOR Reduction (vph)       0       0       189       0       1       0       0       3       0       0       0       1.00       1.00       1.00       1.00       1.00       1.00       1.00       1.00       1.00       1.00       1.00       1.01       1.01       1.02       1.01       1.02       1.01       1.02       1.01       1.02       1.01       1.01       1.01       1.01       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02       1.02 <td>Flt Protected</td> <td>0.95</td> <td>1.00</td> <td>1.00</td> <td>0.95</td> <td>1.00</td> <td></td> <td>0.95</td> <td>1.00</td> <td></td> <td>0.95</td> <td>1.00</td> <td>1.00</td>  | Flt Protected   | 0.95   | 1.00                               | 1.00                                  | 0.95                        | 1.00                              |            | 0.95                                  | 1.00 |                         | 0.95   | 1.00                                   | 1.00                                    |
| Fit Permitted       0.24       1.00       1.00       0.55       1.00       0.16       1.00       0.14       1.00       1.13         Satid. Flow (perm)       483       2000       1619       1079       1338       296       1927       270       1980       16         Peak-hour factor, PHF       0.83       0.83       0.80       0.80       0.80       0.90       0.90       0.95       0.95       0.95       0.95         Adj, Flow (vph)       133       190       293       178       335       5       277       771       67       3       578       1.         Adj, Flow (vph)       133       190       104       178       339       0       277       835       0       3       578       1.         Tum Type       pm+pt       Perm       pm+pt       pm+pt       pm+pt       Perm   | Satd. Flow (prot)   |  | THE R. P. LEWIS CO., LANSING MICH. | 1619                                  | 1863                        |                                   |            |                                       | 1927 |                         | and the second second second second  | The second second second second second | 1650                                    |
| Satd. Flow (perm)         483         2000         1619         1079         1938         296         1927         270         1980         16           Peak-hour factor, PHF         0.83         0.83         0.80         0.80         0.80         0.90         0.90         0.90         0.95         0.95         0.05           Adj. Flow (vph)         133         190         293         178         335         5         277         771         67         3         578         1.           RCOR Reduction (vph)         0         0         189         0         1         0         0         3         0         0         0         189         0         1         0         0         3         0         0         0         100         0         13         190         0         1         10         0         3         0         0         10         0         13         190         104         178         339         0         277         835         0         3         578         11         1019         103         10         11         103         100         10         100         10         100         100         100   |   |  |                                    | 1.00                                  | 0.55                        |                                   |            |                                       | 1.00 |                         | 0.14   | 1.00                                   | 1.00                                    |
| Peak-hour factor, PHF         0.83         0.83         0.83         0.80         0.80         0.90         0.90         0.90         0.95         0.95         0.95           Adj, Flow (vph)         133         190         293         178         335         5         277         771         67         3         578         1.           RTOR Reduction (vph)         0         189         0         1         0         3         0         0         0           Lane Group Flow (vph)         133         190         104         178         339         0         277         835         0         3         578         1.           Lane Group Flow (vph)         133         190         104         178         339         0         277         835         0         3         578         1.           Heavy Vehicles (%)         1%         0%         5%         2%         3%         0%         9%         0%         1%         3           Actuated Green, G (s)         26.2         18.4         18.4         26.6         18.6         47.6         47.6         29.6         29.6         29.6         29.6         29.6         29.6         29.6  | Satd. Flow (perm)   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 1650                                    |
| Adj. Flow (vph)       133       190       293       178       335       5       277       771       67       3       578       1         RTOR Reduction (vph)       0       189       0       1       0       0       3       0       0       0         Lane Group Flow (vph)       133       190       104       178       339       0       277       835       0       3       578       1         Heavy Vehicles (%)       1%       0%       0%       5%       2%       3%       0%       9%       0%       1%       3         Tum Type       pm+pt       Perm       pm+pt       pm+pt       perm       S       0  | generation and the second s   | 0.83   |                                    | 0.83                                  |                             |                                   | 0.80       |                                       | 0.90 | 0.90                    | 0.95   | 0.95                                   | 0.95                                    |
| RTOR Reduction (vph)       0       1       0       0       3       0       0       1         Lane Group Flow (vph)       133       190       104       178       339       0       277       835       0       3       578       4         Heavy Vehicles (%)       1%       0%       5%       2%       3%       0%       9%       0%       1%       3       578       4         Turn Type       pm+pt       Perm       pm+pt       pm+pt       pm+pt       Perm  | an anna an  |  |                                    |                                       |                             |                                   |            |                                       |      |                         | statute analysis in the state  |  | 152                                     |
| Lane Group Flow (vph)         133         190         104         178         339         0         277         835         0         3         578         14           Heavy Vehicles (%)         1%         0%         5%         2%         3%         0%         9%         2%         9%         0%         1%         3           Turn Type         pm+pt         Perm         pm+pt         pm+pt         Perm         Perm         Perm           Protected Phases         7         4         3         8         6         2         5           Actuated Green, G (s)         26.2         18.4         18.4         26.6         18.6         47.6         47.6         29.6 <td></td> <td></td> <td></td> <td>and the grant set of</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>and the second de</td> <td></td> <td></td> <td>72</td>   |   |  |                                    | and the grant set of                  |                             |                                   |            |                                       |      | and the second de       |  |  | 72                                      |
| Heavy Vehicles (%)         1%         0%         5%         2%         3%         0%         9%         2%         9%         0%         1%         3           Turn Type         pm+pt         Perm         pm+pt         pm+pt         pm+pt         Perm  | - construction approximation provide a construction of the second s  | 133  | 190                                |                                       |                             | 339                               |            |                                       |      | 0                       | 3  |  | 80                                      |
| Tum Type         pm+pt         Perm         pm+pt         pm+pt         pm+pt         Perm  |   |  |                                    |                                       |                             |                                   |            |                                       |      | 1 A CANADA SA PARA PARA |  |  | 3%                                      |
| Protected Phases         7         4         3         8         6         2         5           Permitted Phases         4         4         8         2         5         5           Actuated Green, G (s)         26.2         18.4         18.4         26.6         18.6         47.6         29.  |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | Perm                                    |
| Permitted Phases         4         4         8         2         5           Actuated Green, G (s)         26.2         18.4         18.4         26.6         18.6         47.6         29.7         59.6         29.7   |   |  | 4                                  |                                       |                             | 8                                 |            |                                       | 2    |                         |  | 5                                      |   |
| Actuated Green, G (s)       26.2       18.4       18.4       26.6       18.6       47.6       47.6       29.6 <t< td=""><td></td><td></td><td></td><td>4</td><td></td><td></td><td></td><td></td><td></td><td></td><td>5</td><td></td><td>5</td></t<>   |   |  |                                    | 4                                     |                             |                                   |            |                                       |      |                         | 5  |  | 5                                       |
| Effective Green, g (s)       26.2       18.4       18.4       26.6       18.6       47.6       47.6       29.7       10.6       0.7       0.7 <td< td=""><td></td><td></td><td>18.4</td><td></td><td></td><td>18.6</td><td></td><td></td><td>47.6</td><td></td><td></td><td>29.6</td><td>29.6</td></td<>   |   |  | 18.4                               |                                       |                             | 18.6                              |            |                                       | 47.6 |                         |  | 29.6                                   | 29.6                                    |
| Actuated g/C Ratio       0.29       0.20       0.20       0.30       0.21       0.53       0.53       0.30       30       30       30       30       30       30       30       30       30       30       30       30       30       30       30  |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 29.6                                    |
| Clearance Time (s)       4.0       6.1       4.0       6.1       5.9 </td <td></td> <td>0.33</td>  |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 0.33                                    |
| Vehicle Extension (s)         3.0  | and the second  |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 5.9                                     |
| Lane Grp Cap (vph)         262         409         331         389         401         351         1019         89         651         54           v/s Ratio Prot         c0.04         0.10         0.04         c0.18         0.11         c0.43         0.29           v/s Ratio Perm         0.10         0.06         0.09         0.31         0.01         0.01           v/c Ratio         0.51         0.46         0.31         0.46         0.85         0.79         0.82         0.03         0.89         0.7           Uniform Delay, d1         25.0         31.5         30.4         24.7         34.3         29.9         17.6         20.5         28.6         21           Progression Factor         1.00         1.00         1.00         1.00         1.00         1.01         1.01         1.01         1.03         1.1           Incremental Delay, d2         1.5         0.8         0.5         0.9         15.1         12.4         5.5         0.7         16.1         0           Delay (s)         26.6         32.3         31.0         25.6         49.4         47.5         27.5         22.6         48.5         27           Level of Service   | - Contraction and Contraction Contracti           |  |                                    |                                       |                             |                                   |            |                                       |      | i'n tele of electronic  | and the set of the set |  | 3.0                                     |
| v/s Ratio Prot       c0.04       0.10       0.04       c0.18       0.11       c0.43       0.29         v/s Ratio Perm       0.10       0.06       0.09       0.31       0.01       0.0         v/c Ratio       0.51       0.46       0.31       0.46       0.85       0.79       0.82       0.03       0.89       0.7         Uniform Delay, d1       25.0       31.5       30.4       24.7       34.3       29.9       17.6       20.5       28.6       21         Progression Factor       1.00       1.00       1.00       1.00       1.10       1.13       1.2         Incremental Delay, d2       1.5       0.8       0.5       0.9       15.1       12.4       5.5       0.7       16.1       0         Delay (s)       26.6       32.3       31.0       25.6       49.4       47.5       27.5       22.6       48.5       27         Level of Service       C       C       C       D       D       C       D       D       Advo       D       Advo       D       D       D       D       D       D       D       D       D       D       D       D       D       D       D       D   |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 543                                     |
| v/s Ratio Perm       0.10       0.06       0.09       0.31       0.01       0.0         v/c Ratio       0.51       0.46       0.31       0.46       0.85       0.79       0.82       0.03       0.89       0.7         Uniform Delay, d1       25.0       31.5       30.4       24.7       34.3       29.9       17.6       20.5       28.6       21         Progression Factor       1.00       1.00       1.00       1.00       1.18       1.25       1.07       1.13       1.2         Incremental Delay, d2       1.5       0.8       0.5       0.9       15.1       12.4       5.5       0.7       16.1       0         Delay (s)       26.6       32.3       31.0       25.6       49.4       47.5       27.5       22.6       48.5       27         Level of Service       C       C       C       D       D       C       D       D         Approach Delay (s)       30.4       41.2       32.5       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0       44.0  |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         | <b></b>  |  |   |
| v/c Ratio       0.51       0.46       0.31       0.46       0.85       0.79       0.82       0.03       0.89       0.7         Uniform Delay, d1       25.0       31.5       30.4       24.7       34.3       29.9       17.6       20.5       28.6       21         Progression Factor       1.00       1.00       1.00       1.00       1.10       1.13       1.2         Incremental Delay, d2       1.5       0.8       0.5       0.9       15.1       12.4       5.5       0.7       16.1       0         Delay (s)       26.6       32.3       31.0       25.6       49.4       47.5       27.5       22.6       48.5       27         Level of Service       C       C       C       D       D       C       C       D       A4.0         Approach Delay (s)       30.4       41.2       32.5       44.0       A4.0  |   |  |                                    | 0.06                                  |                             |                                   |            |                                       |      |                         | 0.01   |  | 0.05                                    |
| Uniform Delay, d1       25.0       31.5       30.4       24.7       34.3       29.9       17.6       20.5       28.6       21         Progression Factor       1.00       1.00       1.00       1.00       1.00       1.18       1.25       1.07       1.13       1.2         Incremental Delay, d2       1.5       0.8       0.5       0.9       15.1       12.4       5.5       0.7       16.1       0         Delay (s)       26.6       32.3       31.0       25.6       49.4       47.5       27.5       22.6       48.5       27         Level of Service       C       C       C       D       D       C       C       D         Approach Delay (s)       30.4       41.2       32.5       44.0       44.   |   |  | 0.46                               |                                       |                             | 0.85                              |            |                                       | 0.82 |                         |  | 0.89                                   | 0.15                                    |
| Progression Factor         1.00         1.00         1.00         1.00         1.18         1.25         1.07         1.13         1.2           Incremental Delay, d2         1.5         0.8         0.5         0.9         15.1         12.4         5.5         0.7         16.1         0           Delay (s)         26.6         32.3         31.0         25.6         49.4         47.5         27.5         22.6         48.5         27           Level of Service         C         C         C         D         D         C         C         D           Approach Delay (s)         30.4         41.2         32.5         44.0         Approach LOS         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         C         D         C         D         D         C         D         C         D         C         D         C         D         C         D         C         D         C         D         C         D         C         D         C         D         C         C         D <td></td> <td>21.3</td>   |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 21.3                                    |
| Incremental Delay, d2         1.5         0.8         0.5         0.9         15.1         12.4         5.5         0.7         16.1         0           Delay (s)         26.6         32.3         31.0         25.6         49.4         47.5         27.5         22.6         48.5         27           Level of Service         C         C         C         D         D         C         D         D         C         D         D         A8.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         48.5         27         22.6         44.0         22.6         44.0         27         22.6         44.0         27         22.6         44.0         27         22.6         44.0         27         22.6         48.5         27         22.6         48.5         27         22.6         48.7         27         22.6   | <ul> <li>A set of the set of</li></ul>   | and the second |                                    |                                       |                             | a fara an an Araba an Araba       |            | an an taona airi an t-                |      |                         |  |  | 1.25                                    |
| Delay (s)         26.6         32.3         31.0         25.6         49.4         47.5         27.5         22.6         48.5         27           Level of Service         C         C         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D         D         C         D   |   |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 0.6                                     |
| Level of ServiceCCCCDCDApproach Delay (s)30.441.232.544.0Approach LOSCDCDIntersection SummaryHCM Average Control Delay36.4HCM Level of ServiceDHCM Volume to Capacity ratio0.730.7344.0Actuated Cycle Length (s)90.0Sum of lost time (s)9.9Intersection Capacity Utilization84.2%ICU Level of ServiceE   | - A state of the second secon<br>second second sec         |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  | 27.1                                    |
| Approach Delay (s)30.441.232.544.0Approach LOSCDCDIntersection SummaryHCM Average Control Delay36.4HCM Level of ServiceDHCM Volume to Capacity ratio0.73   |   |  |                                    |                                       |                             | en en la seconda activa e e la la |            | · · · · · · · · · · · · · · · · · · · |      |                         |  |  | C                                       |
| Approach LOSCDCDIntersection SummaryHCM Average Control Delay36.4HCM Level of ServiceDHCM Volume to Capacity ratio0.730.73Actuated Cycle Length (s)90.0Sum of lost time (s)9.9Intersection Capacity Utilization84.2%ICU Level of ServiceE  |   |  |                                    | · · · · · · · · · · · · · · · · · · · | (1999) (1997) <b>M</b> aria |                                   |            | 1999 (C. 7. 19                        |      |                         | •  |  | A 31 ( 31 ( 31 ( 31 ( 31 ( 31 ( 31 ( 31 |
| HCM Average Control Delay36.4HCM Level of ServiceDHCM Volume to Capacity ratio0.730.73Actuated Cycle Length (s)90.0Sum of lost time (s)9.9Intersection Capacity Utilization84.2%ICU Level of ServiceE  | (a) A starting the second se<br>second second sec<br>second second s<br>second second s<br>second second se |  | ster orderage of                   |                                       |                             | es esse a co                      |            |                                       | C C  |                         |  |  |   |
| HCM Volume to Capacity ratio       0.73         Actuated Cycle Length (s)       90.0       Sum of lost time (s)       9.9         Intersection Capacity Utilization       84.2%       ICU Level of Service       E   | Intersection Summary  |  |                                    |                                       |                             |                                   |            |                                       |      |                         |  |  |   |
| Actuated Cycle Length (s)90.0Sum of lost time (s)9.9Intersection Capacity Utilization84.2%ICU Level of ServiceE  |   |  |                                    | 36.4                                  | Н                           | CM Level                          | of Servic  | e                                     |      | D                       |  |  |   |
| Intersection Capacity Utilization 84.2% ICU Level of Service E   | HCM Volume to Capacity ra   | atio   |                                    | 0.73                                  |                             |                                   |            |                                       |      |                         |  |  |   |
| Intersection Capacity Utilization 84.2% ICU Level of Service E   | Actuated Cycle Length (s)   |  |                                    | 90.0                                  | S                           | um of lost                        | time (s)   |                                       |      | 9.9                     |  |  |   |
| Analysis Period (min) 15   | Intersection Capacity Utiliza   | ation  |                                    | 84.2%                                 | IC                          | U Level c                         | of Service | •                                     |      |                         |  |  |   |
|  | Analysis Period (min)   |  |                                    | 15                                    |                             |                                   |            |                                       |      |                         |  |  |   |

|                                   | ≯    |      | Ì     | <b>F</b> | <b>4</b>               | Ł          | ٩    | Ť    | Þ    | \$                  | ļ     | 4                  |
|-----------------------------------|------|------|-------|----------|------------------------|------------|------|------|------|---------------------|-------|--------------------|
| Movement                          | EBL  | EBT  | EBR   | WBL      | WBT                    | WBR        | NBL  | NBT  | NBR  | SBL                 | SBT   | SBR                |
| Lane Configurations               | ሻ    | Ŕ    |       | R.       | ¢                      |            | ሻ    | Þ    |      | ٣                   | ŕ     | *آ                 |
| Volume (vph)                      | 25   | 20   | 100   | 175      | 20                     | 60         | 20   | 400  | 80   | 10                  | 500   | 25                 |
| Ideal Flow (vphpl)                | 2000 | 2000 | 2000  | 2000     | 2000                   | 2000       | 2000 | 2000 | 2000 | 2000                | 2000  | 2000               |
| Total Lost time (s)               | 5.8  | 5.8  |       | 5.8      | 5.8                    |            | 5.8  | 5.8  |      | 5.8                 | 5.8   | 5.8                |
| Lane Util. Factor                 | 1.00 | 1.00 |       | 1.00     | 1.00                   |            | 1.00 | 1.00 |      | 1.00                | 1.00  | 1.00               |
| Frt                               | 1.00 | 0.88 |       | 1.00     | 0.89                   |            | 1.00 | 0.98 |      | 1.00                | 1.00  | 0.85               |
| Flt Protected                     | 0.95 | 1.00 |       | 0.95     | 1.00                   |            | 0.95 | 1.00 |      | 0.95                | 1.00  | 1.00               |
| Satd. Flow (prot)                 | 1863 | 1716 |       | 1863     | 1741                   |            | 1863 | 1912 |      | 1863                | 1961  | 1667               |
| Flt Permitted                     | 0.70 | 1.00 |       | 0.67     | 1.00                   |            | 0.41 | 1.00 |      | 0.42                | 1.00  | 1.00               |
| Satd. Flow (perm)                 | 1374 | 1716 |       | 1320     | 1741                   |            | 798  | 1912 |      | 824                 | 1961  | 1667               |
| Peak-hour factor, PHF             | 0.92 | 0.92 | 0.92  | 0.92     | 0.92                   | 0.92       | 0.92 | 0.92 | 0.92 | 0.92                | 0.92  | 0.92               |
| Adj. Flow (vph)                   | 27   | 22   | 109   | 190      | 22                     | 65         | 22   | 435  | 87   | 11                  | 543   | 27                 |
| RTOR Reduction (vph)              | 0    | 87   | 0     | 0        | 52                     | 0          | 0    | 6    | 0    | 0                   | 0     | 7                  |
| Lane Group Flow (vph)             | 27   | 44   | 0     | 190      | 35                     | 0          | 22   | 516  | 0    | 11                  | 543   | 20                 |
| Turn Type                         | Perm |      |       | Perm     |                        |            | Perm |      |      | Perm                |       | Perm               |
| Protected Phases                  |      | 4    |       |          | 8                      |            |      | 2    |      |                     | 6     |                    |
| Permitted Phases                  | 4    |      |       | 8        |                        |            | 2    |      |      | 6                   |       | 6                  |
| Actuated Green, G (s)             | 18.3 | 18.3 |       | 18.3     | 18.3                   |            | 60.1 | 60.1 |      | 60.1                | 60.1  | 60.1               |
| Effective Green, g (s)            | 18.3 | 18.3 |       | 18.3     | 18.3                   |            | 60.1 | 60.1 |      | 60.1                | 60.1  | 60.1               |
| Actuated g/C Ratio                | 0.20 | 0.20 |       | 0.20     | 0.20                   |            | 0.67 | 0.67 |      | 0.67                | 0.67  | 0.67               |
| Clearance Time (s)                | 5.8  | 5.8  |       | 5.8      | 5.8                    |            | 5.8  | 5.8  |      | 5.8                 | 5.8   | 5.8                |
| Vehicle Extension (s)             | 3.0  | 3.0  |       | 3.0      | 3.0                    |            | 3.0  | 3.0  |      | 3.0                 | 3.0   | 3.0                |
| Lane Grp Cap (vph)                | 279  | 349  |       | 268      | 354                    |            | 533  | 1277 |      | 550                 | 1310  | 1113               |
| v/s Ratio Prot                    |      | 0.03 |       |          | 0.02                   |            |      | 0.27 |      |                     | c0.28 |                    |
| v/s Ratio Perm                    | 0.02 |      |       | c0.14    |                        |            | 0.03 |      |      | 0.01                |       | 0.01               |
| v/c Ratio                         | 0.10 | 0.13 |       | 0.71     | 0.10                   |            | 0.04 | 0.40 |      | 0.02                | 0.41  | 0.02               |
| Uniform Delay, d1                 | 29.1 | 29.3 |       | 33.4     | 29.2                   |            | 5.1  | 6.8  |      | 5.0                 | 6.9   | 5.0                |
| Progression Factor                | 1.00 | 1.00 |       | 1.00     | 1.00                   |            | 0.60 | 0.79 |      | 1.37                | 1.27  | 1.76               |
| Incremental Delay, d2             | 0.2  | 0.2  |       | 8.3      | 0.1                    |            | 0.1  | 0.7  |      | 0.1                 | 0.7   | 0.0                |
| Delay (s)                         | 29.3 | 29.5 |       | 41.7     | 29.3                   |            | 3.1  | 6.0  |      | 7.0                 | 9.5   | 8,9                |
| Level of Service                  | С    | С    |       | D        | С                      |            | А    | А    |      | А                   | А     | А                  |
| Approach Delay (s)                |      | 29.4 |       |          | 37.8                   |            |      | 5.9  |      |                     | 9.4   |                    |
| Approach LOS                      |      | С    |       |          | D                      |            |      | А    |      |                     | А     |                    |
| Intersection Summary              |      |      |       |          |                        |            |      |      |      |                     |       |                    |
| HCM Average Control Delay         |      |      | 15.3  | НС       | CM Level               | of Service | 9    |      | В    |                     |       | <u>alanda anna</u> |
| HCM Volume to Capacity ratio      |      |      | 0.48  |          |                        |            |      |      |      |                     |       |                    |
| Actuated Cycle Length (s)         |      |      | 90.0  | Su       | m of lost              | time (s)   |      |      | 11.6 |                     |       |                    |
| Intersection Capacity Utilization |      |      | 50.5% |          | U Level o              |            |      |      | Α    |                     |       |                    |
| Analysis Period (min)             |      |      | 15    |          | n en el catte de la ca |            |      |      |      | e Manazar Masanda a |       |                    |
| c Critical Lane Group             |      |      |       |          |                        |            |      |      |      |                     |       |                    |

|                                      | Å    |       | V     | *     |             | ×.         | *     | t     | p     | 1        | <b>Å</b> | 4    |
|--------------------------------------|------|-------|-------|-------|-------------|------------|-------|-------|-------|----------|----------|------|
| Movement                             | EBL  | EBT   | EBR   | WBL   | WBT         | WBR        | NBL   | NBT   | NBR   | SBL      | SBT      | SBR  |
| Lane Configurations                  | ሻ    | ♠₽    |       | ሻ     | <b>ት</b> ፞ኡ |            | ሻ     | 4     |       | <b>T</b> | 4        |      |
| Volume (vph)                         | 52   | 516   | 75    | 152   | 510         | 104        | 83    | 318   | 83    | 68       | 282      | 18   |
| ldeal Flow (vphpl)                   | 2000 | 2000  | 2000  | 2000  | 2000        | 2000       | 2000  | 2000  | 2000  | 2000     | 2000     | 2000 |
| Total Lost time (s)                  | 6.0  | 6.0   |       | 6.0   | 6.0         |            | 6.0   | 6.0   |       | 6.0      | 6.0      |      |
| Lane Util. Factor                    | 1.00 | 0.95  |       | 1.00  | 0.95        |            | 1.00  | 1.00  |       | 1.00     | 1.00     |      |
| Frt                                  | 1.00 | 0.98  |       | 1.00  | 0.97        |            | 1.00  | 0.97  |       | 1.00     | 0.99     |      |
| Flt Protected                        | 0.95 | 1.00  |       | 0.95  | 1.00        |            | 0.95  | 1.00  |       | 0.95     | 1.00     |      |
| Satd. Flow (prot)                    | 1863 | 3655  |       | 1863  | 3631        |            | 1863  | 1900  |       | 1863     | 1943     |      |
| Flt Permitted                        | 0.95 | 1.00  |       | 0.95  | 1.00        |            | 0.95  | 1.00  |       | 0.95     | 1.00     |      |
| Satd. Flow (perm)                    | 1863 | 3655  |       | 1863  | 3631        |            | 1863  | 1900  |       | 1863     | 1943     |      |
| Peak-hour factor, PHF                | 0.90 | 0.90  | 0.90  | 0.92  | 0.92        | 0.92       | 0.89  | 0.89  | 0.89  | 0.90     | 0.90     | 0.90 |
| Adj. Flow (vph)                      | 58   | 573   | 83    | 165   | 554         | 113        | 93    | 357   | 93    | 76       | 313      | 20   |
| RTOR Reduction (vph)                 | 0    | 12    | 0     | 0     | 18          | 0          | 0     | 10    | 0     | 0        | 2        | 0    |
| Lane Group Flow (vph)                | 58   | 644   | 0     | 165   | 649         | 0          | 93    | 440   | 0     | 76       | 331      | 0    |
| Turn Type                            | Prot |       |       | Prot  |             |            | Prot  |       |       | Prot     |          |      |
| Protected Phases<br>Permitted Phases | 5    | 2     |       | 1     | 6           |            | 3     | 8     |       | 7        | 4        |      |
| Actuated Green, G (s)                | 7.1  | 24.0  |       | 10.6  | 27.5        |            | 8.3   | 23.6  |       | 7.8      | 23.1     |      |
| Effective Green, g (s)               | 7.1  | 24.0  |       | 10.6  | 27.5        |            | 8.3   | 23.6  |       | 7.8      | 23.1     |      |
| Actuated g/C Ratio                   | 0.08 | 0.27  |       | 0.12  | 0.31        |            | 0.09  | 0.26  |       | 0.09     | 0.26     |      |
| Clearance Time (s)                   | 6.0  | 6.0   |       | 6.0   | 6.0         |            | 6.0   | 6.0   |       | 6.0      | 6.0      |      |
| Vehicle Extension (s)                | 3.0  | 3.0   |       | 3.0   | 3.0         |            | 3.0   | 3.0   |       | 3.0      | 3.0      |      |
| Lane Grp Cap (vph)                   | 147  | 975   |       | 219   | 1109        |            | 172   | 498   |       | 161      | 499      |      |
| v/s Ratio Prot                       | 0.03 | c0.18 |       | c0.09 | c0.18       |            | c0.05 | c0.23 |       | 0.04     | 0.17     |      |
| v/s Ratio Perm                       |      |       |       |       |             |            |       |       |       |          |          |      |
| v/c Ratio                            | 0.39 | 0.66  |       | 0.75  | 0.59        |            | 0.54  | 0.88  |       | 0.47     | 0.66     |      |
| Uniform Delay, d1                    | 39.4 | 29.4  |       | 38.4  | 26.4        |            | 39.0  | 31.9  |       | 39.1     | 30.0     |      |
| Progression Factor                   | 1.00 | 1.00  |       | 1.12  | 1.22        |            | 1.17  | 0.69  |       | 1.00     | 1.00     |      |
| Incremental Delay, d2                | 1.7  | 3.5   |       | 9.2   | 1.5         |            | 3.3   | 16.3  |       | 2.2      | 3.3      |      |
| Delay (s)                            | 41.2 | 32.9  |       | 52.2  | 33.6        |            | 49.0  | 38.1  |       | 41.3     | 33.3     |      |
| Level of Service                     | D    | С     |       | D     | С           |            | D     | D     | 1, 1, | D        | С        |      |
| Approach Delay (s)                   |      | 33.5  |       |       | 37.3        |            |       | 40.0  |       |          | 34.8     |      |
| Approach LOS                         |      | С     |       |       | D           |            |       | D     |       |          | С        |      |
| Intersection Summary                 |      |       |       |       |             |            |       |       |       |          |          |      |
| HCM Average Control Delay            |      |       | 36.4  | H     | CM Level    | of Servic  | e     |       | D     |          |          |      |
| HCM Volume to Capacity ratio         |      |       | 0.75  |       |             |            |       |       |       |          |          |      |
| Actuated Cycle Length (s)            |      |       | 90.0  |       |             |            |       | 24.0  |       |          |          |      |
| Intersection Capacity Utilization    | n    |       | 70.3% | IC    | U Level o   | of Service |       |       | С     |          |          |      |
| Analysis Period (min)                |      |       | 15    |       |             |            |       |       |       |          |          |      |
| c Critical Lane Group                |      |       |       |       |             |            |       |       |       |          |          |      |

|                                      | _ <b>A</b> |                           | Ì                    | 1                   | <b>4</b>  | ×.           | ٩        | Î  | p                   | ~~   | Ť               | -  |
|--------------------------------------|------------|---------------------------|----------------------|---------------------|-----------|--------------|----------|--|---------------------|--|-----------------|--|
| Movement                             | EBL        | EBT                       | EBR                  | WBL                 | WBT       | WBR          | NBL      | NBT                                      | NBR                 | SBL  | SBT             | SBR                                      |
| Lane Configurations                  | ሻ          | <u></u> ↑₽                |                      | ሻ                   | ተ         | 7            | ሻ        | ∱>                                       |                     | ኻ  | <b>^</b>        |  |
| Volume (vph)                         | 15         | 944                       | 17                   | 87                  | 941       | 400          | 43       | 55                                       | 188                 | 296  | 108             | 49                                       |
| Ideal Flow (vphpl)                   | 2000       | 2000                      | 2000                 | 2000                | 2000      | 2000         | 2000     | 2000                                     | 2000                | 2000                                       | 2000            | 2000                                     |
| Lane Width                           | 12         | 12                        | 12                   | 12                  | 12        | 12           | 11       | 11                                       | 11                  | 12   | 12              | 12                                       |
| Total Lost time (s)                  | 6.1        | 6.1                       |                      | 6.1                 | 6.1       | 6.1          | 6.0      | 6.0                                      |                     | 6.0  | 6.0             |  |
| Lane Util. Factor                    | 1.00       | 0.95                      |                      | 1.00                | 1.00      | 1.00         | 1.00     | 1.00                                     |                     | 1.00                                       | 1.00            |  |
| Frt                                  | 1.00       | 1.00                      |                      | 1.00                | 1.00      | 0.85         | 1.00     | 0.88                                     |                     | 1.00                                       | 0.95            |  |
| Flt Protected                        | 0.95       | 1.00                      |                      | 0.95                | 1.00      | 1.00         | 0.95     | 1.00                                     |                     | 0.95                                       | 1.00            |  |
| Satd. Flow (prot)                    | 1863       | 3716                      |                      | 1863                | 1961      | 1500         | 1801     | 1676                                     |                     | 1863                                       | 1869            |  |
| Flt Permitted                        | 0.09       | 1.00                      |                      | 0.18                | 1.00      | 1.00         | 0.65     | 1.00                                     |                     | 0.52                                       | 1.00            |  |
| Satd. Flow (perm)                    | 168        | 3716                      |                      | 358                 | 1961      | 1500         | 1226     | 1676                                     |                     | 1027                                       | 1869            |  |
| Peak-hour factor, PHF                | 0.88       | 0.88                      | 0.88                 | 0.92                | 0.92      | 0.92         | 0.94     | 0.94                                     | 0.94                | 0.92                                       | 0.92            | 0.92                                     |
| Adj. Flow (vph)                      | 17         | 1073                      | 19                   | 95                  | 1023      | 435          | 46       | 59                                       | 200                 | 322  | 117             | 53                                       |
| RTOR Reduction (vph)                 | 0          | 1010                      | 0                    | 0<br>0              | 0         | 165          | 0        | Ō  | 0                   | 0  | 20              | Ũ  |
| Lane Group Flow (vph)                | 17         | 1091                      | 0                    | 95                  | 1023      | 270          | 46       | 259                                      | 0                   | 322  | 150             | 0  |
| Parking (#/hr)                       |            | 1001                      | Õ                    |                     | 1020      |              |          | 200                                      |                     |  |                 |  |
|                                      | Perm       |                           |                      | Perm                |           | Perm         | Perm     | a - na a avagora                         | en alter de l'en de | Perm                                       |                 |  |
| Protected Phases                     |            | 2                         | 240 h 34             |                     | 6         |              |          | 8  |                     |  | 4               |  |
| Permitted Phases                     | 2          | e sebés e <del>fo</del> r |                      | 6                   | v         | 6            | 8        |  |                     | 4  | N HERRY HER     |  |
| Actuated Green, G (s)                | 46.8       | 46.8                      |                      | 46.8                | 46.8      | 46.8         | 31.1     | 31.1                                     |                     | 31.1                                       | 31.1            |  |
| Effective Green, g (s)               | 46.8       | 46.8                      |                      | 46.8                | 46.8      | 46.8         | 31.1     | 31.1                                     |                     | 31.1                                       | 31.1            |  |
| Actuated g/C Ratio                   | 0.52       | 0.52                      |                      | 0.52                | 0.52      | 0,52         | 0.35     | 0.35                                     |                     | 0.35                                       | 0.35            |  |
| Clearance Time (s)                   | 6.1        | 6.1                       |                      | 6.1                 | 6.1       | 6.1          | 6.0      | 6.0                                      |                     | 6.0  | 6.0             | 19 11 11 11 11 11 11 11 11 11 11 11 11 1 |
| Vehicle Extension (s)                | 3.0        | 3.0                       |                      | 3.0                 | 3.0       | 3.0          | 3.0      | 3.0                                      |                     | 3.0  | 3.0             |  |
|                                      | 87         | 1932                      |                      | 186                 | 1020      | 780          | 424      | 579                                      |                     | 355  | 646             |  |
| Lane Grp Cap (vph)<br>v/s Ratio Prot | 07         | 0.29                      |                      | 100                 | c0.52     | 100          | 424      | 0.15                                     |                     | 300  | 0.08            |  |
| v/s Ratio Prot                       | 0.40       | 0.29                      |                      | 0.27                | 00.52     | 0.18         | 0.04     | 0.15                                     |                     | c0.31                                      | 0.00            |  |
|                                      | 0.10       | 0.50                      |                      |                     | 1 00      | 0.18         |          | 0.45                                     |                     | server and a server that a first server is | 0.23            |  |
| v/c Ratio                            | 0.20       | 0.56                      |                      | 0.51                | 1.00      | 0.35<br>12.6 | 0.11     |  |                     | 0.91                                       | 0.23<br>21.0    |  |
| Uniform Delay, d1                    | 11.5       | 14.7                      |                      | 14.1                | 21.6      |              | 20.0     | 22.8                                     |                     | 28.1                                       |                 |  |
| Progression Factor                   | 1.15       | 1.06                      |                      | 1.00                | 1.00      | 1.00         | 1.00     | 1.00                                     |                     | 1.00                                       | 1.00            |  |
| Incremental Delay, d2                | 4.8        | 1.2                       |                      | 9.7                 | 28.9      | 1.2          | 0.1      | 0.6                                      |                     | 25.7                                       | 0.2             |  |
| Delay (s)                            | 18.1       | 16.8                      |                      | 23.8                | 50.5      | 13.9         | 20.1     | 23.3                                     |                     | 53.8                                       | 21.1            |  |
| Level of Service                     | В          | B                         |                      | С                   | D         | В            | С        | C  |                     | D  | C               |  |
| Approach Delay (s)<br>Approach LOS   |            | 16.8<br>B                 |                      |                     | 38.6<br>D |              |          | 22.9<br>C                                |                     |  | 42.5<br>D       |  |
| Intersection Summary                 |            | -                         |                      |                     | -         |              |          | -  |                     |  | _               | Den Den Henricken                        |
| HCM Average Control Delay            |            |                           | 30.8                 | H.                  |           | l of Servic  | <u>م</u> |  | C                   |  |                 |  |
| HCM Volume to Capacity ratio         |            |                           | 0.96                 | 11<br>2015 (2012)   |           |              |          |  |                     |  |                 |  |
| Actuated Cycle Length (s)            |            |                           | 90.0                 | C.                  | um of los | t time (e)   |          |  | 12.1                |  |                 |  |
| Intersection Capacity Utilization    |            |                           | 90.0<br>104.9%       |                     |           | of Service   | 1251875  | a an | 12.1<br>G           | NA MA                                      |                 |  |
| Analysis Period (min)                |            |                           | 104.9 <i>%</i><br>15 | es es esse <b>R</b> |           |              |          | e salata ank                             | U                   |  | e van een de la |  |
| c Critical Lane Group                |            |                           | IJ                   |                     |           |              |          |  |                     |  |                 |  |

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|                              |                        | ¥         |            | T                      | 4   | 4                          |  |
|------------------------------|------------------------|-----------|------------|------------------------|---|----------------------------|--|
| Movement                     | EBL                    | EBR       | NBL        | NBT                    | SBT   | SBR                        |  |
| Lane Configurations          | ሻ                      | ٦         |            | <b>Å</b> ∱⊳            | 个   | ก้                         |  |
| Volume (vph)                 | 320                    | 125       | 122        | 533                    | 983   | 148                        |  |
| ldeal Flow (vphpi)           | 2000                   | 2000      | 2000       | 2000                   | 2000  | 2000                       |  |
| Total Lost time (s)          | 6.0                    | 6.0       |            | 6.6                    | 6.6   | 6.6                        |  |
| Lane Util. Factor            | 1.00                   | 1.00      |            | 0.95                   | 1.00  | 1.00                       |  |
| Frt                          | 1.00                   | 0.85      |            | 1.00                   | 1.00  | 0.85                       |  |
| Fit Protected                | 0.95                   | 1.00      |            | 0.99                   | 1.00  | 1.00                       |  |
| Satd. Flow (prot)            | 1863                   | 1667      |            | 3691                   | 1961  | 1667                       |  |
| Flt Permitted                | 0.95                   | 1.00      |            | 0.50                   | 1.00  | 1.00                       |  |
| Satd. Flow (perm)            | 1863                   | 1667      |            | 1856                   | 1961  | 1667                       |  |
| Peak-hour factor, PHF        | 0.92                   | 0.92      | 0.92       | 0.92                   | 0.92  | 0.92                       |  |
| Adj. Flow (vph)              | 348                    | 136       | 133        | 579                    | 1068  | 161                        |  |
| RTOR Reduction (vph)         | 0                      | 78        | 0          | 0                      | 0   | 60                         |  |
| ane Group Flow (vph)         | 348                    | 58        | 0          | 712                    | 1068  | 101                        |  |
| Turn Type                    |                        | Perm      | Perm       |                        |   | Perm                       |  |
| Protected Phases             | 4                      |           |            | 2                      | 6   |                            |  |
| Permitted Phases             |                        | 4         | 2          |                        |   | 6                          |  |
| Actuated Green, G (s)        | 20.7                   | 20.7      |            | 56.7                   | 56.7  | 56.7                       |  |
| Effective Green, g (s)       | 20.7                   | 20.7      |            | 56.7                   | 56.7  | 56.7                       |  |
| Actuated g/C Ratio           | 0.23                   | 0.23      |            | 0.63                   | 0.63  | 0.63                       |  |
| Clearance Time (s)           | 6.0                    | 6.0       |            | 6.6                    | 6.6   | 6.6                        |  |
| /ehicle Extension (s)        | 3.0                    | 3.0       |            | 3.0                    | 3.0   | 3.0                        |  |
| ane Grp Cap (vph)            | 428                    | 383       |            | 1169                   | 1235  | 1050                       |  |
| //s Ratio Prot               | c0.19                  |           |            |                        | c0.54   |                            |  |
| //s Ratio Perm               |                        | 0.03      |            | 0.38                   |   | 0.06                       |  |
| //c Ratio                    | 0.81                   | 0.15      |            | 1.48dl                 | 0.86  | 0.10                       |  |
| Jniform Delay, d1            | 32.8                   | 27.6      |            | 10.0                   | 13.5  | 6.6                        |  |
| Progression Factor           | 1.00                   | 1.00      |            | 1.00                   | 1.10  | 0.99                       |  |
| ncremental Delay, d2         | 11.2                   | 0.2       |            | 2.4                    | 6.5   | 0.1                        |  |
| Delay (s)                    | 44.1                   | 27.8      |            | 12.4                   | 21.5  | 6.6                        |  |
| evel of Service              | D                      | С         |            | В                      | С   | А                          |  |
| Approach Delay (s)           | 39.5                   |           |            | 12.4                   | 19.5  |                            |  |
| Approach LOS                 | D                      |           |            | В                      | В   |                            | n an le bhí na sheanna a tha bhainn an tar bhainn a sha an tar ann an tar an tar an tar an tar an tar an tar an      |
| ntersection Summary          |                        |           |            |                        |   |                            |  |
| CM Average Control Dela      | у                      |           | 21.4       | H                      | CM Level  | of Service                 | С  |
| CM Volume to Capacity ra     |                        |           | 0.85       |                        |   |                            |  |
| Actuated Cycle Length (s)    |                        |           | 90.0       | Su                     | im of lost  | time (s)                   | 12.6   |
| ntersection Capacity Utiliza | ation                  |           | 99.4%      |                        | U Level c   |                            | F States and F   |
| nalysis Period (min)         | an ang miting disina ( |           | 15         | a ta ta ta ta ta faile | 1999 - 1992 - 1997 - 1997<br>1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997<br>1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1 | an de sand slittet di lit. | aanaa ka ahaan ka saara tala ah ahay ka tarka yaa ka waxaa tarka bahariin ka k<br>A |
| Defacto Left Lane. Rec       | code with 1 t          | hough lar | ne as a le | eft lane.              |   |                            |  |
| Critical Lane Group          |                        |           |            |                        |   |                            |  |

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|                                  | - And And         |       |                                 | *     | <b>4</b>   | ×.         | 1     | Ť    | p                   | \$                 | Ļ    | 1                   |
|----------------------------------|-------------------|-------|---------------------------------|-------|------------|------------|-------|------|---------------------|--------------------|------|---------------------|
| Movement                         | EBL               | EBT   | EBR                             | WBL   | WBT        | WBR        | NBL   | NBT  | NBR                 | SBL                | SBT  | SBR                 |
| Lane Configurations              | ሻ                 | 个     | ሾ                               | ሻ     | 4          |            | ሻ     | 4    |                     | ሻ                  | 个    | ሻ                   |
| Volume (vph)                     | 183               | 196   | 214                             | 155   | 87         | 13         | 183   | 504  | 62                  | 3                  | 573  | 37                  |
| Ideal Flow (vphpl)               | 2000              | 2000  | 2000                            | 2000  | 2000       | 2000       | 2000  | 2000 | 2000                | 2000               | 2000 | 2000                |
| Total Lost time (s)              | 6.1               | 6.1   | 6.1                             | 6.1   | 6.1        |            | 5.9   | 5.9  |                     | 5.9                | 5.9  | 5.9                 |
| Lane Util. Factor                | 1.00              | 1.00  | 1.00                            | 1.00  | 1.00       |            | 1.00  | 1.00 |                     | 1.00               | 1.00 | 1.00                |
| Frt                              | 1.00              | 1.00  | 0.85                            | 1.00  | 0.98       |            | 1.00  | 0.98 |                     | 1.00               | 1.00 | 0.85                |
| Fit Protected                    | 0.95              | 1.00  | 1.00                            | 0.95  | 1.00       |            | 0.95  | 1.00 |                     | 0.95               | 1.00 | 1.00                |
| Satd. Flow (prot)                | 1881              | 1923  | 1504                            | 1845  | 1879       |            | 1652  | 1924 |                     | 1900               | 1961 | 1650                |
| Flt Permitted                    | 0.66              | 1.00  | 1.00                            | 0.36  | 1.00       |            | 0.12  | 1.00 |                     | 0.12               | 1.00 | 1.00                |
| Satd. Flow (perm)                | 1311              | 1923  | 1504                            | 705   | 1879       |            | 203   | 1924 |                     | 236                | 1961 | 1650                |
| Peak-hour factor, PHF            | 0.81              | 0.81  | 0.81                            | 0.73  | 0.73       | 0.73       | 0.74  | 0.74 | 0.74                | 0.84               | 0.84 | 0.84                |
| Adj. Flow (vph)                  | 226               | 242   | 264                             | 212   | 119        | 18         | 247   | 681  | 84                  | 4                  | 682  | 44                  |
| RTOR Reduction (vph)             | 0                 | 0     | 132                             | 0     | 6          | 0          | 0     | 5    | 0                   | 0                  | 0    | 18                  |
| Lane Group Flow (vph)            | 226               | 242   | 132                             | 212   | 131        | 0          | 247   | 760  | Ō                   | 4                  | 682  | 26                  |
| Heavy Vehicles (%)               | 1%                | 4%    | 13%                             | 3%    | 2%         | 20%        | 15%   | 2%   | 4%                  | 0%                 | 2%   | 3%                  |
| Turn Type                        | pm+pt             |       | Perm                            | pm+pt |            |            | pm+pt |      |                     | Perm               |      | Perm                |
| Protected Phases                 | 7                 | 4     |                                 | 3     | 8          |            | 5     | 2    |                     |                    | 6    |                     |
| Permitted Phases                 | 4                 |       | 4                               | 8     |            |            | 2     |      |                     | 6                  |      | 6                   |
| Actuated Green, G (s)            | 22.0              | 14.1  | 14.1                            | 22.0  | 14.1       |            | 49.9  | 49.9 |                     | 33.9               | 33.9 | 33.9                |
| Effective Green, g (s)           | 22.0              | 14.1  | 14.1                            | 22.0  | 14.1       |            | 49.9  | 49.9 |                     | 33.9               | 33.9 | 33.9                |
| Actuated g/C Ratio               | 0.24              | 0.16  | 0.16                            | 0.24  | 0.16       |            | 0.55  | 0.55 |                     | 0.38               | 0.38 | 0.38                |
| Clearance Time (s)               | 6.1               | 6.1   | 6.1                             | 6.1   | 6.1        |            | 5.9   | 5.9  |                     | 5.9                | 5.9  | 5.9                 |
| Vehicle Extension (s)            | 3.0               | 3.0   | 3.0                             | 3.0   | 3.0        |            | 3.0   | 3.0  |                     | 3.0                | 3.0  | 3.0                 |
| Lane Grp Cap (vph)               | 371               | 301   | 236                             | 272   | 294        |            | 275   | 1067 |                     | 89                 | 739  | 622                 |
| v/s Ratio Prot                   | 0.05              | c0.13 | - 2012 (2017) (2017) (2017)<br> | c0.07 | 0.07       |            | c0.10 | 0.39 |                     | Saaloola Turood    | 0.35 | an'n'n d'affinistan |
| v/s Ratio Perm                   | 0.10              |       | 0.09                            | 0.12  |            |            | c0.40 |      |                     | 0.02               |      | 0.02                |
| v/c Ratio                        | 0.61              | 0.80  | 0.56                            | 0.78  | 0.45       |            | 0.90  | 0.71 | factoria de 1920.74 | 0.04               | 0.92 | 0.04                |
| Uniform Delay, d1                | 29.3              | 36.6  | 35.1                            | 29.8  | 34.4       |            | 32.6  | 14.8 |                     | 17.8               | 26.8 | 17.8                |
| Progression Factor               | 1.00              | 1.00  | 1.00                            | 1.00  | 1.00       |            | 1.06  | 1.08 |                     | 1.00               | 0.97 | 1.00                |
| Incremental Delay, d2            | 2.8               | 14.3  | 2.8                             | 13.2  | 1.1        |            | 26.3  | 3.5  |                     | 0.9                | 18.7 | 0.1                 |
| Delay (s)                        | 32.1              | 51.0  | 37.9                            | 43.0  | 35.5       |            | 60.9  | 19.5 |                     | 18.8               | 44.5 | 17.8                |
| Level of Service                 | C                 | D     | D                               | D     | D          |            | E     | В    |                     | В                  | D    | В                   |
| Approach Delay (s)               | - 11 - 11 - T. S. | 40.4  | a navatra.                      | 1     | 40.0       |            |       | 29.6 |                     | iya salita a Tarah | 42.8 | n ninga sinit.<br>T |
| Approach LOS                     |                   | D     |                                 |       | D          |            |       | C    |                     |                    | D    |                     |
| Intersection Summary             |                   |       |                                 |       |            |            |       |      |                     |                    |      |                     |
| HCM Average Control Delay        |                   |       | 37.1                            | H     | CM Level   | of Servic  | æ     |      | D                   |                    |      |                     |
| HCM Volume to Capacity ratio     | )                 |       | 0.84                            |       |            |            |       |      |                     |                    |      |                     |
| Actuated Cycle Length (s)        |                   |       | 90.0                            | Sı    | um of lost | time (s)   |       |      | 18.1                |                    |      |                     |
| Intersection Capacity Utilizatio | n                 |       | 76.2%                           | IC    | U Level c  | of Service | ;     |      | D                   |                    |      |                     |
| Analysis Period (min)            |                   |       | 15                              |       |            |            |       |      |                     |                    |      |                     |

|                                 | ٨                   |             | Ý                      | 1              |                         | Ł                     | 4     | Î    | p    | 1    | Ť     | 4                |
|---------------------------------|---------------------|-------------|------------------------|----------------|-------------------------|-----------------------|-------|------|------|------|-------|------------------|
| Movement                        | EBL                 | EBT         | EBR                    | WBL            | WBT                     | WBR                   | NBL   | NBT  | NBR  | SBL  | SBT   | SBR              |
| Lane Configurations             | ¥.                  | <b>ት</b> ᡗ» |                        | ሻ              | ⋪ኁ                      |                       | ሻ     | \$⇒  |      | ሻ    | ۴Î    |                  |
| Volume (vph)                    | 22                  | 508         | 76                     | 74             | 530                     | 14                    | 72    | 176  | 110  | 51   | 310   | 12               |
| Ideal Flow (vphpl)              | 2000                | 2000        | 2000                   | 2000           | 2000                    | 2000                  | 2000  | 2000 | 2000 | 2000 | 2000  | 2000             |
| Total Lost time (s)             | 6.0                 | 6.0         |                        | 6.0            | 6.0                     |                       | 6.0   | 6.0  |      | 6.0  | 6.0   |                  |
| Lane Util. Factor               | 1.00                | 0.95        |                        | 1.00           | 0.95                    |                       | 1.00  | 1.00 |      | 1.00 | 1.00  |                  |
| Frt                             | 1.00                | 0.98        |                        | 1.00           | 1.00                    |                       | 1.00  | 0.94 |      | 1.00 | 0.99  |                  |
| Flt Protected                   | 0.95                | 1.00        |                        | 0.95           | 1.00                    |                       | 0.95  | 1.00 |      | 0.95 | 1.00  |                  |
| Satd. Flow (prot)               | 1863                | 3653        |                        | 1863           | 3711                    |                       | 1863  | 1847 |      | 1863 | 1950  |                  |
| Flt Permitted                   | 0.95                | 1.00        |                        | 0.95           | 1.00                    |                       | 0.95  | 1.00 |      | 0.95 | 1.00  |                  |
| Satd. Flow (perm)               | 1863                | 3653        |                        | 1863           | 3711                    |                       | 1863  | 1847 |      | 1863 | 1950  |                  |
| Peak-hour factor, PHF           | 0.79                | 0.79        | 0.79                   | 0.70           | 0.70                    | 0.70                  | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81             |
| Adj. Flow (vph)                 | 28                  | 643         | 96                     | 106            | 757                     | 20                    | 76    | 185  | 116  | 63   | 383   | 15               |
| RTOR Reduction (vph)            | 0                   | 12          | 0                      | 0              | 2                       | 0                     | 0     | 26   | 0    | 0    | 2     | 0                |
| Lane Group Flow (vph)           | 28                  | 727         | 0                      | 106            | 775                     | 0                     | 76    | 275  | 0    | 63   | 396   | 0                |
| Turn Type                       | Prot                |             |                        | Prot           |                         |                       | Prot  |      |      | Prot |       | ******           |
| Protected Phases                | 5                   | 2           |                        | 1              | 6                       |                       | 3     | 8    |      | 7    | 4     |                  |
| Permitted Phases                |                     |             | , sin in Bath Annah I. |                |                         | , san 'n ar snintsins |       |      |      |      |       |                  |
| Actuated Green, G (s)           | 3.3                 | 30.8        |                        | 7.5            | 35.0                    |                       | 5.6   | 22.1 |      | 5.6  | 22.1  |                  |
| Effective Green, g (s)          | 3.3                 | 30.8        |                        | 7.5            | 35.0                    |                       | 5.6   | 22.1 |      | 5.6  | 22.1  |                  |
| Actuated g/C Ratio              | 0.04                | 0.34        |                        | 0.08           | 0.39                    |                       | 0.06  | 0.25 |      | 0.06 | 0.25  |                  |
| Clearance Time (s)              | 6.0                 | 6.0         |                        | 6.0            | 6.0                     |                       | 6.0   | 6.0  |      | 6.0  | 6.0   |                  |
| Vehicle Extension (s)           | 3.0                 | 3.0         |                        | 3.0            | 3.0                     |                       | 3.0   | 3.0  |      | 3.0  | 3.0   |                  |
| Lane Grp Cap (vph)              | 68                  | 1250        |                        | 155            | 1443                    |                       | 116   | 454  |      | 116  | 479   |                  |
| v/s Ratio Prot                  | 0.02                | c0.20       |                        | c0.06          | c0.21                   |                       | c0.04 | 0.15 |      | 0.03 | c0.20 |                  |
| v/s Ratio Perm                  |                     |             |                        |                |                         |                       |       |      |      |      |       |                  |
| v/c Ratio                       | 0.41                | 0.58        |                        | 0.68           | 0.54                    |                       | 0.66  | 0.60 |      | 0.54 | 0.83  |                  |
| Uniform Delay, d1               | 42.4                | 24.3        |                        | 40.1           | 21.2                    |                       | 41.3  | 30.1 |      | 41.0 | 32.1  |                  |
| Progression Factor              | 1.00                | 1.00        |                        | 1.11           | 1.23                    |                       | 0.92  | 0.88 |      | 1.00 | 1.00  |                  |
| Incremental Delay, d2           | 4.0                 | 2.0         |                        | 8.6            | 1.0                     |                       | 12.1  | 2.2  |      | 5.1  | 11.2  |                  |
| Delay (s)                       | 46.4                | 26.3        |                        | 52.9           | 27.2                    |                       | 49.9  | 28.6 |      | 46.1 | 43.4  |                  |
| Level of Service                | D                   | С           |                        | D              | С                       |                       | D     | С    |      | D    | D     |                  |
| Approach Delay (s)              |                     | 27.0        |                        |                | 30.3                    |                       |       | 32.9 |      |      | 43.7  |                  |
| Approach LOS                    |                     | С           |                        |                | С                       |                       |       | С    |      |      | D     |                  |
| Intersection Summary            |                     |             |                        |                |                         |                       |       |      |      |      |       |                  |
| HCM Average Control Delay       |                     |             | 32.2                   | Н              | CM Level                | of Servic             | е     |      | С    |      |       |                  |
| HCM Volume to Capacity rati     | 0                   |             | 0.76                   |                |                         |                       |       |      |      |      |       |                  |
| Actuated Cycle Length (s)       | a na Silan ta dan S |             | 90.0                   | S              | um of lost              | time (s)              |       |      | 30.0 |      |       | e e Schendel a S |
| Intersection Capacity Utilizati | on                  |             | 63.5%                  |                | U Level o               |                       |       |      | В    |      |       |                  |
| Analysis Period (min)           | unestrut aut 14.    |             | 15                     | e ferre fa dis | na na si si danta fan T |                       |       |      |      |      |       |                  |
| c Critical Lane Group           |                     |             |                        |                |                         |                       |       |      |      |      |       |                  |

|                                   | ≯    |      | $\mathbf{i}$ | <b>\$</b> | <b>4</b>   | Ł          | ٩    | Î    | P      | 1     | <b>.</b> | 1      |
|-----------------------------------|------|------|--------------|-----------|------------|------------|------|------|--------|-------|----------|--------|
| Movement                          | EBL  | EBT  | EBR          | WBL       | WBT        | WBR        | NBL  | NBT  | NBR    | SBL   | SBT      | SBR    |
| Lane Configurations               | ኻ    | 朴诤   |              | ሻ         | 个          | 7          | ኻ    | \$   | ****** | ሻ     | \$       | ****** |
| Volume (vph)                      | 5    | 810  | 8            | 69        | 812        | 135        | 9    | 15   | 183    | 212   | 24       | 12     |
| Ideal Flow (vphpi)                | 2000 | 2000 | 2000         | 2000      | 2000       | 2000       | 2000 | 2000 | 2000   | 2000  | 2000     | 2000   |
| Total Lost time (s)               | 6.1  | 6.1  |              | 4.0       | 6.1        | 6.1        | 6.0  | 6.0  |        | 4.0   | 6.0      |        |
| Lane Util. Factor                 | 1.00 | 0.95 |              | 1.00      | 1.00       | 1.00       | 1.00 | 1.00 |        | 1.00  | 1.00     |        |
| Frt                               | 1.00 | 1.00 |              | 1.00      | 1.00       | 0.85       | 1.00 | 0.86 |        | 1.00  | 0.95     |        |
| Flt Protected                     | 0.95 | 1.00 |              | 0.95      | 1.00       | 1.00       | 0.95 | 1.00 |        | 0.95  | 1.00     |        |
| Satd. Flow (prot)                 | 1863 | 3720 |              | 1863      | 1961       | 1500       | 1863 | 1689 |        | 1863  | 1863     |        |
| Flt Permitted                     | 0.10 | 1.00 |              | 0.13      | 1.00       | 1.00       | 0.73 | 1.00 |        | 0.35  | 1.00     |        |
| Satd. Flow (perm)                 | 203  | 3720 |              | 259       | 1961       | 1500       | 1423 | 1689 |        | 687   | 1863     |        |
| Peak-hour factor, PHF             | 0.76 | 0.76 | 0.76         | 0.83      | 0.83       | 0.83       | 0.83 | 0.83 | 0.83   | 0.75  | 0.75     | 0.75   |
| Adj. Flow (vph)                   | 7    | 1066 | 11           | 83        | 978        | 163        | 11   | 18   | 220    | 283   | 32       | 16     |
| RTOR Reduction (vph)              | 0    | 1    | 0            | 0         | 0          | 66         | 0    | 0    | 0      | 0     | 11       | 0      |
| Lane Group Flow (vph)             | 7    | 1076 | 0            | 83        | 978        | 97         | 11   | 238  | 0      | 283   | 37       | 0      |
| Parking (#/hr)                    |      |      | 0            |           |            | 0          |      |      |        |       |          |        |
| Turn Type                         | Perm |      |              | pm+pt     |            | Perm       | Perm |      |        | pm+pt |          |        |
| Protected Phases                  |      | 2    |              | 1         | 6          |            |      | 8    |        | 7     | 4        |        |
| Permitted Phases                  | 2    |      |              | 6         |            | 6          | 8    |      |        | 4     |          |        |
| Actuated Green, G (s)             | 38.7 | 38.7 |              | 48.6      | 48.6       | 48.6       | 17.3 | 17.3 |        | 29.3  | 29.3     |        |
| Effective Green, g (s)            | 38.7 | 38.7 |              | 48.6      | 48.6       | 48.6       | 17.3 | 17.3 |        | 29.3  | 29.3     |        |
| Actuated g/C Ratio                | 0.43 | 0.43 |              | 0.54      | 0.54       | 0.54       | 0.19 | 0.19 |        | 0.33  | 0.33     |        |
| Clearance Time (s)                | 6.1  | 6.1  |              | 4.0       | 6.1        | 6.1        | 6.0  | 6.0  |        | 4.0   | 6.0      |        |
| Vehicle Extension (s)             | 3.0  | 3.0  |              | 3.0       | 3.0        | 3.0        | 3.0  | 3.0  |        | 3.0   | 3.0      |        |
| Lane Grp Cap (vph)                | 87   | 1600 |              | 245       | 1059       | 810        | 274  | 325  |        | 328   | 607      |        |
| v/s Ratio Prot                    |      | 0.29 |              | 0.02      | c0.50      |            |      | 0.14 |        | c0.08 | 0.02     |        |
| v/s Ratio Perm                    | 0.03 |      |              | 0.16      |            | 0.06       | 0.01 |      |        | c0.20 |          |        |
| v/c Ratio                         | 0.08 | 0.67 |              | 0.34      | 0.92       | 0.12       | 0.04 | 0.73 |        | 0.86  | 0.06     |        |
| Uniform Delay, d1                 | 15.1 | 20.6 |              | 13.0      | 19.0       | 10.2       | 29.6 | 34.2 |        | 27.0  | 20.9     |        |
| Progression Factor                | 1.11 | 0.93 |              | 1.00      | 1.00       | 1.00       | 1.00 | 1.00 |        | 1.00  | 1.00     |        |
| Incremental Delay, d2             | 1.7  | 2.2  |              | 0.8       | 14.5       | 0.3        | 0.1  | 8.3  |        | 20.2  | 0.0      |        |
| Delay (s)                         | 18.6 | 21.3 |              | 13.8      | 33.4       | 10.5       | 29.7 | 42.4 |        | 47.2  | 20.9     |        |
| Level of Service                  | В    | С    |              | В         | С          | В          | С    | D    |        | D     | С        |        |
| Approach Delay (s)                |      | 21.3 |              |           | 29.1       |            |      | 41.9 |        |       | 43.4     |        |
| Approach LOS                      |      | С    |              |           | С          |            |      | D    |        |       | D        |        |
| Intersection Summary              |      |      |              |           |            |            |      |      |        |       |          |        |
| HCM Average Control Delay         |      |      | 28.9         | H         | CM Level   | of Servic  | e    |      | С      |       |          |        |
| HCM Volume to Capacity ratio      |      |      | 0.87         |           |            |            |      |      |        |       |          |        |
| Actuated Cycle Length (s)         |      |      | 90.0         | S         | um of lost | time (s)   |      |      | 10.1   |       |          |        |
| Intersection Capacity Utilization |      |      | 90.1%        |           |            | of Service |      |      | E      |       |          |        |
| Analysis Period (min)             |      |      | 15           |           |            |            |      |      |        |       |          |        |
| o Critical Lana Crown             |      |      |              |           |            |            |      |      |        |       |          |        |

|                                 | Å     | $\mathbf{i}$ | ٩                                    | Î              | ₽          | 4          |      |
|---------------------------------|-------|--------------|--------------------------------------|----------------|------------|------------|------|
| Movement                        | EBL   | EBR          | NBL                                  | NBT            | SBT        | SBR        |      |
| Lane Configurations             | *     | ۴            | na na ann an tha ann an tha gu a she | <del>ብ</del> ት | <b>A</b>   | ř          |      |
| Volume (vph)                    | 785   | 411          | 87                                   | 520            | 944        | 223        |      |
| Ideal Flow (vphpl)              | 2000  | 2000         | 2000                                 | 2000           | 2000       | 2000       |      |
| Total Lost time (s)             | 6.0   | 6.0          |                                      | 6.6            | 6.6        | 6.6        |      |
| Lane Util. Factor               | 1.00  | 1.00         |                                      | 0.95           | 1.00       | 1.00       |      |
| Frt                             | 1.00  | 0.85         |                                      | 1.00           | 1.00       | 0.85       |      |
| Fit Protected                   | 0.95  | 1.00         |                                      | 0.99           | 1.00       | 1.00       |      |
| Satd. Flow (prot)               | 1863  | 1667         |                                      | 3699           | 1961       | 1667       |      |
| FIt Permitted                   | 0.95  | 1.00         |                                      | 0.51           | 1.00       | 1.00       |      |
| Satd. Flow (perm)               | 1863  | 1667         |                                      | 1887           | 1961       | 1667       |      |
| Peak-hour factor, PHF           | 0.92  | 0.92         | 0.92                                 | 0.92           | 0.92       | 0.92       |      |
| Adj. Flow (vph)                 | 853   | 447          | 95                                   | 565            | 1026       | 242        |      |
| RTOR Reduction (vph)            | 0     | 36           | 0                                    | 0              | 0          | 104        |      |
| _ane Group Flow (vph)           | 853   | 411          | 0                                    | 660            | 1026       | 138        |      |
| Turn Type                       |       | Perm         | Perm                                 |                |            | Perm       |      |
| Protected Phases                | 4     |              |                                      | 2              | 6          |            |      |
| Permitted Phases                |       | 4            | 2                                    |                |            | 6          |      |
| Actuated Green, G (s)           | 35.0  | 35.0         |                                      | 42.4           | 42.4       | 42.4       |      |
| Effective Green, g (s)          | 35.0  | 35.0         |                                      | 42.4           | 42.4       | 42.4       |      |
| Actuated g/C Ratio              | 0.39  | 0.39         |                                      | 0.47           | 0.47       | 0.47       |      |
| Clearance Time (s)              | 6.0   | 6.0          |                                      | 6.6            | 6.6        | 6.6        |      |
| /ehicle Extension (s)           | 3.0   | 3.0          |                                      | 3.0            | 3.0        | 3.0        |      |
| ane Grp Cap (vph)               | 725   | 648          |                                      | 889            | 924        | 785        |      |
| //s Ratio Prot                  | c0.46 |              |                                      |                | c0.52      |            |      |
| //s Ratio Perm                  |       | 0.25         |                                      | 0.35           |            | 0.08       |      |
| ı/c Ratio                       | 1.18  | 0.63         |                                      | 1.09dl         | 1.11       | 0.18       |      |
| Jniform Delay, d1               | 27.5  | 22.3         |                                      | 19.4           | 23.8       | 13.7       |      |
| Progression Factor              | 1.00  | 1.00         |                                      | 1.00           | 0.75       | 0.43       |      |
| ncremental Delay, d2            | 93.5  | 2.0          |                                      | 5.6            | 59.2       | 0.3        |      |
| Delay (s)                       | 121.0 | 24.3         |                                      | 24.9           | 77.1       | 6.2        |      |
| evel of Service                 | F     | С            |                                      | С              | Е          | А          |      |
| Approach Delay (s)              | 87.8  |              |                                      | 24.9           | 63.6       |            |      |
| Approach LOS                    | F     |              |                                      | С              | Е          |            |      |
| ntersection Summary             |       |              |                                      |                |            |            |      |
| CM Average Control Delay        |       |              | 65.4                                 | Н              | CM Level   | of Service | Е    |
| ICM Volume to Capacity ratio    | )     |              | 1.14                                 |                |            |            |      |
| Actuated Cycle Length (s)       |       |              | 90.0                                 | SI             | um of lost | time (s)   | 12.6 |
| ntersection Capacity Utilizatio | n     |              | 120.6%                               |                | U Level c  |            | H    |
| Analysis Period (min)           |       |              | 15                                   | - 1            |            |            |      |

|   | Å     |      | $\mathbf{F}$ | *                 | 4                      | ×.                  | ٩                  | Å     | p    | 6                        | ţ    | 4     |
|---|-------|------|--------------|-------------------|------------------------|---------------------|--------------------|-------|------|--------------------------|------|-------|
| Movement  | EBL   | EBT  | EBR          | WBL               | WBT                    | WBR                 | NBL                | NBT   | NBR  | SBL                      | SBT  | SBR   |
| Lane Configurations   | ٦     | ተ    | ሻ            | ٢                 | ĥ                      |                     | ሻ                  | ĥ     |      | ሻ                        | ዯ    | กี    |
| Volume (vph)  | 128   | 183  | 282          | 165               | 312                    | 5                   | 289                | 805   | 69   | 4                        | 637  | 167   |
| Ideal Flow (vphpl)  | 2000  | 2000 | 2000         | 2000              | 2000                   | 2000                | 2000               | 2000  | 2000 | 2000                     | 2000 | 2000  |
| Total Lost time (s)   | 6.1   | 6.1  | 5.9          | 6.1               | 6.1                    |                     | 5.9                | 5.9   |      | 5.9                      | 5.9  | 6.1   |
| Lane Util. Factor   | 1.00  | 1.00 | 1.00         | 1.00              | 1.00                   |                     | 1.00               | 1.00  |      | 1.00                     | 1.00 | 1.00  |
| Frt   | 1.00  | 1.00 | 0.85         | 1.00              | 1.00                   |                     | 1.00               | 0.99  |      | 1.00                     | 1.00 | 0.85  |
| Flt Protected   | 0.95  | 1.00 | 1.00         | 0.95              | 1.00                   |                     | 0.95               | 1.00  |      | 0.95                     | 1.00 | 1.00  |
| Satd. Flow (prot)   | 1881  | 2000 | 1619         | 1863              | 1938                   |                     | 1743               | 1927  |      | 1900                     | 1980 | 1650  |
| Flt Permitted   | 0.21  | 1.00 | 1.00         | 0.49              | 1.00                   |                     | 0.11               | 1.00  |      | 0.14                     | 1.00 | 1.00  |
| Satd. Flow (perm)   | 419   | 2000 | 1619         | 967               | 1938                   |                     | 210                | 1927  |      | 275                      | 1980 | 1650  |
| Peak-hour factor, PHF   | 0.83  | 0.83 | 0.83         | 0.80              | 0.80                   | 0.80                | 0.90               | 0.90  | 0.90 | 0.95                     | 0.95 | 0.95  |
| Adj. Flow (vph)   | 154   | 220  | 340          | 206               | 390                    | 6                   | 321                | 894   | 77   | 4                        | 671  | 176   |
| RTOR Reduction (vph)  | 0     | 0    | 77           | 0                 | 11 - 11 - 11 - 11<br>1 | 0                   | 0                  | 3     | 0    | 0                        | 0    | 51    |
| Lane Group Flow (vph)   | 154   | 220  | 263          | 206               | 395                    | 0                   | 321                | 968   | 0    | 4                        | 671  | 125   |
| Heavy Vehicles (%)  | 1%    | 0%   | 5%           | 2%                | 3%                     | 0%                  | 9%                 | 2%    | 9%   | 0%                       | 1%   | 3%    |
| Turn Type   | pm+pt |      | pm+ov        | pm+pt             |                        |                     | pm+pt              |       |      | Perm                     |      | pm+ov |
| Protected Phases  | 7     | 4    | 5            | 3                 | 8                      |                     | 5                  | 2     |      |                          | 6    | 7     |
| Permitted Phases  | 4     |      | 4            | 8                 |                        |                     | 2                  |       |      | 6                        |      | 6     |
| Actuated Green, G (s)   | 26.7  | 18.9 | 29.0         | 26.9              | 19.0                   |                     | 45.1               | 45.1  |      | 29.1                     | 29.1 | 36.9  |
| Effective Green, g (s)  | 26.7  | 18.9 | 29.0         | 26.9              | 19.0                   |                     | 45.1               | 45.1  |      | 29.1                     | 29.1 | 36.9  |
| Actuated g/C Ratio  | 0.30  | 0.21 | 0.32         | 0.30              | 0.21                   |                     | 0.50               | 0.50  |      | 0.32                     | 0.32 | 0.41  |
| Clearance Time (s)  | 6.1   | 6.1  | 5.9          | 6.1               | 6.1                    |                     | 5.9                | 5.9   |      | 5.9                      | 5.9  | 6.1   |
| Vehicle Extension (s)   | 3.0   | 3.0  | 3.0          | 3.0               | 3.0                    | t nodisčítna tručna | 3.0                | 3.0   |      | 3.0                      | 3.0  | 3.0   |
| Lane Grp Cap (vph)  | 251   | 420  | 522          | 368               | 409                    |                     | 277                | 966   |      | 89                       | 640  | 677   |
| v/s Ratio Prot  | c0.05 | 0.11 | 0.06         | 0.05              | c0.20                  |                     | 0.13               | c0.50 |      | ititin ay <b>T</b> alati | 0.34 | 0.02  |
| v/s Ratio Perm  | 0.13  |      | 0.11         | 0.12              | 00120                  |                     | c0.45              | 00.00 |      | 0.01                     | 0.0  | 0.06  |
| v/c Ratio   | 0.61  | 0.52 | 0.50         | 0.56              | 0.97                   |                     | 1.16               | 1.00  |      | 0.04                     | 1.05 | 0.19  |
| Uniform Delay, d1   | 25.4  | 31.6 | 24.7         | 25.0              | 35.2                   |                     | 35.9               | 22.4  |      | 20.9                     | 30.4 | 17.0  |
| Progression Factor  | 1.00  | 1.00 | 1.00         | 1.00              | 1.00                   |                     | 1.17               | 1.26  |      | 0.95                     | 0.94 | 0.79  |
| Incremental Delay, d2   | 4.4   | 1.2  | 0.8          | 1.8               | 35.4                   |                     | 91.7               | 21.8  |      | 0.9                      | 48.5 | 0.1   |
| Delay (s)   | 29.8  | 32.7 | 25.4         | 26.8              | 70.6                   |                     | 133.7              | 50.0  |      | 20.8                     | 77.0 | 13.5  |
| Level of Service  | C     | C    | <br>C        | C                 | E                      |                     | E F                | D     |      | C                        | E    | В     |
| Approach Delay (s)  |       | 28.6 |              | in a schilleffin. | -<br>55.6              |                     | Asharitan Maha     | 70.8  |      |                          | 63.6 | ····· |
| Approach LOS  |       | C    |              |                   | E                      |                     |                    | Ē     |      |                          | Ē    |       |
| Intersection Summary  |       |      |              |                   |                        |                     |                    |       |      |                          |      |       |
| HCM Average Control Delay   |       |      | 57.7         | H                 | CM Level               | of Servic           | ce                 |       | Е    |                          |      |       |
| HCM Volume to Capacity rati   | 0     |      | 0.94         |                   |                        |                     | an ister e te ar é |       |      |                          |      |       |
| Actuated Cycle Length (s)   |       |      | 90.0         | S                 | um of lost             | time (s)            |                    |       | 12.0 |                          |      |       |
| Intersection Capacity Utilizati   | on    |      | 95.2%        |                   | CU Level o             |                     |                    |       | F    |                          |      |       |
| Analysis Period (min)   |       |      | 15           |                   |                        |                     |                    |       |      |                          |      |       |
| e e la completa de la |       |      |              |                   |                        |                     |                    |       |      |                          |      |       |

|                                   | ۶                  |                     | $\mathbf{k}$ | 1              | 4             | Ł          | 1     | Ť                     | p    | 1                | Ļ                        | 4       |
|-----------------------------------|--------------------|---------------------|--------------|----------------|---------------|------------|-------|-----------------------|------|------------------|--------------------------|---------|
| Movement                          | EBL                | EBT                 | EBR          | WBL            | WBT           | WBR        | NBL   | NBT                   | NBR  | SBL              | SBT                      | SBR     |
| Lane Configurations               | ሻ                  | <b>ቶ</b> ኈ          |              | ሻ              | <b>ት</b> ጮ    |            | ኻ     | Ŕ                     |      | ሻ                | ¢1                       |         |
| Volume (vph)                      | 60                 | 599                 | 87           | 177            | 592           | 121        | 96    | 369                   | 96   | 80               | 327                      | 21      |
| Ideal Flow (vphpl)                | 2000               | 2000                | 2000         | 2000           | 2000          | 2000       | 2000  | 2000                  | 2000 | 2000             | 2000                     | 2000    |
| Total Lost time (s)               | 6.0                | 6.0                 |              | 6.0            | 6.0           |            | 6,0   | 6.0                   |      | 6.0              | 6.0                      |         |
| Lane Util. Factor                 | 1.00               | 0.95                |              | 1.00           | 0.95          |            | 1.00  | 1.00                  |      | 1.00             | 1.00                     |         |
| Frt                               | 1.00               | 0.98                |              | 1.00           | 0.97          |            | 1.00  | 0.97                  |      | 1.00             | 0.99                     |         |
| Flt Protected                     | 0.95               | 1.00                |              | 0.95           | 1.00          |            | 0.95  | 1.00                  |      | 0.95             | 1.00                     |         |
| Satd. Flow (prot)                 | 1863               | 3654                |              | 1863           | 3630          |            | 1863  | 1900                  |      | 1863             | 1943                     |         |
| Flt Permitted                     | 0.95               | 1.00                |              | 0.95           | 1.00          |            | 0.95  | 1.00                  |      | 0.95             | 1.00                     |         |
| Satd. Flow (perm)                 | 1863               | 3654                |              | 1863           | 3630          |            | 1863  | 1900                  |      | 1863             | 1943                     |         |
| Peak-hour factor, PHF             | 0.90               | 0.90                | 0.90         | 0.92           | 0.92          | 0.92       | 0.89  | 0.89                  | 0.89 | 0.90             | 0.90                     | 0.90    |
| Adj. Flow (vph)                   | 67                 | 666                 | 97           | 192            | 643           | 132        | 108   | 415                   | 108  | 89               | 363                      | 23      |
| RTOR Reduction (vph)              | 0                  | 13                  | 0            | 0              | 18            | 0          | 0     | 9                     | 0    | 0                | 2                        | 0       |
| Lane Group Flow (vph)             | 67                 | 750                 | 0            | 192            | 757           | 0          | 108   | 514                   | 0    | 89               | 384                      | 0       |
| Turn Type                         | Prot               |                     |              | Prot           |               |            | Prot  |                       |      | Prot             |                          |         |
| Protected Phases                  | 5                  | 2                   |              | 1              | 6             |            | 3     | 8                     |      | 7                | 4                        |         |
| Permitted Phases                  |                    |                     |              |                |               |            |       |                       |      |                  |                          |         |
| Actuated Green, G (s)             | 7.3                | 20.9                |              | 10.9           | 24.5          |            | 8.9   | 25.8                  |      | 8.4              | 25.3                     |         |
| Effective Green, g (s)            | 7.3                | 20.9                |              | 10.9           | 24.5          |            | 8.9   | 25.8                  |      | 8.4              | 25.3                     |         |
| Actuated g/C Ratio                | 0.08               | 0.23                |              | 0.12           | 0.27          |            | 0.10  | 0.29                  |      | 0.09             | 0.28                     |         |
| Clearance Time (s)                | 6.0                | 6.0                 |              | 6.0            | 6.0           |            | 6.0   | 6.0                   |      | 6.0              | 6.0                      |         |
| Vehicle Extension (s)             | 3.0                | 3.0                 |              | 3.0            | 3.0           |            | 3.0   | 3.0                   |      | 3.0              | 3.0                      |         |
| Lane Grp Cap (vph)                | 151                | 849                 |              | 226            | 988           |            | 184   | 545                   |      | 174              | 546                      | <u></u> |
| v/s Ratio Prot                    | 0.04               | c0.21               |              | c0.10          | c0.21         | Strate -   | c0.06 | c0.27                 |      | 0.05             | 0.20                     |         |
| v/s Ratio Perm                    | an an Can Braid a' | 313-15 TATIOT TATIO |              | aliyan shakeda | 997.507.504.0 |            |       | 1917: 707: 1919<br>19 |      | wila Fe Fi Birk. | and shi të të të të shte |         |
| v/c Ratio                         | 0.44               | 0.88                |              | 0.85           | 0.77          |            | 0.59  | 0.94                  |      | 0.51             | 0.70                     |         |
| Uniform Delay, d1                 | 39.4               | 33.4                |              | 38.7           | 30.1          |            | 38.8  | 31.4                  |      | 38.8             | 29.0                     |         |
| Progression Factor                | 1.00               | 1.00                |              | 1.07           | 1.31          |            | 1.43  | 0.67                  |      | 1.00             | 1.00                     |         |
| Incremental Delay, d2             | 2.1                | 12.9                |              | 11.1           | 2.3           |            | 4.4   | 23.8                  |      | 2.5              | 4.1                      |         |
| Delay (s)                         | 41.5               | 46.3                |              | 52.6           | 41.7          |            | 60.1  | 44.7                  |      | 41.4             | 33.1                     |         |
| Level of Service                  | D                  | D                   |              | D              | D             |            | E     | D                     |      | D                | С                        |         |
| Approach Delay (s)                |                    | 45.9                |              |                | 43.9          |            |       | 47.3                  |      |                  | 34.6                     |         |
| Approach LOS                      |                    | D                   |              |                | D             |            |       | D                     |      |                  | С                        |         |
| Intersection Summary              |                    |                     |              |                |               |            |       |                       |      |                  |                          |         |
| HCM Average Control Delay         |                    |                     | 43.7         | H              | CM Level      | of Servic  | е     |                       | D    |                  |                          |         |
| HCM Volume to Capacity rati       | 0                  |                     | 0.88         |                |               |            |       |                       |      |                  |                          |         |
| Actuated Cycle Length (s)         |                    |                     | 90.0         | Si             | um of lost    | time (s)   |       |                       | 24.0 |                  |                          |         |
| Intersection Capacity Utilization | on                 |                     | 77.5%        | IC             | U Level c     | of Service |       |                       | D    |                  |                          |         |
| Analysis Period (min)             |                    |                     | 15           |                |               |            |       |                       |      |                  |                          |         |
| c Critical Lane Group             |                    |                     |              |                |               |            |       |                       |      |                  |                          |         |

|                                   | ٨    |  | 7                         | *           | 4           | ٩.           | ٩    | ĥ       | p                  | \$          | Ť                    | ~                |
|-----------------------------------|------|--|---------------------------|-------------|-------------|--------------|------|---------|--------------------|-------------|----------------------|------------------|
| Movement                          | EBL  | EBT  | EBR                       | WBL         | WBT         | WBR          | NBL  | NBT     | NBR                | SBL         | SBT                  | SBR              |
| Lane Configurations               | ኻ    | <u></u><br>ትኈ  |                           | ኻ           | <b>Å</b>    | ŕ            | ኻ    | ĥ       |                    | ሻ           | ĥ                    |                  |
| Volume (vph)                      | 18   | 1096   | 19                        | 101         | 1093        | 464          | 50   | 64      | 218                | 344         | 126                  | 56               |
| Ideal Flow (vphpl)                | 2000 | 2000   | 2000                      | 2000        | 2000        | 2000         | 2000 | 2000    | 2000               | 2000        | 2000                 | 2000             |
| Lane Width                        | 12   | 12   | 12                        | 12          | 12          | 12           | 11   | 11      | 11                 | 12          | 12                   | 12               |
| Total Lost time (s)               | 6.1  | 6.1  |                           | 6.1         | 6.1         | 6.1          | 6.0  | 6.0     |                    | 6.0         | 6.0                  | anta historia de |
| Lane Util. Factor                 | 1.00 | 0.95   |                           | 1.00        | 1.00        | 1.00         | 1.00 | 1.00    |                    | 1.00        | 1.00                 |                  |
| Frt                               | 1.00 | 1.00   |                           | 1.00        | 1.00        | 0.85         | 1.00 | 0.88    |                    | 1.00        | 0.95                 | 1.19115-1.13     |
| Flt Protected                     | 0.95 | 1.00   |                           | 0.95        | 1.00        | 1.00         | 0.95 | 1.00    |                    | 0.95        | 1.00                 |                  |
| Satd. Flow (prot)                 | 1863 | 3716   |                           | 1863        | 1961        | 1500         | 1801 | 1676    |                    | 1863        | 1870                 |                  |
| Flt Permitted                     | 0.13 | 1.00   |                           | 0.11        | 1.00        | 1.00         | 0.63 | 1.00    |                    | 0.26        | 1.00                 |                  |
| Satd. Flow (perm)                 | 248  | 3716   |                           | 208         | 1961        | 1500         | 1200 | 1676    |                    | 519         | 1870                 |                  |
| Peak-hour factor, PHF             | 0.88 | 0.88   | 0.88                      | 0.92        | 0.92        | 0.92         | 0.94 | 0.94    | 0.94               | 0.92        | 0.92                 | 0.92             |
| Adj. Flow (vph)                   | 20   | 1245   | 22                        | 110         | 1188        | 504          | 53   | 68      | 232                | 374         | 137                  | 61               |
| RTOR Reduction (vph)              | 20   | 1  | 0                         | 0           | 0           | 175          | 0    | 0       | 202                | 0           | 19                   | 0                |
| Lane Group Flow (vph)             | 20   | 1266   | 0                         | 110         | 1188        | 329          | 53   | 300     | 0                  | 374         | 179                  | 0<br>0           |
| Parking (#/hr)                    | 20   | 1200   | Ŭ                         |             | 1100        | 0            |      | 000     | v                  |             |                      | v<br>Neverse     |
| Turn Type                         | Perm | glassia de terret  | 17 - 1999 - 1997 A. V. J. | pm+pt       |             | Perm         | Perm |         |                    | pm+pt       |                      |                  |
| Protected Phases                  | Leun | 2  |                           | - piii.br   | 6           | Leiiii       |      | 8       |                    | pm+pt<br>7  | 4                    |                  |
| Permitted Phases                  | 2    | <u>. 1999</u> - 1997 - 199<br>- 1997 - |                           | 6           | <b>0</b>    | 6            | 8    | 0       |                    | 4           | 1) (Sel)( <b>4</b> - |                  |
| Actuated Green, G (s)             | 31.6 | 31.6   |                           | 44.0        | 44.0        | 44.0         | 19.9 | 19.9    |                    | 33.9        | 33.9                 |                  |
| Effective Green, g (s)            | 31.6 | 31.6   | 10×3.0903                 | 44.0        | 44.0        | 44.0         | 19.9 | 19.9    |                    | 33.9        | 33.9                 |                  |
| Actuated g/C Ratio                | 0.35 | 0.35   |                           | 0.49        | 0.49        | 0.49         | 0.22 | 0.22    |                    | 0.38        | 0.38                 |                  |
| Clearance Time (s)                | 6.1  | 0.55<br>6.1  |                           | 0.49<br>6.1 | 0.49<br>6.1 | 0.45<br>6.1  | 6.0  | 6.0     |                    | 0.38<br>6.0 | 6.0                  |                  |
| Vehicle Extension (s)             | 3.0  | 3.0  | 100000                    | 3.0         | 3.0         | 0.1<br>3.0   | 3.0  | 3.0     | 1997 1979          | 0.0<br>3.0  | 3.0                  |                  |
|                                   |      |  | (* 5 ST ( 1993 S.)        | ů.          |             |              |      |         | n Shi Alabiya<br>T |             |                      | VERMON S         |
| Lane Grp Cap (vph)                | 87   | 1305   |                           | 218         | 959         | 733          | 265  | 371     |                    | 315         | 704                  |                  |
| v/s Ratio Prot                    |      | 0.34   |                           | 0.04        | c0.61       | 0.00         | 0.04 | 0.18    |                    | c0.11       | 0.10                 |                  |
| v/s Ratio Perm                    | 0.08 | 0.07   |                           | 0.21        |             | 0.22         | 0.04 | • • • • |                    | c0.34       | 0.05                 |                  |
| v/c Ratio                         | 0.23 | 0.97   |                           | 0.50        | 1.24        | 0.45         | 0.20 | 0.81    |                    | 1.19        | 0.25                 |                  |
| Uniform Delay, d1                 | 20.6 | 28.7   |                           | 19.2        | 23.0        | 15.1         | 28.6 | 33.2    |                    | 26.5        | 19.3                 |                  |
| Progression Factor                | 1.08 | 0.97   |                           | 1.00        | 1.00        | 1.00         | 1.00 | 1.00    |                    | 1.00        | 1.00                 |                  |
| Incremental Delay, d2             | 5.6  | 17.8   |                           | 1.8         | 116.4       | 2.0          | 0.4  | 12.2    |                    | 111.6       | 0.2                  |                  |
| Delay (s)                         | 27.9 | 45.7   |                           | 21.0        | 139.4       | 17.0         | 28.9 | 45.5    |                    | 138.1       | 19.5                 |                  |
| Level of Service                  | С    | D  |                           | С           | F           | В            | С    | D       |                    | F           | В                    |                  |
| Approach Delay (s)                |      | 45.5   |                           |             | 98.0        |              |      | 43.0    |                    |             | 97.1                 |                  |
| Approach LOS                      |      | D  |                           |             | F           |              |      | D       |                    |             | F                    |                  |
| Intersection Summary              |      |  |                           |             |             |              |      |         |                    |             |                      |                  |
| HCM Average Control Delay         |      |  | 76.2                      | H           | CM Level    | of Service   | е    |         | E                  |             |                      |                  |
| HCM Volume to Capacity ratio      |      |  | 1.18                      |             |             |              |      |         |                    |             |                      |                  |
| Actuated Cycle Length (s)         |      |  | 90.0                      | Si          | um of lost  | time (s)     |      |         | 12.1               |             |                      |                  |
| Intersection Capacity Utilization |      |  | 117.2%                    |             |             | of Service   |      |         | Н                  |             |                      |                  |
| Analysis Period (min)             |      |  | 15                        |             |             |              |      |         |                    |             |                      |                  |
| c Critical Lane Group             |      |  |                           |             |             | <u>(888)</u> |      |         |                    |             |                      |                  |

Appendix C

2015 and 2030 Traffic Volume Detail With National Street

| <i>a</i> •  | No  | rthbou | ınd | So  | uthbou | nd    | E   | astbou | nd  | W   | estbou | nd  |       |
|---|-----|--------|-----|-----|--------|-------|-----|--------|-----|-----|--------|-----|-------|
| Scenario  | LT  | TH     | RT  | LT  | TH     | RT    | LT  | TH     | RT  | LT  | TH     | RT  | Total |
|   |     |        |     |     | AN     | M PEA | K   |        |     |     |        | 1   | 1     |
| Existing  | 120 | 417    | -   | -   | 678    | 127   | 214 | -      | 75  | -   | -      | -   | 1631  |
| Background<br>2015                                    | 105 | 459    | -   | -   | 786    | 118   | 276 | -      | 100 | -   | -      | -   | 1,844 |
| Background<br>2030                                    | 122 | 533    | -   | -   | 983    | 148   | 320 | -      | 125 | -   | -      | -   | 2,231 |
| Use National<br>St. Ext.                              | -   | -57    | 57  | -   | -48    | -9    | -29 | 29     | -   | 47  | 10     | -   | 0     |
| Future 2015<br>w/ National<br>St. Ext.                | 105 | 402    | 57  | -   | 738    | 109   | 247 | 29     | 100 | 47  | 10     | -   | 1,844 |
| National St.<br>Ext.<br>Development                   | -   | -      | 237 | 366 | -      | -     | -   | 130    | -   | 110 | 34     | 85  | 962   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 105 | 402    | 294 | 366 | 738    | 109   | 247 | 159    | 100 | 157 | 44     | 85  | 2,806 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 122 | 467    | 341 | 425 | 923    | 136   | 287 | 185    | 125 | 182 | 51     | 99  | 3,343 |
| <b>c</b> •  | No  | rthbou | ınd | So  | uthbou | nd    | Ε   | astbou | nd  | W   | estbou | nd  | Total |
| Scenario  | LT  | TH     | RT  | LT  | TH     | RT    | LT  | TH     | RT  | LT  | TH     | RT  |       |
|   |     |        |     |     | PN     | A PEA | K   |        |     | •   |        |     |       |
| Existing  | 84  | 408    | -   | -   | 650    | 191   | 520 | -      | 240 | -   | -      | -   | 2,093 |
| Background<br>2015                                    | 75  | 448    | -   | -   | 755    | 178   | 676 | -      | 329 | -   | -      | -   | 2,461 |
| Background<br>2030                                    | 87  | 520    | -   | -   | 944    | 223   | 785 | -      | 411 | -   | -      | -   | 2,970 |
| Use National<br>St. Ext.                              | -   | -44    | 44  | -   | -155   | -46   | -55 | 55     | -   | 155 | 46     | -   | 0     |
| Future 2015<br>w/ National<br>St. Ext.                | 75  | 404    | 44  | -   | 600    | 132   | 621 | 55     | 329 | 155 | 46     | -   | 2,461 |
| National St.<br>Ext.<br>Development                   | -   | -      | 96  | 162 | -      | -     | -   | 96     | -   | 322 | 100    | 294 | 1,070 |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 75  | 404    | 140 | 162 | 600    | 132   | 621 | 151    | 329 | 477 | 146    | 294 | 3,531 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 87  | 469    | 163 | 188 | 750    | 165   | 721 | 175    | 411 | 554 | 170    | 341 | 4,194 |

Table C1: Traffic at D-19/I-96 WB Ramps

| <b>S</b>  | N  | orthbou | nd  | So | outhbou | nd    | E  | astbou | nd | W  | estbou | nd | T-4-1 |
|---|----|---------|-----|----|---------|-------|----|--------|----|----|--------|----|-------|
| Scenario  | LT | ТН      | RT  | LT | ТН      | RT    | LT | ТН     | RT | LT | TH     | RT | Total |
|   | I  |         |     | 1  | AN      | I PEA | K  |        |    | 1  |        |    |       |
| Existing  | -  | 672     | 31  | 1  | 679     | -     | -  | -      | -  | 6  | -      | 6  | 1,395 |
| Background<br>2015                                    | -  | 742     | 34  | 1  | 750     | -     | -  | -      | -  | 7  | -      | 7  | 1,541 |
| Background<br>2030                                    | -  | 862     | 40  | 1  | 871     | -     | -  | -      | -  | 8  | -      | 8  | 1,790 |
| Use National<br>St. Ext.                              | -  | -86     | -   | -  | -57     | -     | -  | -      | -  | -  | -      | -  | -143  |
| Future 2015<br>w/ National<br>St. Ext.                | -  | 656     | 34  | 1  | 693     | -     | -  | -      | -  | 7  | -      | 7  | 1,398 |
| National St.<br>Ext.<br>Development                   | -  | 81      | 4   | -  | 363     | -     | -  | -      | -  | 3  | -      | -  | 451   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | -  | 737     | 38  | 1  | 1,056   | -     | -  | -      | -  | 10 | -      | 7  | 1,849 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | -  | 856     | 44  | 1  | 1,226   | -     | -  | -      | -  | 11 | -      | 8  | 2,146 |
| Scenario  | N  | orthbou | nd  | So | outhbou | nd    | E  | astbou | nd | W  | estbou | nd | Total |
| Scenario  | LR | ТН      | RT  | LT | ТН      | RT    | LT | ТН     | RT | LT | TH     | RT | Total |
|   |    |         | •   | •  | PN      | I PEA | K  | •      | •  | •  |        | •  |       |
| Existing  | -  | 747     | 61  | 3  | 781     | -     | -  | -      | -  | 6  | -      | 0  | 1,598 |
| Background<br>2015                                    | -  | 825     | 67  | 3  | 863     | -     | -  | -      | -  | 7  | -      | 0  | 1,765 |
| Background<br>2030                                    | -  | 958     | 78  | 4  | 1,002   | -     | -  | -      | -  | 8  | -      | 0  | 2,050 |
| Use National<br>St. Ext.                              | -  | -99     | -   | -  | -201    | -     | -  | -      | -  | -  | -      | -  | -300  |
| Future 2015<br>w/ National<br>St. Ext.                | -  | 726     | 67  | 3  | 662     | -     | -  | -      | -  | 7  | -      | 0  | 1,465 |
| National St.<br>Ext.<br>Development                   | -  | 269     | 25  | -  | 158     | -     | -  | -      | -  | 4  | -      | -  | 456   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | -  | 995     | 92  | 3  | 820     | -     | -  | -      | -  | 11 | -      | 0  | 1,921 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | -  | 1,355   | 107 | 4  | 952     | -     | -  | -      | -  | 12 | -      | 0  | 2,430 |

 Table C2: Traffic at D-19 (Pinckney Road)/Pulford St.

| <b>a</b> .  | No  | rthbou | nd | So | uthbou | ınd   | Ea  | astbou | nd  | W   | estbou | nd |       |
|---|-----|--------|----|----|--------|-------|-----|--------|-----|-----|--------|----|-------|
| Scenario  | LT  | TH     | RT | LT | TH     | RT    | LT  | ТН     | RT  | LT  | TH     | RT | Total |
|   |     |        |    |    | AN     | M PEA | K   |        |     |     |        |    |       |
| Existing  | 143 | 393    | 48 | 2  | 447    | 29    | 143 | 153    | 167 | 121 | 68     | 10 | 1724  |
| Background<br>2015                                    | 158 | 434    | 53 | 2  | 494    | 32    | 158 | 169    | 184 | 134 | 75     | 11 | 1,904 |
| Background<br>2030                                    | 183 | 504    | 62 | 3  | 573    | 37    | 183 | 196    | 214 | 155 | 87     | 13 | 2,210 |
| Use National<br>St. Ext.                              | -   | -86    | -  | -  | -57    | -     | -   | -      | -   | -   | -      | -  | -143  |
| Future 2015<br>w/ National<br>St. Ext.                | 158 | 348    | 53 | 3  | 437    | 32    | 158 | 169    | 184 | 134 | 75     | 11 | 1,816 |
| National St.<br>Ext.<br>Development                   | 10  | 65     | 6  | -  | 220    | -     | -   | -      | 83  | 60  | -      | 60 | 504   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 168 | 413    | 59 | 2  | 657    | 32    | 158 | 169    | 267 | 194 | 75     | 71 | 2,265 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 195 | 480    | 69 | 3  | 767    | 37    | 183 | 196    | 311 | 225 | 87     | 82 | 2,630 |
| Scenario  | No  | rthbou | nd | So | uthbou | nd    | Ea  | astbou | nd  | W   | estbou | nd | Total |
| Scenario  | LT  | TH     | RT | LT | TH     | RT    | LT  | ТН     | RT  | LT  | TH     | RT | Total |
|   |     |        |    |    | PN     | A PEA | K   |        |     |     |        |    |       |
| Existing  | 225 | 628    | 54 | 3  | 497    | 130   | 100 | 143    | 220 | 129 | 243    | 4  | 2,376 |
| Background 2015                                       | 249 | 694    | 60 | 3  | 549    | 144   | 110 | 158    | 243 | 142 | 268    | 4  | 2,624 |
| Background<br>2030                                    | 289 | 805    | 69 | 4  | 637    | 167   | 128 | 183    | 282 | 165 | 312    | 5  | 3,046 |
| Use National<br>St. Ext.                              | -   | -99    | -  | -  | -201   | -     | -   | -      | -   | -   | -      | -  | -300  |
| Future 2015<br>w/ National<br>St. Ext.                | 249 | 595    | 60 | 3  | 348    | 144   | 110 | 158    | 243 | 142 | 268    | 4  | 2,324 |
| National St.<br>Ext.<br>Development                   | 74  | 178    | 17 | -  | 86     | -     | -   | -      | 45  | 27  | -      | -  | 427   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 323 | 773    | 77 | 3  | 434    | 144   | 110 | 158    | 288 | 169 | 268    | 4  | 2,751 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 374 | 897    | 89 | 4  | 504    | 167   | 128 | 183    | 334 | 197 | 312    | 5  | 3,194 |

Table C3: Traffic at Pinckney (Michigan)/Marion St. (Mason)

|   | No | orthbou | Ind | So | uthbou | nd    | E  | astbou | nd | W  | estbou  | nd |       |
|---|----|---------|-----|----|--------|-------|----|--------|----|----|---------|----|-------|
| Scenario  | LT | TH      | RT  | LT | TH     | RT    | LT | TH     | RT | LT | TH      | RT | Total |
|   |    |         | I   |    |        | M PEA |    |        |    |    |         |    | I     |
| Existing  | 21 | 574     | 12  | 9  | 484    | 6     | 2  | 0      | 30 | 6  | 3       | 3  | 1,150 |
| Background<br>2015                                    | 23 | 634     | 13  | 10 | 535    | 7     | 2  | 0      | 33 | 7  | 3       | 3  | 1,270 |
| Background<br>2030                                    | 27 | 736     | 15  | 12 | 621    | 8     | 3  | 0      | 38 | 8  | 4       | 4  | 1,476 |
| Use National<br>St. Ext.                              | -  | -86     | -   | -  | -57    | -     | -  | -      | -  | -  | -       | -  | -143  |
| Future 2015<br>w/ National<br>St. Ext.                | 23 | 548     | 13  | 10 | 478    | 7     | 2  | 0      | 33 | 7  | 3       | 3  | 1,127 |
| National St.<br>Ext.<br>Development                   | 3  | 60      | 2   | -  | 205    | -     | -  | -      | 12 | 3  | -       | -  | 285   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 26 | 608     | 15  | 10 | 683    | 7     | 2  | 0      | 45 | 10 | 3       | 3  | 1,412 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 30 | 706     | 18  | 12 | 793    | 8     | 3  | 0      | 52 | 11 | 4       | 4  | 1,641 |
| Scenario  | No | orthbou | ind | So | uthbou | nd    | E  | astbou | nd | W  | 'estbou | nd | Total |
| Stenario  | LT | TH      | RT  | LT | TH     | RT    | LT | TH     | RT | LT | TH      | RT | Total |
|   |    |         |     |    |        | A PEA |    |        |    |    |         |    |       |
| Existing  | 52 | 721     | 13  | 12 | 616    | 63    | 3  | 7      | 4  | 5  | 0       | 4  | 1,500 |
| Background<br>2015                                    | 57 | 796     | 14  | 13 | 680    | 70    | 3  | 8      | 4  | 6  | 0       | 4  | 1,655 |
| Background<br>2030                                    | 67 | 925     | 17  | 15 | 790    | 81    | 4  | 9      | 5  | 6  | 0       | 5  | 1,924 |
| Use National<br>St. Ext.                              | -  | -99     | -   | -  | -201   | -     | -  | -      | -  | -  | -       | -  | -300  |
| Future 2015<br>w/ National<br>St. Ext.                | 57 | 697     | 14  | 13 | 479    | 70    | 3  | 8      | 4  | 6  | 0       | 4  | 1,355 |
| National St.<br>Ext.<br>Development                   | 13 | 161     | 4   | -  | 83     | -     | -  | -      | -  | 3  | -       | -  | 264   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 70 | 858     | 18  | 13 | 562    | 70    | 3  | 8      | 4  | 9  | 0       | 4  | 1,619 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 82 | 997     | 21  | 15 | 653    | 81    | 4  | 9      | 5  | 10 | 0       | 5  | 1,882 |

Table C4: Traffic at Michigan (M-155)/Livingston St.

| ~ .   | No  | rthbou | ınd | So | uthbou | nd    | E  | astbou | nd | W  | estbou | nd |       |
|---|-----|--------|-----|----|--------|-------|----|--------|----|----|--------|----|-------|
| Scenario  | LT  | TH     | RT  | LT | TH     | RT    | LT | TH     | RT | LT | TH     | RT | Total |
|   |     |        |     |    | AN     | A PEA | K  |        |    |    |        |    |       |
| Existing  | 55  | 367    | 99  | 20 | 469    | 1     | 2  | 3      | 30 | 9  | 3      | 10 | 1,068 |
| Background<br>2015                                    | 61  | 405    | 109 | 22 | 518    | 1     | 2  | 3      | 33 | 10 | 3      | 11 | 1,178 |
| Background<br>2030                                    | 71  | 471    | 127 | 26 | 601    | 1     | 3  | 4      | 38 | 12 | 4      | 13 | 1,371 |
| Use National<br>St. Ext.                              | -   | -70    | -16 | -  | -48    | -     | -  | -      | -  | -8 | -      | -  | -142  |
| Future 2015<br>w/ National<br>St. Ext.                | 61  | 335    | 93  | 22 | 470    | 1     | 2  | 3      | 33 | 2  | 3      | 11 | 1,036 |
| National St.<br>Ext.<br>Development                   | 4   | 50     | 6   | -  | 189    | -     | -  | -      | 12 | 4  | -      | -  | 265   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 65  | 385    | 99  | 22 | 659    | 1     | 2  | 3      | 45 | 6  | 3      | 11 | 1,301 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 75  | 447    | 115 | 26 | 765    | 1     | 3  | 4      | 52 | 7  | 4      | 13 | 1,512 |
| Scenario  | No  | rthbou | ınd | So | uthbou | nd    | E  | astbou | nd | W  | estbou | nd | Total |
| Scenario  | LT  | TH     | RT  | LT | TH     | RT    | LT | TH     | RT | LT | TH     | RT | 10141 |
|   | -   |        |     |    |        | A PEA | K  | -      |    | -  |        |    |       |
| Existing  | 75  | 440    | 99  | 55 | 651    | 5     | 1  | 2      | 13 | 12 | 5      | 16 | 1,374 |
| Background<br>2015                                    | 83  | 486    | 109 | 61 | 719    | 6     | 1  | 2      | 14 | 13 | 6      | 18 | 1,518 |
| Background<br>2030                                    | 96  | 564    | 127 | 71 | 835    | 6     | 1  | 3      | 17 | 15 | 6      | 21 | 1,762 |
| Use National<br>St. Ext.                              | -   | -99    | -   | -  | -201   | -     | -  | -      | -  | -  | -      | -  | -300  |
| Future 2015<br>w/ National<br>St. Ext.                | 83  | 387    | 109 | 61 | 518    | 6     | 1  | 2      | 14 | 13 | 6      | 18 | 1,218 |
| National St.<br>Ext.<br>Development                   | 22  | 109    | 30  | -  | 79     | -     | -  | -      | 2  | 2  | -      | -  | 244   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 105 | 496    | 139 | 61 | 597    | 6     | 1  | 2      | 16 | 15 | 6      | 18 | 1,462 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 122 | 576    | 162 | 71 | 693    | 6     | 1  | 3      | 19 | 18 | 6      | 21 | 1,698 |

Table C5: Traffic at Michigan (M-155)/Washington St.

| ~ .   | No  | rthbou | ınd | So | uthbou | nd    | Ε  | astbou | nd  | W   | estbou | nd  |       |
|---|-----|--------|-----|----|--------|-------|----|--------|-----|-----|--------|-----|-------|
| Scenario  | LT  | TH     | RT  | LT | TH     | RT    | LT | TH     | RT  | LT  | TH     | RT  | Total |
|   |     |        |     |    | A      | M PEA | ٩K |        |     |     |        |     |       |
| Existing  | 56  | 137    | 86  | 40 | 242    | 9     | 17 | 396    | 59  | 58  | 413    | 11  | 1,524 |
| Background<br>2015                                    | 62  | 151    | 95  | 44 | 267    | 10    | 19 | 437    | 65  | 64  | 456    | 12  | 1,682 |
| Background<br>2030                                    | 72  | 176    | 110 | 51 | 310    | 12    | 22 | 508    | 76  | 74  | 530    | 14  | 1,955 |
| Use National<br>St. Ext.                              | -   | -      | -52 | -  | -      | -     | -  | -      | -   | -35 | -      | -   | -87   |
| Future 2015<br>w/ National<br>St. Ext.                | 62  | 151    | 43  | 44 | 267    | 10    | 19 | 437    | 65  | 29  | 456    | 12  | 1,595 |
| National St.<br>Ext.<br>Development                   | 10  | 40     | -   | -  | 151    | -     | -  | 154    | 38  | -   | 45     | -   | 438   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 72  | 191    | 43  | 44 | 418    | 10    | 19 | 591    | 103 | 29  | 501    | 12  | 2,033 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 83  | 222    | 50  | 51 | 486    | 12    | 22 | 687    | 120 | 34  | 582    | 14  | 2,363 |
| <u>G</u>  | No  | rthbou | ınd | So | uthbou | ind   | E  | astbou | nd  | W   | estbou | nd  | T-4-1 |
| Scenario  | LT  | TH     | RT  | LT | TH     | RT    | LT | TH     | RT  | LT  | TH     | RT  | Total |
|   |     |        |     |    | P      | M PEA | K  |        |     |     |        |     |       |
| Existing  | 75  | 288    | 75  | 62 | 255    | 16    | 47 | 467    | 68  | 138 | 462    | 94  | 2,047 |
| Background<br>2015                                    | 83  | 318    | 83  | 68 | 282    | 18    | 52 | 516    | 75  | 152 | 510    | 104 | 2,261 |
| Background<br>2030                                    | 96  | 369    | 96  | 80 | 327    | 21    | 60 | 599    | 87  | 177 | 592    | 121 | 2,625 |
| Use National<br>St. Ext.                              | -   | -      | -46 | -  | -      | -     | -  | -      | -   | -86 | -      | -   | -132  |
| Future 2015<br>w/ National<br>St. Ext.                | 83  | 318    | 37  | 68 | 282    | 18    | 52 | 516    | 75  | 66  | 510    | 104 | 2,129 |
| National St.<br>Ext.<br>Development                   | 22  | 87     | -   | -  | 63     | -     | -  | 70     | 16  | -   | 146    | -   | 404   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 105 | 405    | 37  | 68 | 345    | 18    | 52 | 586    | 91  | 66  | 656    | 104 | 2,533 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 122 | 470    | 43  | 80 | 400    | 21    | 60 | 680    | 106 | 77  | 762    | 121 | 2,942 |

Table C6: Traffic at Grand River/Michigan (M-155)

|   | No | orthbou | und | So | outhbo | und   | E  | astbou | nd | W   | estbou | nd |       |
|---|----|---------|-----|----|--------|-------|----|--------|----|-----|--------|----|-------|
| Scenario  | LT | ТН      | RT  | LT | TH     | RT    | LT | TH     | RT | LT  | TH     | RT | Total |
|   |    |         |     |    | A      | M PEA | K  |        |    |     |        |    |       |
| Existing  | 1  | -       | 61  | -  | -      | -     | -  | 531    | 8  | 34  | 493    | -  | 1,128 |
| Background<br>2015                                    | 1  | -       | 67  | -  | -      | -     | -  | 587    | 9  | 38  | 545    | -  | 1,247 |
| Background<br>2030                                    | 1  | -       | 78  | -  | -      | -     | -  | 681    | 10 | 44  | 632    | -  | 1,446 |
| Use National<br>St. Ext.                              | -  | -       | -13 | -  | -      | -     | -  | -52    | -  | -15 | -35    | -  | -115  |
| Future 2015<br>w/ National<br>St. Ext.                | 1  | -       | 54  | -  | -      | -     | -  | 535    | 9  | 23  | 510    | -  | 1,132 |
| National St.<br>Ext.<br>Development                   | -  | -       | -   | -  | -      | -     | -  | 75     | -  | -   | 45     | -  | 120   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 1  | -       | 54  | -  | -      | -     | -  | 610    | 9  | 23  | 555    | -  | 1,252 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 1  | -       | 63  | -  | -      | -     | -  | 708    | 10 | 26  | 644    | -  | 1,452 |
| Scenario  | No | orthbou | und | So | outhbo | und   | E  | astbou | nd | W   | estbou | nd | Total |
| Scenario  | LT | TH      | RT  | LT | TH     | RT    | LT | TH     | RT | LT  | TH     | RT | Total |
|   |    |         |     |    | P      | M PEA | K  |        |    |     |        |    |       |
| Existing  | 3  | -       | 47  | -  | -      | -     | -  | 751    | 24 | 104 | 772    | -  | 1,701 |
| Background<br>2015                                    | 3  | -       | 52  | -  | -      | -     | -  | 830    | 27 | 115 | 853    | -  | 1,880 |
| Background<br>2030                                    | 4  | -       | 60  | -  | -      | -     | -  | 963    | 31 | 133 | 990    | -  | 2,181 |
| Use National<br>St. Ext.                              | -  | -       | -15 | -  | -      | -     | -  | -46    | -  | -75 | -86    | -  | -222  |
| Future 2015<br>w/ National<br>St. Ext.                | 3  | -       | 37  | -  | -      | -     | -  | 784    | 27 | 40  | 767    | -  | 1,658 |
| National St.<br>Ext.<br>Development                   | -  | -       | -   | -  | -      | -     | -  | 55     | -  | -   | 85     | -  | 140   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 3  | -       | 37  | -  | -      | -     | -  | 839    | 27 | 40  | 852    | -  | 1,798 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 4  | -       | 43  | -  | -      | -     | -  | 974    | 31 | 46  | 989    | -  | 2,087 |

Table C7: Traffic at Grand River/Court St.

| ~ .   | No | rthbou | ınd | So | uthbou | ınd   | E  | astbou | nd | W   | estbou | nd |       |
|---|----|--------|-----|----|--------|-------|----|--------|----|-----|--------|----|-------|
| Scenario  | LT | TH     | RT  | LT | TH     | RT    | LT | TH     | RT | LT  | TH     | RT | Total |
|   |    |        |     |    | A      | M PEA | ٩K |        |    | 1   |        |    |       |
| Existing  | 3  | 1      | 26  | 13 | 3      | 10    | 5  | 579    | 13 | 41  | 572    | 1  | 1,267 |
| Background<br>2015                                    | 3  | 1      | 29  | 14 | 3      | 11    | 6  | 640    | 14 | 45  | 632    | 1  | 1,399 |
| Background<br>2030                                    | 4  | 1      | 33  | 17 | 4      | 13    | 6  | 743    | 17 | 53  | 734    | 1  | 1,626 |
| Use National<br>St. Ext.                              | -  | -      | -4  | -  | -      | -     | -  | -65    | -  | -2  | -50    | -  | -121  |
| Future 2015<br>w/ National<br>St. Ext.                | 3  | 1      | 25  | 14 | 3      | 11    | 6  | 575    | 14 | 43  | 582    | 1  | 1,278 |
| National St.<br>Ext.<br>Development                   | -  | -      | -   | -  | -      | -     | -  | 154    | -  | -   | 45     | -  | 199   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 3  | 1      | 25  | 14 | 3      | 11    | 6  | 729    | 14 | 43  | 627    | 1  | 1,477 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 4  | 1      | 29  | 17 | 4      | 13    | 6  | 846    | 17 | 50  | 728    | 1  | 1,716 |
| Scenario  | No | rthbou | ınd | So | uthbou | ınd   | E  | astbou | nd | W   | estbou | nd | Total |
| Scenario  | LT | ТН     | RT  | LT | ТН     | RT    | LT | TH     | RT | LT  | ТН     | RT | Total |
|   |    |        |     |    | P      | M PEA | AK |        |    |     |        |    |       |
| Existing  | 3  | 10     | 58  | 9  | 2      | 20    | 38 | 718    | 13 | 32  | 696    | 13 | 1,612 |
| Background<br>2015                                    | 3  | 11     | 64  | 10 | 2      | 22    | 42 | 793    | 14 | 35  | 769    | 14 | 1,779 |
| Background<br>2030                                    | 4  | 13     | 74  | 12 | 3      | 26    | 49 | 921    | 17 | 41  | 893    | 17 | 2,070 |
| Use National<br>St. Ext.                              | -  | -      | -11 | -  | -      | -     | -  | -61    | -  | -21 | -161   | -  | -254  |
| Future 2015<br>w/ National<br>St. Ext.                | 3  | 11     | 53  | 10 | 2      | 22    | 42 | 732    | 14 | 14  | 608    | 14 | 1,525 |
| National St.<br>Ext.<br>Development                   | -  | -      | -   | -  | -      | -     | -  | 70     | -  | -   | 146    | -  | 216   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 3  | 11     | 53  | 10 | 2      | 22    | 42 | 802    | 14 | 14  | 754    | 14 | 1,741 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 4  | 13     | 62  | 12 | 3      | 26    | 49 | 931    | 17 | 17  | 875    | 17 | 2,026 |

Table C8: Traffic at Grand River/Barnard St.

| <i>a</i> .  | No | orthbou | ind | So | uthbou | ind   | E  | astbour  | nd | W   | estbou | nd |       |
|---|----|---------|-----|----|--------|-------|----|----------|----|-----|--------|----|-------|
| Scenario  | LT | TH      | RT  | LT | TH     | RT    | LT | TH       | RT | LT  | TH     | RT | Total |
|   | 1  |         |     | 1  | A      | M PEA | 4K |          |    | 1   |        |    |       |
| Existing  | 6  | -       | 104 | -  | -      | -     | -  | 589      | 19 | 90  | 546    | -  | 1,354 |
| Background<br>2015                                    | 7  | -       | 115 | -  | -      | -     | -  | 651      | 21 | 99  | 603    | -  | 1,496 |
| Background<br>2030                                    | 8  | -       | 133 | -  | -      | -     | -  | 755      | 24 | 115 | 700    | -  | 1,735 |
| Use National<br>St. Ext.                              | -  | -       | -17 | -  | -      | -     | -  | -69      | -  | -5  | -52    | -  | -143  |
| Future 2015<br>w/ National<br>St. Ext.                | 7  | -       | 98  | -  | -      | -     | -  | 582      | 21 | 94  | 551    | -  | 1,353 |
| National St.<br>Ext.<br>Development                   | -  | -       | -   | -  | -      | -     | -  | 154      | -  | -   | 45     | -  | 199   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 7  | -       | 98  | -  | -      | -     | -  | 736      | 21 | 94  | 596    | -  | 1,552 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 8  | -       | 114 | -  | -      | -     | -  | 854      | 24 | 110 | 692    | -  | 1,802 |
| Scenario  | No | orthbou | und | So | uthbou | ınd   | E  | Castbour | nd | W   | estbou | nd | Total |
| Scenario  | LT | TH      | RT  | LT | TH     | RT    | LT | TH       | RT | LT  | TH     | RT | Total |
|   |    |         |     |    | P      | M PEA | λK |          |    |     |        |    |       |
| Existing  | 7  | -       | 140 | -  | -      | -     | -  | 826      | 15 | 152 | 747    | -  | 1,887 |
| Background<br>2015                                    | 8  | -       | 155 | -  | -      | -     | -  | 912      | 17 | 168 | 825    | -  | 2,085 |
| Background<br>2030                                    | 9  | -       | 180 | -  | -      | -     | -  | 1,059    | 19 | 195 | 958    | -  | 2,420 |
| Use National<br>St. Ext.                              | -  | -       | -27 | -  | -      | -     | -  | -72      | -  | -19 | -182   | -  | -300  |
| Future 2015<br>w/ National<br>St. Ext.                | 8  | -       | 128 | -  | -      | -     | -  | 840      | 17 | 149 | 643    | -  | 1,785 |
| National St.<br>Ext.<br>Development                   | -  | -       | -   | -  | -      | -     | -  | 70       | -  | -   | 146    | -  | 216   |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 8  | -       | 128 | -  | -      | -     | -  | 910      | 17 | 149 | 789    | -  | 2,001 |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 9  | -       | 148 | -  | -      | -     | -  | 1,057    | 19 | 173 | 916    | -  | 2,322 |

Table C9: Traffic at Grand River/Fowler St.

|   | No  | rthbou | ınd | Sou | ıthbou | nd    | F  | astbour  | ıd  | W   | estbour | ıd  | <b>T</b> ( ) |
|---|-----|--------|-----|-----|--------|-------|----|----------|-----|-----|---------|-----|--------------|
| Scenario  | LT  | TH     | RT  | LT  | ТН     | RT    | LT | TH       | RT  | LT  | ТН      | RT  | Total        |
|   |     |        |     |     | Al     | M PEA | AK |          |     | I   | 1       |     |              |
| Existing  | 7   | 12     | 143 | 165 | 19     | 9     | 4  | 632      | 6   | 54  | 633     | 105 | 1,789        |
| Background<br>2015                                    | 8   | 13     | 158 | 182 | 21     | 10    | 4  | 698      | 7   | 60  | 699     | 116 | 1,976        |
| Background<br>2030                                    | 9   | 15     | 183 | 212 | 24     | 12    | 5  | 810      | 8   | 69  | 812     | 135 | 2,294        |
| Use National<br>St. Ext.                              | -   | -      | 86  | -   | -      | -     | -  | -86      | -   | 57  | -57     | -   | 0            |
| Future 2015<br>w/ National<br>St. Ext.                | 8   | 13     | 244 | 182 | 21     | 10    | 4  | 612      | 7   | 117 | 642     | 116 | 1,976        |
| National St.<br>Ext.<br>Development                   | 45  | 8      | 45  | -   | -      | -     | -  | -        | 154 | -   | -       | -   | 252          |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 53  | 21     | 289 | 182 | 41     | 10    | 4  | 612      | 161 | 271 | 642     | 116 | 2,402        |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 61  | 25     | 335 | 212 | 48     | 12    | 5  | 711      | 186 | 314 | 746     | 135 | 2,790        |
| Second  | No  | rthbou | ınd | Sou | ıthbou | nd    | E  | Castbour | nd  | W   | estbour | nd  | Total        |
| Scenario  | LT  | TH     | RT  | LT  | ТН     | RT    | LT | TH       | RT  | LT  | ТН      | RT  | Total        |
|   |     |        |     |     | PI     | M PEA | AK |          |     |     |         |     |              |
| Existing  | 39  | 50     | 170 | 268 | 98     | 44    | 14 | 855      | 15  | 79  | 852     | 362 | 2,846        |
| Background<br>2015                                    | 43  | 55     | 188 | 296 | 108    | 49    | 15 | 944      | 17  | 87  | 941     | 400 | 3,143        |
| Background<br>2030                                    | 50  | 64     | 218 | 344 | 126    | 56    | 18 | 1,096    | 19  | 101 | 1,093   | 464 | 3,649        |
| Use National<br>St. Ext.                              | -   | -      | 99  | -   | 14     | -14   | -  | -99      | -   | 187 | -187    | -   | 0            |
| Future 2015<br>w/ National<br>St. Ext.                | 43  | 55     | 287 | 296 | 122    | 35    | 15 | 845      | 17  | 274 | 754     | 400 | 3,143        |
| National St.<br>Ext.<br>Development                   | 146 | 15     | 146 | -   | 12     | -     | -  | -        | 70  | 70  | -       | -   | 459          |
| Future 2015<br>w/ National<br>St. Ext.<br>Development | 189 | 70     | 433 | 296 | 134    | 35    | 15 | 845      | 87  | 344 | 754     | 400 | 3,602        |
| Future 2030<br>w/ National<br>St. Ext.<br>Development | 220 | 82     | 502 | 344 | 156    | 40    | 18 | 982      | 101 | 400 | 876     | 464 | 4,185        |

Table C10: Traffic at Grand River/National Street

Appendix D

Level of Service Capacity Analysis with National Street

|                               | ٨                         |       | $\mathbf{k}$ | <b>\$</b> | -          | Ł          | 4                           | å<br>I | p     | \$   | Ļ     | 1    |
|-------------------------------|---------------------------|-------|--------------|-----------|------------|------------|-----------------------------|--------|-------|------|-------|------|
| Movement                      | EBL                       | EBT   | EBR          | WBL       | WBT        | WBR        | NBL                         | NBT    | NBR   | SBL  | SBT   | SBR  |
| Lane Configurations           | ሻ                         | ¢î _  |              | Ϋ́ς       | 个          | 7          |                             | ፋኈ     |       |      | र्स   | ĩ    |
| Volume (vph)                  | 247                       | 159   | 100          | 157       | 44         | 85         | 105                         | 402    | 294   | 366  | 738   | 109  |
| Ideal Flow (vphpl)            | 2000                      | 2000  | 2000         | 2000      | 2000       | 2000       | 2000                        | 2000   | 2000  | 2000 | 2000  | 2000 |
| Total Lost time (s)           | 6.0                       | 6.0   |              | 6.0       | 6.0        | 6.0        |                             | 6.6    |       |      | 6.6   | 6.6  |
| Lane Util. Factor             | 1.00                      | 1.00  |              | 1.00      | 1.00       | 1.00       |                             | 0.95   |       |      | 1.00  | 1.00 |
| Frt                           | 1.00                      | 0.94  |              | 1.00      | 1.00       | 0.85       |                             | 0.94   |       |      | 1.00  | 0.85 |
| Fit Protected                 | 0.95                      | 1.00  |              | 0.95      | 1.00       | 1.00       |                             | 0.99   |       |      | 0.98  | 1.00 |
| Satd. Flow (prot)             | 1863                      | 1847  |              | 1863      | 1961       | 1667       |                             | 3497   |       |      | 1929  | 1667 |
| Flt Permitted                 | 0.95                      | 1.00  |              | 0.95      | 1.00       | 1.00       |                             | 0.51   |       |      | 0.45  | 1.00 |
| Satd. Flow (perm)             | 1863                      | 1847  |              | 1863      | 1961       | 1667       |                             | 1784   |       |      | 887   | 1667 |
| Peak-hour factor, PHF         | 0.92                      | 0.92  | 0.92         | 0.92      | 0.92       | 0.92       | 0.92                        | 0.92   | 0.92  | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)               | 268                       | 173   | 109          | 171       | 48         | 92         | 114                         | 437    | 320   | 398  | 802   | 118  |
| RTOR Reduction (vph)          | 0                         | 26    | 0            | 0         | 0          | 84         | 0                           | 93     | 0     | 0    | 0     | 43   |
| Lane Group Flow (vph)         | 268                       | 256   | 0            | 171       | 48         | 8          | 0                           | 778    | 0     | 0    | 1200  | 75   |
| Turn Type                     | Prot                      |       |              | Prot      |            | Perm       | Perm                        |        |       | Perm |       | Perm |
| Protected Phases              | 7                         | 4     |              | 3         | 8          |            |                             | 2      |       |      | 6     |      |
| Permitted Phases              |                           |       |              |           |            | 8          | 2                           |        |       | 6    |       | 6    |
| Actuated Green, G (s)         | 17.3                      | 15.0  |              | 10.2      | 7.9        | 7.9        |                             | 46.4   |       |      | 46.4  | 46.4 |
| Effective Green, g (s)        | 17.3                      | 15.0  |              | 10.2      | 7.9        | 7.9        |                             | 46.4   |       |      | 46.4  | 46.4 |
| Actuated g/C Ratio            | 0.19                      | 0.17  |              | 0.11      | 0.09       | 0.09       |                             | 0.51   |       |      | 0.51  | 0.51 |
| Clearance Time (s)            | 6.0                       | 6.0   |              | 6.0       | 6.0        | 6.0        |                             | 6.6    |       |      | 6.6   | 6.6  |
| Vehicle Extension (s)         | 3.0                       | 3.0   |              | 3.0       | 3.0        | 3.0        |                             | 3.0    |       |      | 3.0   | 3.0  |
| Lane Grp Cap (vph)            | 357                       | 307   |              | 211       | 172        | 146        |                             | 918    |       |      | 456   | 858  |
| v/s Ratio Prot                | c0.14                     | c0.14 |              | 0.09      | 0.02       |            |                             |        |       |      |       |      |
| v/s Ratio Perm                |                           |       |              |           |            | 0.00       |                             | 0.44   |       |      | c1.35 | 0.04 |
| v/c Ratio                     | 0.75                      | 0.83  |              | 0.81      | 0.28       | 0.06       |                             | 0.85   |       |      | 2.63  | 0.09 |
| Uniform Delay, d1             | 34.4                      | 36.4  |              | 39.1      | 38.5       | 37.7       |                             | 18.9   |       |      | 21.9  | 11.1 |
| Progression Factor            | 1.00                      | 1.00  |              | 1.00      | 1.00       | 1.00       |                             | 1.00   |       |      | 1.00  | 1.00 |
| Incremental Delay, d2         | 8.6                       | 17.4  |              | 20.5      | 0.9        | 0.2        | t                           | 9.6    |       |      | 740.5 | 0.2  |
| Delay (s)                     | 43.0                      | 53.8  |              | 59.5      | 39.4       | 37.9       |                             | 28.4   |       |      | 762.4 | 11.3 |
| Level of Service              | D                         | D     |              | E         | D          | D          |                             | С      |       |      | F     | В    |
| Approach Delay (s)            |                           | 48.6  |              |           | 50.0       |            |                             | 28.4   |       |      | 695.2 |      |
| Approach LOS                  |                           | D     |              |           | D          |            |                             | С      |       |      | F     |      |
| Intersection Summary          |                           |       |              |           |            |            |                             |        |       |      |       |      |
| HCM Average Control Dela      |                           |       | 322.4        | H         | CM Level   | of Service | <b>)</b><br>2402-00 0 00000 |        | F     |      |       |      |
| HCM Volume to Capacity ra     | atio                      |       | 2.02         |           |            |            |                             |        |       |      |       |      |
| Actuated Cycle Length (s)     | ella constante e constant |       | 90.2         |           | um of lost |            |                             |        | 18.6  |      |       |      |
| Intersection Capacity Utiliza | ation                     |       | 121.5%       | IC        | U Level o  | of Service |                             |        | N H S |      |       |      |
| Analysis Period (min)         |                           |       | 15           |           |            |            |                             |        |       |      |       |      |
| c Critical Lane Group         |                           |       |              |           |            |            |                             |        |       |      |       |      |

|                                  | A                 | <b></b> > | 7                  | ∢     | <b></b>    | Ł          | 1                       | Ť    | M    | \$                         | Ļ    | ~     |
|----------------------------------|-------------------|-----------|--------------------|-------|------------|------------|-------------------------|------|------|----------------------------|------|-------|
| Movement                         | EBL               | EBT       | EBR                | WBL   | WBT        | WBR        | NBL                     | NBT  | NBR  | SBL                        | SBT  | SBR   |
| Lane Configurations              | ሻ                 | ef 🕺      |                    | ٣     | ĥ          |            | ۲Ĩ                      | ₽    |      | ሻ                          | ተ    | ሻ     |
| Volume (vph)                     | 158               | 169       | 267                | 194   | 75         | 71         | 168                     | 413  | 59   | 2                          | 657  | 32    |
| Ideal Flow (vphpl)               | 2000              | 2000      | 2000               | 2000  | 2000       | 2000       | 2000                    | 2000 | 2000 | 2000                       | 2000 | 2000  |
| Total Lost time (s)              | 6.1               | 6.1       |                    | 6.1   | 6.1        |            | 5.9                     | 5.9  |      | 5.9                        | 5.9  | 6.1   |
| Lane Util. Factor                | 1.00              | 1.00      |                    | 1.00  | 1.00       |            | 1.00                    | 1.00 |      | 1.00                       | 1.00 | 1.00  |
| Frt                              | 1.00              | 0.91      |                    | 1.00  | 0.93       |            | 1.00                    | 0.98 |      | 1.00                       | 1.00 | 0.85  |
| Flt Protected                    | 0.95              | 1.00      |                    | 0.95  | 1.00       |            | 0.95                    | 1.00 |      | 0.95                       | 1.00 | 1.00  |
| Satd. Flow (prot)                | 1881              | 1762      |                    | 1863  | 1826       |            | 1743                    | 1907 |      | 1900                       | 1980 | 1650  |
| Flt Permitted                    | 0.51              | 1.00      |                    | 0.22  | 1.00       |            | 0.11                    | 1.00 |      | 0.35                       | 1.00 | 1.00  |
| Satd. Flow (perm)                | 1008              | 1762      |                    | 433   | 1826       |            | 193                     | 1907 |      | 694                        | 1980 | 1650  |
| Peak-hour factor, PHF            | 0.81              | 0.81      | 0.81               | 0.73  | 0.73       | 0.73       | 0.74                    | 0.74 | 0.74 | 0.84                       | 0.84 | 0.84  |
| Adj. Flow (vph)                  | 195               | 209       | 330                | 266   | 103        | 97         | 227                     | 558  | 80   | 2                          | 782  | 38    |
| RTOR Reduction (vph)             | 0                 | 63        | 0                  | 0     | 38         | 0          | 0                       | 5    | 0    | 0                          | 0    | 8     |
| Lane Group Flow (vph)            | 195               | 476       | 0                  | 266   | 162        | 0          | 227                     | 633  | 0    | 2                          | 782  | 30    |
| Heavy Vehicles (%)               | 1%                | 0%        | 5%                 | 2%    | 3%         | 0%         | 9%                      | 2%   | 9%   | 0%                         | 1%   | 3%    |
| Turn Type                        | pm+pt             |           |                    | pm+pt |            |            | pm+pt                   |      |      | Perm                       |      | pm+ov |
| Protected Phases                 | 7                 | 4         | a da ani ara di sa | 3     | 8          |            | 5                       | 2    |      |                            | 6    | 7     |
| Permitted Phases                 | 4                 |           |                    | 8     |            |            | 2                       |      |      | 6                          |      | 6     |
| Actuated Green, G (s)            | 27.6              | 18.9      |                    | 26.0  | 18.1       |            | 45.1                    | 45.1 |      | 32.1                       | 32.1 | 40.8  |
| Effective Green, g (s)           | 27.6              | 18.9      |                    | 26.0  | 18.1       |            | 45.1                    | 45.1 |      | 32.1                       | 32.1 | 40.8  |
| Actuated g/C Ratio               | 0.31              | 0.21      |                    | 0.29  | 0.20       |            | 0.50                    | 0.50 |      | 0.36                       | 0.36 | 0.45  |
| Clearance Time (s)               | 6.1               | 6.1       |                    | 6.1   | 6.1        |            | 5.9                     | 5.9  |      | 5.9                        | 5.9  | 6.1   |
| Vehicle Extension (s)            | 3.0               | 3.0       |                    | 3.0   | 3.0        |            | 3.0                     | 3.0  |      | 3.0                        | 3.0  | 3.0   |
| Lane Grp Cap (vph)               | 394               | 370       |                    | 251   | 367        |            | 219                     | 956  |      | 248                        | 706  | 748   |
| v/s Ratio Prot                   | 0.05              | c0.27     |                    | c0.09 | 0.09       |            | c0.08                   | 0.33 |      |                            | 0.39 | 0.00  |
| v/s Ratio Perm                   | 0.10              |           |                    | 0.21  |            |            | c0.44                   |      |      | 0.00                       |      | 0.01  |
| v/c Ratio                        | 0.49              | 1.29      |                    | 1.06  | 0.44       |            | 1.04                    | 0.66 |      | 0.01                       | 1.11 | 0.04  |
| Uniform Delay, d1                | 24.2              | 35.6      |                    | 29.9  | 31.5       |            | 22.7                    | 16.8 |      | 18.7                       | 28.9 | 13.7  |
| Progression Factor               | 1.00              | 1.00      |                    | 1.00  | 1.00       |            | 1.00                    | 1.00 |      | 0.76                       | 0.89 | 0.69  |
| Incremental Delay, d2            | 1.0               | 147.7     |                    | 73.5  | 0.9        |            | 70.7                    | 3.6  |      | 0.1                        | 67.0 | 0.0   |
| Delay (s)                        | 25.2              | 183.3     |                    | 103.4 | 32.4       |            | 93.3                    | 20.4 |      | 14.3                       | 92.8 | 9.5   |
| Level of Service                 | С                 | E.        |                    | F     | С          |            | F                       | С    |      | В                          | F    | Α     |
| Approach Delay (s)               | suddi seldi. Estu | 141.3     |                    |       | 72.9       |            | alg (al al fhire hain a | 39.5 |      | e ageste die terse die hit | 88.8 |       |
| Approach LOS                     |                   | F.        |                    |       | Е          |            |                         | D    |      |                            | F    |       |
| Intersection Summary             |                   |           |                    |       |            |            |                         |      |      |                            |      |       |
| HCM Average Control Delay        |                   |           | 84.8               | H     | CM Level   | of Service | ce                      |      | F    |                            |      |       |
| HCM Volume to Capacity ratio     | )                 |           | 0.98               |       |            |            |                         |      |      |                            |      |       |
| Actuated Cycle Length (s)        |                   |           | 90.0               | S     | um of lost | time (s)   |                         |      | 12.0 |                            |      |       |
| Intersection Capacity Utilizatio | n                 |           | 95.9%              | IC    | U Level o  | of Service | <b>;</b>                |      | F    |                            |      |       |
| Analysis Period (min)            |                   |           | 15                 |       |            |            |                         |      |      |                            |      |       |

|                                   | ٨    |      | ~     | 1     | <b>\$</b>  | Ł          | 4    | 1        | P    | \$   | Ť     | ~    |
|-----------------------------------|------|------|-------|-------|------------|------------|------|----------|------|------|-------|------|
| Movement                          | EBL  | EBT  | EBR   | WBL   | WBT        | WBR        | NBL  | NBT      | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | Ϋ́ς  | ĥ    |       | ሻ     | ኈ          |            | ሻ    | <b>Þ</b> |      | ሻ    | ዯ     | ٦    |
| Volume (vph)                      | 10   | 10   | 80    | 40    | 10         | 10         | 20   | 300      | 60   | 10   | 540   | 10   |
| Ideal Flow (vphpl)                | 2000 | 2000 | 2000  | 2000  | 2000       | 2000       | 2000 | 2000     | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)               | 5.8  | 5.8  |       | 5.8   | 5.8        |            | 5.8  | 5.8      |      | 5.8  | 5.8   | 5.8  |
| Lane Util. Factor                 | 1.00 | 1.00 |       | 1.00  | 1.00       |            | 1.00 | 1.00     |      | 1.00 | 1.00  | 1.00 |
| Frt                               | 1.00 | 0.87 |       | 1.00  | 0.92       |            | 1.00 | 0.98     |      | 1.00 | 1.00  | 0.85 |
| Flt Protected                     | 0.95 | 1.00 |       | 0.95  | 1.00       |            | 0.95 | 1.00     |      | 0.95 | 1.00  | 1.00 |
| Satd. Flow (prot)                 | 1863 | 1700 |       | 1863  | 1814       |            | 1863 | 1912     |      | 1863 | 1961  | 1667 |
| Flt Permitted                     | 0.74 | 1.00 |       | 0.69  | 1.00       |            | 0.42 | 1.00     |      | 0.53 | 1.00  | 1.00 |
| Satd. Flow (perm)                 | 1457 | 1700 |       | 1360  | 1814       |            | 828  | 1912     |      | 1041 | 1961  | 1667 |
| Peak-hour factor, PHF             | 0.92 | 0.92 | 0.92  | 0.92  | 0.92       | 0.92       | 0.92 | 0.92     | 0.92 | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)                   | 11   | 11   | 87    | 43    | 11         | 11         | 22   | 326      | 65   | 11   | 587   | 11   |
| RTOR Reduction (vph)              | 0    | 80   | 0     | 0     | 10         | 0          | 0    | 4        | 0    | 0    | 0     | 2    |
| Lane Group Flow (vph)             | 11   | 18   | 0     | 43    | 12         | 0          | 22   | 387      | 0    | 11   | 587   | 9    |
| Turn Type                         | Perm |      |       | Perm  |            |            | Perm |          |      | Perm |       | Perm |
| Protected Phases                  |      | 4    |       |       | 8          |            |      | 2        |      |      | 6     |      |
| Permitted Phases                  | 4    |      |       | 8     |            |            | 2    |          |      | 6    |       | 6    |
| Actuated Green, G (s)             | 7.3  | 7.3  |       | 7.3   | 7.3        |            | 71.1 | 71.1     |      | 71.1 | 71.1  | 71.1 |
| Effective Green, g (s)            | 7.3  | 7.3  |       | 7.3   | 7.3        |            | 71.1 | 71.1     |      | 71.1 | 71.1  | 71.1 |
| Actuated g/C Ratio                | 0.08 | 0.08 |       | 0.08  | 0.08       |            | 0.79 | 0.79     |      | 0.79 | 0.79  | 0.79 |
| Clearance Time (s)                | 5.8  | 5.8  |       | 5.8   | 5.8        |            | 5.8  | 5.8      |      | 5.8  | 5.8   | 5.8  |
| Vehicle Extension (s)             | 3.0  | 3.0  |       | 3.0   | 3.0        |            | 3.0  | 3.0      |      | 3.0  | 3.0   | 3.0  |
| Lane Grp Cap (vph)                | 118  | 138  |       | 110   | 147        |            | 654  | 1510     |      | 822  | 1549  | 1317 |
| v/s Ratio Prot                    |      | 0.01 |       |       | 0.01       |            |      | 0.20     |      |      | c0.30 |      |
| v/s Ratio Perm                    | 0.01 |      |       | c0.03 |            |            | 0.03 |          |      | 0.01 |       | 0.01 |
| v/c Ratio                         | 0.09 | 0.13 |       | 0.39  | 0.08       |            | 0.03 | 0.26     |      | 0.01 | 0.38  | 0.01 |
| Uniform Delay, d1                 | 38.3 | 38.4 |       | 39.2  | 38.2       |            | 2.0  | 2.5      |      | 2.0  | 2.8   | 2.0  |
| Progression Factor                | 1.00 | 1.00 |       | 1.00  | 1.00       |            | 0.97 | 1.23     |      | 0.55 | 0.49  | 0.36 |
| Incremental Delay, d2             | 0.3  | 0.4  |       | 2.3   | 0.2        |            | 0.1  | 0.3      |      | 0.0  | 0.4   | 0.0  |
| Delay (s)                         | 38,6 | 38.8 |       | 41.5  | 38.5       |            | 2.1  | 3.4      |      | 1.1  | 1.8   | 0.7  |
| Level of Service                  | D    | D    |       | D     | D          |            | А    | А        |      | А    | А     | А    |
| Approach Delay (s)                |      | 38.8 |       |       | 40.5       |            |      | 3.3      |      |      | 1.8   |      |
| Approach LOS                      |      | D    |       |       | D          |            |      | А        |      |      | А     |      |
| Intersection Summary              |      |      |       |       |            |            |      |          |      |      |       |      |
| HCM Average Control Delay         |      |      | 7.8   | H     | CM Level   | of Service | е    |          | А    |      |       |      |
| HCM Volume to Capacity ratio      |      |      | 0.38  |       |            |            |      |          |      |      |       |      |
| Actuated Cycle Length (s)         |      |      | 90.0  | Su    | im of lost | time (s)   |      |          | 11.6 |      |       |      |
| Intersection Capacity Utilization | 1    |      | 45.4% |       | U Level o  |            |      |          | Α    |      |       |      |
| Analysis Period (min)             |      |      | 15    |       |            |            |      |          |      |      |       |      |
| c Critical Lane Group             |      |      |       |       |            |            |      |          |      |      |       |      |

|  | <u>^</u> |            | Ì     | 1     | 4          | ×.        | ٩     | Ť    | p    | \$   | Ť     | 4    |
|--|----------|------------|-------|-------|------------|-----------|-------|------|------|------|-------|------|
| Movement                                       | EBL      | EBT        | EBR   | WBL   | WBT        | WBR       | NBL   | NBT  | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations                            | ሻ        | <b>ት</b> ኈ |       | ሻ     | ♠₽         |           | ሻ     | î∌   |      | ሻ    | ₿     |      |
| Volume (vph)                                   | 19       | 591        | 103   | 29    | 501        | 12        | 72    | 191  | 43   | 44   | 418   | 10   |
| Ideal Flow (vphpl)                             | 2000     | 2000       | 2000  | 2000  | 2000       | 2000      | 2000  | 2000 | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)                            | 6.0      | 6.0        |       | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |      |
| Lane Util. Factor                              | 1.00     | 0.95       |       | 1.00  | 0.95       |           | 1.00  | 1.00 |      | 1.00 | 1.00  |      |
| Frt  | 1.00     | 0.98       |       | 1.00  | 1.00       |           | 1.00  | 0.97 |      | 1.00 | 1.00  |      |
| Flt Protected                                  | 0.95     | 1.00       |       | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (prot)                              | 1863     | 3643       |       | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |      |
| Flt Permitted                                  | 0.95     | 1.00       |       | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (perm)                              | 1863     | 3643       |       | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |      |
| Peak-hour factor, PHF                          | 0.79     | 0.79       | 0.79  | 0.70  | 0.70       | 0.70      | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81 |
| Adj. Flow (vph)                                | 24       | 748        | 130   | 41    | 716        | 17        | 76    | 201  | 45   | 54   | 516   | 12   |
| RTOR Reduction (vph)                           | 0        | 14         | 0     | 0     | 1          | 0         | 0     | 9    | 0    | 0    | 1     | 0    |
| Lane Group Flow (vph)                          | 24       | 864        | 0     | 41    | 732        | 0         | 76    | 237  | 0    | 54   | 527   | 0    |
| Turn Type                                      | Prot     |            |       | Prot  |            |           | Prot  |      |      | Prot |       |      |
| Protected Phases                               | 5        | 2          |       | 1     | 6          |           | 3     | 8    |      | 7    | 4     |      |
| Permitted Phases                               |          |            |       |       |            |           |       |      |      |      |       |      |
| Actuated Green, G (s)                          | 2.8      | 29.1       |       | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |      |
| Effective Green, g (s)                         | 2.8      | 29.1       |       | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |      |
| Actuated g/C Ratio                             | 0.03     | 0.32       |       | 0.05  | 0.34       |           | 0.06  | 0.30 |      | 0.06 | 0.30  |      |
| Clearance Time (s)                             | 6.0      | 6.0        |       | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |      |
| Vehicle Extension (s)                          | 3.0      | 3.0        |       | 3.0   | 3.0        |           | 3.0   | 3.0  |      | 3.0  | 3.0   |      |
| Lane Grp Cap (vph)                             | 58       | 1178       |       | 87    | 1258       |           | 116   | 574  |      | 116  | 588   |      |
| v/s Ratio Prot                                 | 0.01     | c0.24      |       | c0.02 | 0.20       |           | c0.04 | 0.12 |      | 0.03 | c0.27 |      |
| v/s Ratio Perm                                 |          |            |       |       |            |           |       |      |      |      |       |      |
| v/c Ratio                                      | 0.41     | 0.73       |       | 0.47  | 0.58       |           | 0.66  | 0.41 |      | 0.47 | 0.90  |      |
| Uniform Delay, d1                              | 42.8     | 27.0       |       | 41.8  | 24.5       |           | 41.3  | 25.1 |      | 40.8 | 30.1  |      |
| Progression Factor                             | 1.00     | 1.00       |       | 1.08  | 1.22       |           | 0.89  | 0.78 |      | 1.00 | 1.00  |      |
| Incremental Delay, d2                          | 4.7      | 4.1        |       | 3.4   | 1.7        |           | 12.4  | 0.5  |      | 2.9  | 16.2  |      |
| Delay (s)                                      | 47.5     | 31.1       |       | 48.5  | 31.6       |           | 49.0  | 20.0 |      | 43.7 | 46.3  |      |
| Level of Service                               | D        | С          |       | D     | С          |           | D     | В    |      | D    | D     |      |
| Approach Delay (s)                             |          | 31.5       |       |       | 32.5       |           |       | 26.8 |      |      | 46.1  |      |
| Approach LOS                                   |          | С          |       |       | C          |           |       | С    |      |      | D     |      |
| Intersection Summary                           |          |            |       |       |            |           |       |      |      |      |       |      |
| HCM Average Control Delay                      |          |            | 34.5  | H     | CM Level   | of Servic | e     |      | С    |      |       |      |
| HCM Volume to Capacity ratio                   |          |            | 0.78  |       |            |           |       |      |      |      |       |      |
| Actuated Cycle Length (s)                      |          |            | 90.0  |       | im of lost |           |       |      | 24.0 |      |       |      |
| Intersection Capacity Utilization              |          |            | 65.2% | IC    | U Level o  | f Service |       |      | С    |      |       |      |
| Analysis Period (min)<br>c Critical Lane Group |          |            | 15    |       |            |           |       |      |      |      |       |      |

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|----------------------------------|--------|---------------|----------------|----------------------------|-----------------------------------|------------|------------|------|---|-------|------------|---|
| Movement                         | EBL    | EBT           | EBR            | WBL                        | WBT                               | WBR        | NBL        | NBT  | NBR   | SBL   | SBT        | SBR   |
| Lane Configurations              | ሻ      | <u></u><br>ተኑ |                | ሻ                          | 个                                 | ሻ          | ħ          | ÷    |   | k     | ĥ          | A SPANIC CONTRACTOR   |
| Volume (vph)                     | 4      | 612           | 161            | 203                        | 642                               | 116        | 53         | 21   | 217   | 182   | 41         | 10  |
| Ideal Flow (vphpl)               | 2000   | 2000          | 2000           | 2000                       | 2000                              | 2000       | 2000       | 2000 | 2000  | 2000  | 2000       | 2000  |
| Lane Width                       | 12     | 12            | 12             | 12                         | 12                                | 12         | 11         | 11   | 11  | 12    | 12         | 12  |
| Total Lost time (s)              | 6.1    | 6.1           | t i tonatione. | 6.1                        | 6.1                               | 6.1        | 6.0        | 6.0  | al Alexandre I.   | 6.0   | 6.0        | 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -<br>1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -<br>1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - |
| Lane Util. Factor                | 1.00   | 0.95          |                | 1.00                       | 1.00                              | 1.00       | 1.00       | 1.00 |   | 1.00  | 1.00       |   |
| Frt                              | 1.00   | 0.97          |                | 1.00                       | 1.00                              | 0.85       | 1.00       | 0.86 |   | 1.00  | 0.97       | anan beshi  |
| Flt Protected                    | 0.95   | 1.00          |                | 0.95                       | 1.00                              | 1.00       | 0.95       | 1.00 |   | 0.95  | 1.00       |   |
| Satd. Flow (prot)                | 1863   | 3609          |                | 1863                       | 1961                              | 1500       | 1801       | 1636 |   | 1863  | 1905       |   |
| Flt Permitted                    | 0.23   | 1.00          |                | 0.11                       | 1.00                              | 1.00       | 0.71       | 1.00 |   | 0.28  | 1.00       |   |
| Satd. Flow (perm)                | 456    | 3609          |                | 223                        | 1961                              | 1500       | 1351       | 1636 |   | 544   | 1905       |   |
| Peak-hour factor, PHF            | 0.76   | 0.76          | 0.76           | 0.83                       | 0.83                              | 0.83       | 0.83       | 0.83 | 0.83  | 0.75  | 0.75       | 0.75  |
| Adj. Flow (vph)                  | 5      | 805           | 212            | 245                        | 773                               | 140        | 0.03<br>64 | 25   | 261   | 243   | 0.73<br>55 | 0.73<br>13  |
| RTOR Reduction (vph)             | 0<br>0 | 25            | 0              | 240                        | 0                                 | 69         | 0          | 23   | 201   | 243   | 8          | 0   |
| Lane Group Flow (vph)            | 5      | 992           | 0              | 245                        | 773                               | - 05<br>71 | 64         | 286  | 0   | 243   | 60         |   |
| Parking (#/hr)                   | J      | 552           | 0              | 240                        | 115                               | 0          | 04         | 200  | V   | 243   | 00         | 0   |
| Turn Type                        | Perm   |               | U.             | riedeligereiger<br>Am Lowe | 1월197 - 146 - 4 <u>6 1</u> 87<br> |            | Derm       |      | 2019년 1997년<br>1997년 - 1997년 19 |       |            |   |
| Protected Phases                 | Perm   | <b>.</b>      |                | pm+pt                      | <b>^</b>                          | Perm       | Perm       |      |   | pm+pt |            |   |
|                                  |        | 2             |                | 1                          | 6                                 | •          |            | 8    |   | 7     | 4          |   |
| Permitted Phases                 | 2      | 00 A          | ana ana ang    | 6                          | AF F                              | 6          | 8          |      |   | 4     |            |   |
| Actuated Green, G (s)            | 29.0   | 29.0          |                | 45.5                       | 45.5                              | 45.5       | 19.4       | 19.4 |   | 32.4  | 32.4       |   |
| Effective Green, g (s)           | 29.0   | 29.0          |                | 45.5                       | 45.5                              | 45.5       | 19.4       | 19.4 |   | 32.4  | 32.4       |   |
| Actuated g/C Ratio               | 0.32   | 0.32          |                | 0.51                       | 0.51                              | 0.51       | 0.22       | 0.22 |   | 0.36  | 0.36       |   |
| Clearance Time (s)               | 6.1    | 6.1           |                | 6.1                        | 6.1                               | 6.1        | 6.0        | 6.0  |   | 6.0   | 6.0        |   |
| Vehicle Extension (s)            | 3.0    | 3.0           |                | 3.0                        | 3.0                               | 3.0        | 3.0        | 3.0  | 말 같은 것을 같을  | 3.0   | 3.0        |   |
| Lane Grp Cap (vph)               | 147    | 1163          |                | 302                        | 991                               | 758        | 291        | 353  |   | 298   | 686        |   |
| v/s Ratio Prot                   |        | 0.27          |                | 0.09                       | c0.39                             |            |            | 0.17 |   | c0.06 | 0.03       |   |
| v/s Ratio Perm                   | 0.01   |               |                | c0.32                      |                                   | 0.05       | 0.05       |      |   | c0.23 |            |   |
| v/c Ratio                        | 0.03   | 0.85          |                | 0.81                       | 0.78                              | 0.09       | 0.22       | 0.81 |   | 0.82  | 0.09       |   |
| Uniform Delay, d1                | 20.9   | 28.5          |                | 19.6                       | 18.2                              | 11.5       | 29.1       | 33.6 |   | 24.6  | 19.0       |   |
| Progression Factor               | 1.20   | 0.96          |                | 1.00                       | 1.00                              | 1.00       | 1.00       | 1.00 |   | 1,00  | 1.00       |   |
| Incremental Delay, d2            | 0.4    | 7.6           |                | 15.1                       | 6.1                               | 0.2        | 0.4        | 13.1 |   | 15.6  | 0.1        |   |
| Delay (s)                        | 25.5   | 35.1          |                | 34.8                       | 24.2                              | 11.8       | 29.5       | 46.7 |   | 40.2  | 19.1       |   |
| Level of Service                 | С      | D             |                | С                          | С                                 | В          | С          | D    |   | D     | В          |   |
| Approach Delay (s)               |        | 35.1          |                |                            | 25.0                              |            |            | 43.5 |   |       | 35.6       |   |
| Approach LOS                     |        | D             |                |                            | С                                 |            |            | D    |   |       | D          |   |
| Intersection Summary             |        |               |                |                            |                                   |            |            |      |   |       |            |   |
| HCM Average Control Delay        |        |               | 32.0           | H                          | CM Level                          | of Servic  | е          |      | С   |       |            |   |
| HCM Volume to Capacity ratio     |        |               | 0.78           |                            |                                   |            |            |      |   |       |            |   |
| Actuated Cycle Length (s)        |        |               | 90.0           |                            | um of lost                        |            |            |      | 12.1  |       |            |   |
| ntersection Capacity Utilization |        |               | 84.0%          | IC                         | U Level o                         | f Service  |            |      | Е   |       |            |   |
| Analysis Period (min)            |        |               | 15             |                            |                                   |            |            |      |   |       |            |   |
| c Critical Lane Group            |        |               |                |                            |                                   |            |            |      |   |       |            |   |

|                               | ≯     | <b></b> > | ¥      | *     | ◄          | Ł          | ٩    | Ť     | p    | 6    | Å.    | -    |
|-------------------------------|-------|-----------|--------|-------|------------|------------|------|-------|------|------|-------|------|
| Movement                      | EBL   | EBT       | EBR    | WBL   | WBT        | WBR        | NBL  | NBT   | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations           | ሻ     | ¢Î        |        | ሻ     | ዯ          | ŕ          |      | €Î î⇒ |      |      | र्स   | ሻ    |
| Volume (vph)                  | 621   | 151       | 329    | 477   | 146        | 294        | 75   | 404   | 140  | 162  | 600   | 132  |
| ldeal Flow (vphpl)            | 2000  | 2000      | 2000   | 2000  | 2000       | 2000       | 2000 | 2000  | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)           | 6.0   | 6.0       |        | 6.0   | 6.0        | 6.0        |      | 6.6   |      |      | 6.6   | 6.6  |
| Lane Util. Factor             | 1.00  | 1.00      |        | 1.00  | 1.00       | 1.00       |      | 0.95  |      |      | 1.00  | 1.00 |
| Frt                           | 1.00  | 0.90      |        | 1.00  | 1.00       | 0.85       |      | 0.97  |      |      | 1.00  | 0.85 |
| Flt Protected                 | 0.95  | 1.00      |        | 0.95  | 1.00       | 1.00       |      | 0.99  |      |      | 0.99  | 1.00 |
| Satd. Flow (prot)             | 1863  | 1759      |        | 1863  | 1961       | 1667       |      | 3577  |      |      | 1940  | 1667 |
| Flt Permitted                 | 0.95  | 1.00      |        | 0.95  | 1.00       | 1.00       |      | 0.50  |      |      | 0.60  | 1.00 |
| Satd. Flow (perm)             | 1863  | 1759      | 아이를 사  | 1863  | 1961       | 1667       |      | 1816  |      |      | 1176  | 1667 |
| Peak-hour factor, PHF         | 0.92  | 0.92      | 0.92   | 0.92  | 0.92       | 0.92       | 0.92 | 0.92  | 0.92 | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)               | 675   | 164       | 358    | 518   | 159        | 320        | 82   | 439   | 152  | 176  | 652   | 143  |
| RTOR Reduction (vph)          | 0     | 84        | 0      | 0     | 0          | 163        | 0    | 30    | 0    | 0    | 0     | 76   |
| Lane Group Flow (vph)         | 675   | 438       | 0      | 518   | 159        | 157        | 0    | 643   | 0    | 0    | 828   | 67   |
| Turn Type                     | Prot  |           |        | Prot  |            | Perm       | Perm |       |      | Perm |       | Perm |
| Protected Phases              | 7     | 4         |        | 3     | 8          |            |      | 2     |      |      | 6     |      |
| Permitted Phases              |       |           |        |       |            | 8          | 2    |       |      | 6    |       | 6    |
| Actuated Green, G (s)         | 20.6  | 17.0      |        | 17.0  | 13.4       | 13.4       |      | 37.4  |      |      | 37.4  | 37.4 |
| Effective Green, g (s)        | 20.6  | 17.0      |        | 17.0  | 13.4       | 13.4       |      | 37.4  |      |      | 37.4  | 37.4 |
| Actuated g/C Ratio            | 0.23  | 0.19      |        | 0.19  | 0.15       | 0.15       |      | 0.42  |      |      | 0.42  | 0.42 |
| Clearance Time (s)            | 6.0   | 6.0       |        | 6.0   | 6.0        | 6.0        |      | 6.6   |      |      | 6.6   | 6.6  |
| Vehicle Extension (s)         | 3.0   | 3.0       |        | 3.0   | 3.0        | 3.0        |      | 3.0   |      |      | 3.0   | 3.0  |
| Lane Grp Cap (vph)            | 426   | 332       |        | 352   | 292        | 248        |      | 755   |      |      | 489   | 693  |
| v/s Ratio Prot                | c0.36 | c0.25     |        | 0.28  | 0.08       |            |      |       |      |      |       |      |
| v/s Ratio Perm                |       |           |        |       |            | 0.09       |      | 0.35  |      |      | c0.70 | 0.04 |
| v/c Ratio                     | 1.58  | 1.32      |        | 1.47  | 0.54       | 0.63       |      | 0.85  |      |      | 1.69  | 0.10 |
| Uniform Delay, d1             | 34.7  | 36.5      |        | 36.5  | 35.5       | 36.0       |      | 23.8  |      |      | 26.3  | 16.0 |
| Progression Factor            | 1.00  | 1.00      |        | 1.00  | 1.00       | 1.00       |      | 1.00  |      |      | 1.00  | 1.00 |
| Incremental Delay, d2         | 274.0 | 163.9     |        | 227.1 | 2.1        | 5.2        |      | 11.6  |      |      | 320.7 | 0.3  |
| Delay (s)                     | 308.7 | 200.4     |        | 263.6 | 37.5       | 41.1       |      | 35.4  |      |      | 347.0 | 16.3 |
| Level of Service              | F     | F         |        | F     | D          | D          |      | D     |      |      | F     | В    |
| Approach Delay (s)            |       | 261.5     |        |       | 156.2      |            |      | 35.4  |      |      | 298.3 |      |
| Approach LOS                  |       | F         |        |       | F          |            |      | D     |      |      | F     |      |
| Intersection Summary          |       |           |        |       |            |            |      |       |      |      |       |      |
| HCM Average Control Dela      |       |           | 203.8  | НС    | CM Level   | of Service | )    |       | F    |      |       |      |
| HCM Volume to Capacity ra     | atio  |           | 1.66   |       |            |            |      |       |      |      |       |      |
| Actuated Cycle Length (s)     |       |           | 90.0   |       | im of lost |            |      |       | 18.6 |      |       |      |
| Intersection Capacity Utiliza | ition |           | 128.3% | IC    | U Level c  | of Service |      |       | Н    |      |       |      |
| Analysis Period (min)         |       |           | 15     |       |            |            |      |       |      |      |       |      |
| c Critical Lane Group         |       |           |        |       |            |            |      |       |      |      |       |      |

|                                   | ٨                |       | $\mathbf{i}$ | 1   | 4          | ×.  | ٩                                  | Î     | p                   | \$             | Ť    | ~             |
|-----------------------------------|------------------|-------|--------------|---|------------|---|------------------------------------|-------|---------------------|----------------|------|---------------|
| Movement                          | EBL              | EBT   | EBR          | WBL   | WBT        | WBR   | NBL                                | NBT   | NBR                 | SBL            | SBT  | SBR           |
| Lane Configurations               | ሻ                | 4Î    |              | ĥ   | ĥ          |   | ሻ                                  | ĥ     |                     | ሻ              | ተ    | กี            |
| Volume (vph)                      | 110              | 158   | 288          | 169   | 268        | 4   | 323                                | 773   | 77                  | 3              | 434  | 144           |
| Ideal Flow (vphpl)                | 2000             | 2000  | 2000         | 2000  | 2000       | 2000  | 2000                               | 2000  | 2000                | 2000           | 2000 | 2000          |
| Total Lost time (s)               | 6.1              | 6.1   |              | 6.1   | 6.1        |   | 5.9                                | 5.9   |                     | 5.9            | 5.9  | 6.1           |
| Lane Util. Factor                 | 1.00             | 1.00  |              | 1.00  | 1.00       |   | 1.00                               | 1.00  |                     | 1.00           | 1.00 | 1.00          |
| Ert                               | 1.00             | 0.90  |              | 1.00  | 1.00       |   | 1.00                               | 0.99  |                     | 1.00           | 1.00 | 0.85          |
| Flt Protected                     | 0.95             | 1.00  |              | 0.95  | 1.00       |   | 0.95                               | 1.00  |                     | 0.95           | 1.00 | 1.00          |
| Satd. Flow (prot)                 | 1881             | 1750  |              | 1863  | 1938       |   | 1743                               | 1922  |                     | 1900           | 1980 | 1650          |
| Flt Permitted                     | 0.33             | 1.00  |              | 0.17  | 1.00       |   | 0.17                               | 1.00  |                     | 0.19           | 1.00 | 1.00          |
| Satd. Flow (perm)                 | 655              | 1750  |              | 340   | 1938       |   | 321                                | 1922  |                     | 379            | 1980 | 1650          |
| Peak-hour factor, PHF             | 0.83             | 0.83  | 0.83         | 0.80  | 0.80       | 0.80  | 0.90                               | 0.90  | 0.90                | 0.95           | 0.95 | 0.95          |
| Adj. Flow (vph)                   | 133              | 190   | 347          | 211   | 335        | 5   | 359                                | 859   | 86                  | 3              | 457  | 152           |
| RTOR Reduction (vph)              | 0                | 73    | 0            | 0   | 1          | 0   | 0                                  | 4     | 0                   | 0              | 0    | 48            |
| Lane Group Flow (vph)             | 133              | 464   | 0            | 211   | 339        | 0   | 359                                | 941   | 0                   | 3              | 457  | 104           |
| Heavy Vehicles (%)                | 1%               | 0%    | 5%           | 2%  | 3%         | 0%  | 9%                                 | 2%    | 9%                  | 0%             | 1%   | 3%            |
| Turn Type                         | pm+pt            |       |              | pm+pt   |            |   | pm+pt                              |       | 10. sa 19.          | Perm           |      | pm+ov         |
| Protected Phases                  | 7                | 4     |              | 3   | 8          |   | 5                                  | 2     |                     |                | 6    | 7             |
| Permitted Phases                  | 4                |       |              | 8   |            |   | 2                                  |       |                     | 6              |      | 6             |
| Actuated Green, G (s)             | 30.6             | 22.9  |              | 31.0  | 23.1       |   | 41.1                               | 41.1  |                     | 21.1           | 21.1 | 28.8          |
| Effective Green, g (s)            | 30.6             | 22.9  |              | 31.0  | 23.1       |   | 41,1                               | 41.1  |                     | 21.1           | 21.1 | 28.8          |
| Actuated g/C Ratio                | 0.34             | 0.25  |              | 0.34  | 0.26       |   | 0.46                               | 0.46  |                     | 0.23           | 0.23 | 0.32          |
| Clearance Time (s)                | 6.1              | 6.1   |              | 6.1   | 6.1        |   | 5.9                                | 5.9   |                     | 5.9            | 5.9  | 6.1           |
| Vehicle Extension (s)             | 3.0              | 3.0   |              | 3.0   | 3.0        | Life Children A   | 3.0                                | 3.0   | n an th' Alliannai. | 3.0            | 3.0  | 3.0           |
| Lane Grp Cap (vph)                | 328              | 445   |              | 251   | 497        |   | 369                                | 878   |                     | 89             | 464  | 528           |
| v/s Ratio Prot                    | 0.03             | c0.27 |              | c0.07   | 0.18       |   | 0.15                               | c0.49 |                     |                | 0.23 | 0.02          |
| v/s Ratio Perm                    | 0.10             |       |              | 0.22  |            |   | 0.29                               |       |                     | 0.01           |      | 0.05          |
| v/c Ratio                         | 0.41             | 1.04  |              | 0.84  | 0.68       |   | 0.97                               | 1.07  |                     | 0.03           | 0.98 | 0.20          |
| Uniform Delay, d1                 | 21.6             | 33.6  |              | 24.1  | 30.1       |   | 31.9                               | 24.4  |                     | 26.6           | 34.3 | 22.2          |
| Progression Factor                | 1.00             | 1.00  |              | 1.00  | 1.00       |   | 1.00                               | 1.00  |                     | 0.98           | 1.00 | 0.94          |
| Incremental Delay, d2             | 0.8              | 54.2  |              | 21.6  | 3.9        |   | 39.4                               | 51.6  |                     | 0.7            | 37.7 | 0.2           |
| Delay (s)                         | 22.5             | 87.7  |              | 45.7  | 34.0       |   | 71.3                               | 76.0  |                     | 26.8           | 71.8 | 21.0          |
| Level of Service                  | C                | E F   |              | D   | С          |   | E                                  | E     |                     | C              | E    | С             |
| Approach Delay (s)                | andra i Cultania | 74.8  |              | - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 199<br>- 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 | 38.5       |   | al ta Maria an <del>tal</del> a an |       |                     | toralar (BTAB) | 59.0 | en beten dit. |
| Approach LOS                      |                  | Е     |              |   | D          |   |                                    | E     |                     |                | E    |               |
| Intersection Summary              |                  |       |              |   |            |   |                                    |       |                     |                |      |               |
| HCM Average Control Delay         |                  |       | 65.3         | H   | CM Level   | of Servic   | ж                                  |       | Е                   |                |      |               |
| HCM Volume to Capacity ratio      |                  |       | 1.04         |   |            |   |                                    |       |                     |                |      |               |
| Actuated Cycle Length (s)         |                  |       | 90.0         | Sı  | um of lost | time (s)  |                                    |       | 18.1                |                |      |               |
| Intersection Capacity Utilization | 1                |       | 105.0%       |   | U Level o  | a state and the second s | )                                  |       | G                   |                |      |               |
| Analysis Period (min)             |                  |       | 15           |   |            |   |                                    |       |                     |                |      |               |

|                                  | ٨          |            | >     | 1        | 4          | Ł         | ٩     | Î               | 1           | 1    | Ļ                              | 4    |
|----------------------------------|------------|------------|-------|----------|------------|-----------|-------|-----------------|-------------|------|--------------------------------|------|
| Movement                         | EBL        | EBT        | EBR   | WBL      | WBT        | WBR       | NBL   | NBT             | NBR         | SBL  | SBT                            | SBR  |
| Lane Configurations              | ሻ          | <b>ት</b> ኩ |       | ۳Ę<br>۲  | <b>ት</b> ኈ |           | ٣     | <b>^</b>        |             | ۳Ę   | ₽                              |      |
| Volume (vph)                     | 52         | 586        | 91    | 66       | 656        | 104       | 105   | 405             | 37          | 68   | 345                            | 18   |
| Ideal Flow (vphpl)               | 2000       | 2000       | 2000  | 2000     | 2000       | 2000      | 2000  | 2000            | 2000        | 2000 | 2000                           | 2000 |
| Total Lost time (s)              | 6.0        | 6.0        |       | 6.0      | 6.0        |           | 6.0   | 6.0             |             | 6.0  | 6.0                            |      |
| Lane Util. Factor                | 1.00       | 0.95       |       | 1.00     | 0.95       |           | 1.00  | 1.00            |             | 1.00 | 1.00                           |      |
| Frt                              | 1.00       | 0.98       |       | 1.00     | 0.98       |           | 1.00  | 0.99            |             | 1.00 | 0.99                           |      |
| Flt Protected                    | 0.95       | 1.00       |       | 0.95     | 1.00       |           | 0.95  | 1.00            |             | 0.95 | 1.00                           |      |
| Satd. Flow (prot)                | 1863       | 3650       |       | 1863     | 3649       |           | 1863  | 1936            |             | 1863 | 1946                           |      |
| Flt Permitted                    | 0.95       | 1.00       |       | 0.95     | 1.00       |           | 0.95  | 1.00            |             | 0.95 | 1.00                           |      |
| Satd. Flow (perm)                | 1863       | 3650       |       | 1863     | 3649       |           | 1863  | 1936            |             | 1863 | 1946                           |      |
| Peak-hour factor, PHF            | 0.90       | 0.90       | 0.90  | 0.92     | 0.92       | 0.92      | 0.89  | 0.89            | 0.89        | 0.90 | 0.90                           | 0.90 |
| Adj. Flow (vph)                  | 58         | 651        | 101   | 72       | 713        | 113       | 118   | 455             | 42          | 76   | 383                            | 20   |
| RTOR Reduction (vph)             | 0          | 13         | 0     | 0        | 13         | 0         | 0     | 4               | 0           | 0    | 2                              | 0    |
| Lane Group Flow (vph)            | 58         | 739        | 0     | 72       | 813        | 0         | 118   | 493             | 0           | 76   | 401                            | 0    |
| Turn Type                        | Prot       |            |       | Prot     |            |           | Prot  |                 |             | Prot |                                |      |
| Protected Phases                 | 5          | 2          |       | <b>1</b> | 6          |           | 3     | 8               |             | 7    | 4                              |      |
| Permitted Phases                 |            |            |       |          |            |           |       |                 |             |      |                                |      |
| Actuated Green, G (s)            | 5.6        | 27.6       |       | 5.6      | 27.6       |           | 9.9   | 25.2            |             | 7.6  | 22.9                           |      |
| Effective Green, g (s)           | 5.6        | 27.6       |       | 5.6      | 27.6       |           | 9.9   | 25.2            |             | 7.6  | 22.9                           |      |
| Actuated g/C Ratio               | 0.06       | 0.31       |       | 0.06     | 0.31       |           | 0.11  | 0.28            |             | 0.08 | 0.25                           |      |
| Clearance Time (s)               | 6.0        | 6.0        |       | 6.0      | 6.0        |           | 6.0   | 6.0             |             | 6.0  | 6.0                            |      |
| Vehicle Extension (s)            | 3.0        | 3.0        |       | 3.0      | 3.0        |           | 3.0   | 3.0             |             | 3.0  | 3.0                            |      |
| Lane Grp Cap (vph)               | 116        | 1119       |       | 116      | 1119       |           | 205   | 542             |             | 157  | 495                            |      |
| v/s Ratio Prot                   | 0.03       | 0.20       |       | c0.04    | c0.22      |           | c0.06 | c0.25           |             | 0.04 | 0.21                           |      |
| v/s Ratio Perm                   |            |            |       |          |            |           |       |                 |             |      |                                |      |
| v/c Ratio                        | 0.50       | 0.66       |       | 0.62     | 0.73       |           | 0.58  | 0.91            |             | 0.48 | 0.81                           |      |
| Uniform Delay, d1                | 40.8       | 27.1       |       | 41.2     | 27.8       |           | 38.1  | 31.3            |             | 39.3 | 31.5                           |      |
| Progression Factor               | 1.00       | 1.00       |       | 1.09     | 1.19       |           | 1.32  | 0.65            |             | 1.00 | 1.00                           |      |
| Incremental Delay, d2            | 3.4        | 3.1        |       | 6.7      | 2.8        |           | 3.7   | 18.8            |             | 2.3  | 9.5                            |      |
| Delay (s)                        | 44.2       | 30.2       |       | 51.6     | 36.0       |           | 54.1  | 39.0            |             | 41.7 | 41.0                           |      |
| Level of Service                 | D          | С          |       | D        | D          |           | D     | D               |             | D    | D                              |      |
| Approach Delay (s)               |            | 31.2       |       |          | 37.3       |           |       | 41.9            |             |      | 41.1                           |      |
| Approach LOS                     |            | С          |       |          | D          |           |       | D               |             |      | D                              |      |
| Intersection Summary             |            |            |       |          |            |           |       |                 |             |      |                                |      |
| HCM Average Control Delay        |            |            | 37.2  | H        | CM Level   | of Servic | e     |                 | D           |      |                                |      |
| HCM Volume to Capacity ratio     | <u>.</u>   |            | 0.72  |          |            |           |       |                 |             |      |                                |      |
| Actuated Cycle Length (s)        | a herdelen |            | 90.0  | SI       | um of lost | time (s)  |       | , addinaet (201 | 18.0        |      |                                |      |
| Intersection Capacity Utilizatio | nsses      |            | 74.4% |          | U Level c  |           |       |                 | D           |      |                                |      |
| Analysis Period (min)            |            |            | 15    | * * .:   |            |           |       |                 | ar calitada |      | ., 18. 1. 1, 1883 (19. 19. 19. |      |
| c Critical Lane Group            |            |            |       |          |            |           |       |                 |             |      |                                |      |

|                                   | هر   |                  | $\mathbf{i}$ | *          | 4         | ×.          | 4    | Ť              | p                   | \$    | Ļ                            | 4    |
|-----------------------------------|------|------------------|--------------|------------|-----------|-------------|------|----------------|---------------------|-------|------------------------------|------|
| Movement                          | EBL  | EBT              | EBR          | WBL        | WBT       | WBR         | NBL  | NBT            | NBR                 | SBL   | SBT                          | SBF  |
| Lane Configurations               | ۲    | <u></u> ተኑ       |              | <u>ارم</u> | ♠         | 7           | ኻ    | ۴              |                     | ኘ     | \$⇒                          |      |
| Volume (vph)                      | 15   | 845              | 87           | 239        | 754       | 400         | 189  | 70             | 323                 | 296   | 134                          | 35   |
| Ideal Flow (vphpl)                | 2000 | 2000             | 2000         | 2000       | 2000      | 2000        | 2000 | 2000           | 2000                | 2000  | 2000                         | 2000 |
| Lane Width                        | 12   | 12               | 12           | 12         | 12        | 12          | 11   | 11             | 11                  | 12    | 12                           | 12   |
| Total Lost time (s)               | 6.1  | 6.1              |              | 6.1        | 6.1       | 6.0         | 6.0  | 6.0            |                     | 6.0   | 6.0                          |      |
| Lane Util. Factor                 | 1.00 | 0.95             |              | 1.00       | 1.00      | 1.00        | 1.00 | 1.00           |                     | 1.00  | 1.00                         |      |
| Frt                               | 1.00 | 0.99             |              | 1.00       | 1.00      | 0.85        | 1.00 | 0.88           |                     | 1.00  | 0.97                         |      |
| Flt Protected                     | 0.95 | 1.00             |              | 0.95       | 1.00      | 1.00        | 0.95 | 1.00           |                     | 0.95  | 1.00                         |      |
| Satd. Flow (prot)                 | 1863 | 3673             |              | 1863       | 1961      | 1500        | 1801 | 1661           |                     | 1863  | 1900                         |      |
| Flt Permitted                     | 0.17 | 1.00             |              | 0.13       | 1.00      | 1.00        | 0.64 | 1.00           |                     | 0.14  | 1.00                         |      |
| Satd. Flow (perm)                 | 328  | 3673             |              | 261        | 1961      | 1500        | 1216 | 1661           |                     | 280   | 1900                         |      |
| Peak-hour factor, PHF             | 0.88 | 0.88             | 0.88         | 0.92       | 0.92      | 0.92        | 0.94 | 0.94           | 0.94                | 0.92  | 0.92                         | 0.92 |
| Adj. Flow (vph)                   | 17   | 960              | 99           | 260        | 820       | 435         | 201  | 74             | 344                 | 322   | 146                          | 38   |
| RTOR Reduction (vph)              | 0    | 9                | 0            | 0          | 0         | 194         | 0    | 0              | 0                   | 0     | 10                           | C    |
| Lane Group Flow (vph)             | 17   | 1050             | 0            | 260        | 820       | 241         | 201  | 418            | 0                   | 322   | 174                          | С    |
| Parking (#/hr)                    |      |                  | 0            |            |           | 0           |      |                |                     |       |                              |      |
| Turn Type                         | Perm |                  |              | pm+pt      |           | pm+ov       | Perm |                |                     | pm+pt |                              |      |
| Protected Phases                  |      | 2                |              | 1          | 6         | 7           |      | 8              |                     | 7     | 4                            |      |
| Permitted Phases                  | 2    | 1.1.4.1.1.111.TT |              | 6          |           | 6           | 8    |                |                     | 4     |                              |      |
| Actuated Green, G (s)             | 23.9 | 23.9             |              | 38.9       | 38.9      | 49.9        | 22.0 | 22.0           |                     | 39.0  | 39.0                         |      |
| Effective Green, g (s)            | 23.9 | 23.9             |              | 38.9       | 38.9      | 49.9        | 22.0 | 22.0           |                     | 39.0  | 39.0                         |      |
| Actuated g/C Ratio                | 0.27 | 0.27             |              | 0.43       | 0.43      | 0.55        | 0.24 | 0.24           |                     | 0.43  | 0.43                         |      |
| Clearance Time (s)                | 6.1  | 6.1              |              | 6.1        | 6.1       | 6.0         | 6.0  | 6.0            | t contra la la data | 6.0   | 6.0                          |      |
| Vehicle Extension (s)             | 3.0  | 3.0              |              | 3.0        | 3.0       | 3.0         | 3.0  | 3.0            |                     | 3.0   | 3.0                          |      |
| Lane Grp Cap (vph)                | 87   | 975              |              | 271        | 848       | 832         | 297  | 406            |                     | 315   | 823                          |      |
| v/s Ratio Prot                    |      | c0.29            |              | 0.09       | c0.42     | 0.04        |      | 0.25           |                     | c0.13 | 0.09                         |      |
| v/s Ratio Perm                    | 0.05 |                  |              | 0.32       | 00764.974 | 0.13        | 0.17 | 140° TITI 1400 |                     | c0.32 | 2 - 0 <b>- 1 - 7</b> - 7 - 7 |      |
| v/c Ratio                         | 0.20 | 1.08             |              | 0.96       | 0.97      | 0.29        | 0.68 | 1.03           |                     | 1.02  | 0.21                         |      |
| Uniform Delay, d1                 | 25.6 | 33.0             |              | 21.2       | 24.9      | 10.6        | 30.8 | 34.0           |                     | 22.8  | 15.9                         |      |
| Progression Factor                | 1.13 | 0.99             |              | 1.00       | 1.00      | 1.00        | 1.00 | 1.00           |                     | 1.00  | 1.00                         |      |
| Incremental Delay, d2             | 4.8  | 51.4             |              | 43.0       | 23.9      | 0.2         | 6.0  | 52.5           |                     | 56.5  | 0.1                          |      |
| Delay (s)                         | 33.7 | 84.2             |              | 64.2       | 48.8      | 10.8        | 36.8 | 86.5           |                     | 79.4  | 16.0                         |      |
| Level of Service                  | С    | F                |              | E          | D         | В           | D    | F              |                     | E E   | В                            |      |
| Approach Delay (s)                |      | 83.4             |              |            | 40.5      | 888 - E.    |      | 70.3           |                     |       | 56.3                         |      |
| Approach LOS                      |      | F                |              |            | D         |             |      | E              |                     |       | E                            |      |
| Intersection Summary              |      |                  |              |            |           |             |      |                | August 1            |       |                              |      |
| HCM Average Control Delay         |      |                  | 60.1         | Н          | CM Leve   | l of Servic | e    |                | Е                   |       |                              |      |
| HCM Volume to Capacity ratio      |      |                  | 1.04         |            |           |             |      |                |                     |       |                              |      |
| Actuated Cycle Length (s)         |      |                  | 90.0         | S          | um of los | t time (s)  |      |                | 18.2                |       |                              |      |
| Intersection Capacity Utilization | n    |                  | 104.2%       | i i c      | CU Level  | of Service  |      |                | G                   |       |                              |      |
| Analysis Period (min)             |      |                  | 15           |            |           |             |      |                |                     |       |                              |      |
| c Critical Lane Group             |      |                  |              |            |           |             |      |                |                     |       |                              |      |

|                                   | ۶     |      | *     | *    |           | ×.         | ٩    | Î          | M                 | 6    | ļ        | 4    |
|-----------------------------------|-------|------|-------|------|-----------|------------|------|------------|-------------------|------|----------|------|
| Movement                          | EBL   | EBT  | EBR   | WBL  | WBT       | WBR        | NBL  | NBT        | NBR               | SBL  | SBT      | SBR  |
| Lane Configurations               | ሻሻ    | Ŷ    | ř     | ኻኻ   | 个         | ۲          | ۲    | <u></u> የጉ |                   | ሻ    | <u> </u> | Ĩ    |
| Volume (vph)                      | 247   | 29   | 1,00  | 47   | 10        | 0          | 105  | 402        | 57                | 0    | 738      | 109  |
| Ideal Flow (vphpl)                | 2000  | 2000 | 2000  | 2000 | 2000      | 2000       | 2000 | 2000       | 2000              | 2000 | 2000     | 2000 |
| Total Lost time (s)               | 6.0   | 6.0  | 6.0   | 6.0  | 6.0       |            | 6.6  | 6.6        |                   |      | 6.6      | 6.6  |
| Lane Util. Factor                 | 0.97  | 1.00 | 1.00  | 0.97 | 1.00      |            | 1.00 | 0.95       |                   |      | 0.95     | 1.00 |
| Frt                               | 1.00  | 1.00 | 0.85  | 1.00 | 1.00      |            | 1.00 | 0.98       |                   |      | 1.00     | 0.85 |
| Flt Protected                     | 0.95  | 1.00 | 1.00  | 0.95 | 1.00      |            | 0.95 | 1.00       |                   |      | 1.00     | 1.00 |
| Satd. Flow (prot)                 | 3614  | 1961 | 1667  | 3614 | 1961      |            | 1863 | 3656       |                   |      | 3725     | 1667 |
| Flt Permitted                     | 0.95  | 1.00 | 1.00  | 0.95 | 1.00      |            | 0.31 | 1.00       |                   |      | 1.00     | 1.00 |
| Satd. Flow (perm)                 | 3614  | 1961 | 1667  | 3614 | 1961      |            | 617  | 3656       |                   |      | 3725     | 1667 |
| Peak-hour factor, PHF             | 0.92  | 0.92 | 0.92  | 0.92 | 0.92      | 0.92       | 0.92 | 0.92       | 0.92              | 0.92 | 0.92     | 0.92 |
| Adj. Flow (vph)                   | 268   | 32   | 109   | 51   | 11        | 0          | 114  | 437        | 62                | 0    | 802      | 118  |
| RTOR Reduction (vph)              | 0     | 0    | 92    | 0    | 0         | 0          | 0    | 11         | 0                 | 0    | 0        | 48   |
| Lane Group Flow (vph)             | 268   | 32   | 17    | 51   | 11        | 0          | 114  | 488        | 0                 | 0    | 802      | 70   |
| Turn Type                         | Prot  |      | Perm  | Prot |           | Perm       | Perm |            |                   | Perm |          | Perm |
| Protected Phases                  | 7     | 4    |       | 3    | 8         |            |      | 2          |                   |      | 6        |      |
| Permitted Phases                  |       |      | 4     |      |           | 8          | 2    |            |                   | 6    |          | 6    |
| Actuated Green, G (s)             | 15.0  | 12.7 | 12.7  | 4.1  | 1.8       |            | 43.8 | 43.8       |                   |      | 43.8     | 43.8 |
| Effective Green, g (s)            | 15.0  | 12.7 | 12.7  | 4.1  | 1.8       |            | 43.8 | 43.8       |                   |      | 43.8     | 43.8 |
| Actuated g/C Ratio                | 0.19  | 0.16 | 0.16  | 0.05 | 0.02      |            | 0.55 | 0.55       |                   |      | 0.55     | 0.55 |
| Clearance Time (s)                | 6.0   | 6.0  | 6.0   | 6.0  | 6.0       |            | 6.6  | 6.6        |                   |      | 6.6      | 6.6  |
| Vehicle Extension (s)             | 3.0   | 3.0  | 3.0   | 3.0  | 3.0       |            | 3.0  | 3.0        | : 2012 - 2012<br> |      | 3.0      | 3.0  |
| Lane Grp Cap (vph)                | 684   | 314  | 267   | 187  | 45        |            | 341  | 2022       |                   |      | 2060     | 922  |
| v/s Ratio Prot                    | c0.07 | 0.02 |       | 0.01 | c0.01     |            |      | 0.13       |                   |      | c0.22    |      |
| v/s Ratio Perm                    |       |      | 0.01  |      |           |            | 0.18 |            |                   |      |          | 0.04 |
| v/c Ratio                         | 0.39  | 0.10 | 0.07  | 0.27 | 0.24      |            | 0.33 | 0.24       |                   |      | 0.39     | 0.08 |
| Uniform Delay, d1                 | 28.1  | 28.4 | 28.2  | 36.1 | 38.0      |            | 9.7  | 9.1        |                   |      | 10.1     | 8.3  |
| Progression Factor                | 1.00  | 1.00 | 1.00  | 1.00 | 1.00      |            | 1.00 | 1.00       |                   |      | 1.00     | 1.00 |
| Incremental Delay, d2             | 0.4   | 0.1  | 0.1   | 0.8  | 2.8       |            | 2.6  | 0.3        |                   |      | 0.6      | 0.2  |
| Delay (s)                         | 28.5  | 28.5 | 28.3  | 36.9 | 40.9      |            | 12.3 | 9.4        |                   |      | 10.6     | 8.4  |
| Level of Service                  | С     | С    | С     | D    | D         |            | В    | А          |                   |      | В        | A    |
| Approach Delay (s)                |       | 28.4 |       |      | 37.6      |            |      | 10.0       |                   |      | 10.4     |      |
| Approach LOS                      |       | С    |       |      | D         |            |      | А          |                   |      | В        |      |
| Intersection Summary              |       |      |       |      |           |            |      |            |                   |      |          |      |
| HCM Average Control Dela          | у     |      | 14.8  | Н    | CM Level  | of Servic  | e    |            | В                 |      |          |      |
| HCM Volume to Capacity ra         | atio  |      | 0.39  |      |           |            |      |            |                   |      |          |      |
| Actuated Cycle Length (s)         |       |      | 79.2  |      | um of los |            |      |            | 18.6              |      |          |      |
| Intersection Capacity Utilization | ation |      | 57.1% | IC   | U Level o | of Service |      |            | В                 |      |          |      |
| Analysis Period (min)             |       |      | 15    |      |           |            |      |            |                   |      |          |      |
| c Critical Lane Group             |       |      |       |      |           |            |      |            |                   |      |          |      |

|                                  | ٨                     |       | >                         | 1              |            | Ł                 |       | Å       | P           | 1                                 | Ļ       | 4    |
|----------------------------------|-----------------------|-------|---------------------------|----------------|------------|-------------------|-------|---------|-------------|-----------------------------------|---------|------|
| Movement                         | EBL                   | EBT   | EBR                       | WBL.           | WBT        | WBR               | NBL   | NBT     | NBR         | SBL                               | SBT     | SBR  |
| Lane Configurations              | ٦                     | 个     | 7                         | ሻ              | †≽         |                   | ሻ     | 4       |             | ሻ                                 | <b></b> | ۲    |
| Volume (vph)                     | 158                   | 169   | 184                       | 134            | 75         | 11                | 158   | 348     | 53          | 3                                 | 437     | 32   |
| Ideal Flow (vphpl)               | 2000                  | 2000  | 2000                      | 2000           | 2000       | 2000              | 2000  | 2000    | 2000        | 2000                              | 2000    | 2000 |
| Total Lost time (s)              | 4.0                   | 6.1   | 6.1                       | 4.0            | 6.1        |                   | 4.0   | 5.9     |             | 5.9                               | 5.9     | 5.9  |
| Lane Util. Factor                | 1.00                  | 1.00  | 1.00                      | 1.00           | 1.00       |                   | 1.00  | 1.00    |             | 1.00                              | 1.00    | 1.00 |
| Frt                              | 1.00                  | 1.00  | 0.85                      | 1.00           | 0.98       |                   | 1.00  | 0.98    |             | 1.00                              | 1.00    | 0.85 |
| Flt Protected                    | 0.95                  | 1.00  | 1.00                      | 0.95           | 1.00       |                   | 0.95  | 1.00    |             | 0.95                              | 1.00    | 1.00 |
| Satd. Flow (prot)                | 1881                  | 2000  | 1619                      | 1863           | 1912       |                   | 1743  | 1904    |             | 1900                              | 1980    | 1650 |
| Flt Permitted                    | 0.68                  | 1.00  | 1.00                      | 0.45           | 1.00       |                   | 0.30  | 1.00    |             | 0.33                              | 1.00    | 1.00 |
| Satd. Flow (perm)                | 1349                  | 2000  | 1619                      | 877            | 1912       |                   | 554   | 1904    |             | 668                               | 1980    | 1650 |
| Peak-hour factor, PHF            | 0.81                  | 0.81  | 0.81                      | 0.73           | 0.73       | 0.73              | 0.74  | 0.74    | 0.74        | 0.84                              | 0.84    | 0.84 |
| Adj. Flow (vph)                  | 195                   | 209   | 227                       | 184            | 103        | 15                | 214   | 470     | 72          | 4                                 | 520     | 38   |
| RTOR Reduction (vph)             | 0                     | 0     | 134                       | 0              | 6          | 0                 | 0     | 6       | 0           | 0                                 | 0       | 20   |
| Lane Group Flow (vph)            | 195                   | 209   | 93                        | 184            | 112        | Ő                 | 214   | 536     | Ō           | 4                                 | 520     | 18   |
| Heavy Vehicles (%)               | 1%                    | 0%    | 5%                        | 2%             | 3%         | 0%                | 9%    | 2%      | 9%          | 0%                                | 1%      | 3%   |
| Turn Type                        | pm+pt                 |       | Perm                      | pm+pt          |            |                   | pm+pt |         |             | Perm                              |         | Perm |
| Protected Phases                 | 7                     | 4     | linder Skalling Stationer | 3              | 8          |                   | 5     | 2       |             |                                   | 6       |      |
| Permitted Phases                 | 4                     |       | 4                         | 8              |            |                   | 2     | 388.878 |             | 6                                 |         | 6    |
| Actuated Green, G (s)            | 21.7                  | 13.7  | 13.7                      | 21.7           | 13.7       | e ted billiogili. | 54.2  | 52.3    |             | 37.3                              | 37.3    | 37.3 |
| Effective Green, g (s)           | 21.7                  | 13.7  | 13.7                      | 21.7           | 13.7       |                   | 54.2  | 52.3    |             | 37.3                              | 37.3    | 37.3 |
| Actuated g/C Ratio               | 0.24                  | 0.15  | 0.15                      | 0.24           | 0.15       |                   | 0.60  | 0.58    |             | 0.41                              | 0.41    | 0.41 |
| Clearance Time (s)               | 4.0                   | 6.1   | 6.1                       | 4.0            | 6.1        |                   | 4.0   | 5.9     |             | 5.9                               | 5.9     | 5.9  |
| Vehicle Extension (s)            | 3.0                   | 3.0   | 3.0                       | 3.0            | 3.0        |                   | 3.0   | 3.0     |             | 3.0                               | 3.0     | 3.0  |
| Lane Grp Cap (vph)               | 373                   | 304   | 246                       | 299            | 291        | a Mariak          | 479   | 1106    |             | 277                               | 821     | 684  |
| v/s Ratio Prot                   | 0.05                  | c0.10 |                           | c0.05          | 0.06       |                   | 0.05  | c0.28   |             | , herei h <del>er</del> af de ski | c0.26   |      |
| v/s Ratio Perm                   | 0.08                  |       | 0.06                      | 0.09           |            |                   | 0.21  | 00.20   |             | 0.01                              |         | 0.01 |
| v/c Ratio                        | 0.52                  | 0.69  | 0.38                      | 0.62           | 0.39       |                   | 0.45  | 0.48    | an shekarar | 0.01                              | 0.63    | 0.03 |
| Uniform Delay, d1                | 28.9                  | 36.1  | 34.3                      | 28.9           | 34.4       |                   | 19.4  | 11.0    |             | 15.5                              | 20.9    | 15.6 |
| Progression Factor               | 1.00                  | 1.00  | 1.00                      | 1.00           | 1.00       |                   | 1.00  | 1.00    |             | 1.35                              | 1.26    | 1.85 |
| Incremental Delay, d2            | 1.3                   | 6.3   | 1.0                       | 3.7            | 0.8        |                   | 0.7   | 1.5     |             | 0.1                               | 3.6     | 0.1  |
| Delay (s)                        | 30.2                  | 42.5  | 35.3                      | 32.6           | 35.2       |                   | 20.1  | 12.5    |             | 21.0                              | 30.0    | 28.9 |
| Level of Service                 | C                     | D     | D                         | C              | D          |                   | C     | е       |             | Ċ                                 | C       | °.   |
| Approach Delay (s)               | en 1910 i Litera<br>I | 36.1  | ni Unite Etc.             | en en son Film | 33.6       |                   | 1     | 14.7    |             | oner ann aite an                  | 29.9    |      |
| Approach LOS                     |                       | D     |                           |                | C          |                   |       | В       |             |                                   | C       |      |
| Intersection Summary             |                       |       |                           |                |            |                   |       |         |             |                                   |         |      |
| HCM Average Control Delay        |                       |       | 27.0                      | H              | CM Level   | of Servic         | )e    |         | С           |                                   |         |      |
| HCM Volume to Capacity ratio     |                       |       | 0.59                      |                |            |                   |       |         |             |                                   |         |      |
| Actuated Cycle Length (s)        |                       |       | 90.0                      |                | um of lost |                   |       |         | 16.0        |                                   |         |      |
| Intersection Capacity Utilizatio | n                     |       | 62.5%                     | IC             | U Level o  | f Service         | )     |         | В           |                                   |         |      |
| Analysis Period (min)            |                       |       | 15                        |                |            |                   |       |         |             |                                   |         |      |

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|-----------------------------------|------|------|--------------|-------|------------|-----------|------|----------|------|------|-------|------|
| Movement                          | EBL  | EBT  | EBR          | WBL   | WBT        | WBR       | NBL  | NBT      | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | ሻ    | ¢Î   |              | ሻ     | <b>ħ</b>   |           | ំត្  | <b>1</b> |      | ٣    | ት     | أمً  |
| Volume (vph)                      | 10   | 10   | 80           | 40    | 10         | 10        | 20   | 300      | 60   | 10   | 540   | 10   |
| Ideal Flow (vphpl)                | 2000 | 2000 | 2000         | 2000  | 2000       | 2000      | 2000 | 2000     | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)               | 5.8  | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8      |      | 5.8  | 5.8   | 5.8  |
| Lane Util. Factor                 | 1.00 | 1.00 |              | 1.00  | 1.00       |           | 1.00 | 1.00     |      | 1.00 | 1.00  | 1.00 |
| Frt                               | 1.00 | 0.87 |              | 1.00  | 0.92       |           | 1.00 | 0.98     |      | 1.00 | 1.00  | 0.85 |
| Flt Protected                     | 0.95 | 1.00 |              | 0.95  | 1.00       |           | 0.95 | 1.00     |      | 0.95 | 1.00  | 1.00 |
| Satd. Flow (prot)                 | 1863 | 1700 |              | 1863  | 1814       |           | 1863 | 1912     |      | 1863 | 1961  | 1667 |
| Flt Permitted                     | 0.74 | 1.00 |              | 0.69  | 1.00       |           | 0.42 | 1.00     |      | 0.53 | 1.00  | 1.00 |
| Satd. Flow (perm)                 | 1457 | 1700 |              | 1360  | 1814       |           | 828  | 1912     |      | 1041 | 1961  | 1667 |
| Peak-hour factor, PHF             | 0.92 | 0.92 | 0.92         | 0.92  | 0.92       | 0.92      | 0.92 | 0.92     | 0.92 | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)                   | 11   | 11   | 87           | 43    | 11         | 11        | 22   | 326      | 65   | 11   | 587   | 11   |
| RTOR Reduction (vph)              | 0    | 80   | 0            | 0     | 10         | 0         | 0    | 4        | 0    | 0    | 0     | 2    |
| Lane Group Flow (vph)             | 11   | 18   | 0            | 43    | 12         | 0         | 22   | 387      | 0    | 11   | 587   | 9    |
| Turn Type                         | Perm |      |              | Perm  |            |           | Perm |          |      | Perm |       | Perm |
| Protected Phases                  |      | 4    |              |       | 8          |           |      | 2        |      |      | 6     |      |
| Permitted Phases                  | 4    |      |              | 8     |            |           | 2    |          |      | 6    |       | 6    |
| Actuated Green, G (s)             | 7.3  | 7.3  |              | 7.3   | 7.3        |           | 71.1 | 71.1     |      | 71.1 | 71.1  | 71.1 |
| Effective Green, g (s)            | 7.3  | 7.3  |              | 7.3   | 7.3        |           | 71.1 | 71.1     |      | 71.1 | 71.1  | 71.1 |
| Actuated g/C Ratio                | 0.08 | 0.08 |              | 0.08  | 0.08       |           | 0.79 | 0.79     |      | 0.79 | 0.79  | 0.79 |
| Clearance Time (s)                | 5.8  | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8      |      | 5.8  | 5.8   | 5.8  |
| Vehicle Extension (s)             | 3.0  | 3.0  |              | 3.0   | 3.0        |           | 3.0  | 3.0      |      | 3.0  | 3.0   | 3.0  |
| Lane Grp Cap (vph)                | 118  | 138  |              | 110   | 147        |           | 654  | 1510     |      | 822  | 1549  | 1317 |
| v/s Ratio Prot                    |      | 0.01 |              |       | 0.01       |           |      | 0.20     |      |      | c0.30 |      |
| v/s Ratio Perm                    | 0.01 |      |              | c0.03 |            |           | 0.03 |          |      | 0.01 |       | 0.01 |
| v/c Ratio                         | 0.09 | 0.13 |              | 0.39  | 0.08       |           | 0.03 | 0.26     |      | 0.01 | 0.38  | 0.01 |
| Uniform Delay, d1                 | 38.3 | 38.4 |              | 39.2  | 38.2       |           | 2.0  | 2.5      |      | 2.0  | 2.8   | 2.0  |
| Progression Factor                | 1.00 | 1.00 |              | 1.00  | 1.00       |           | 0.73 | 0.66     |      | 0,63 | 0.57  | 0.45 |
| Incremental Delay, d2             | 0.3  | 0.4  |              | 2.3   | 0.2        |           | 0.1  | 0.4      |      | 0.0  | 0.7   | 0.0  |
| Delay (s)                         | 38.6 | 38.8 |              | 41.5  | 38.5       |           | 1.6  | 2.0      |      | 1.3  | 2.3   | 0.9  |
| Level of Service                  | D    | D    |              | D     | D          |           | А    | А        |      | А    | А     | А    |
| Approach Delay (s)                |      | 38.8 |              |       | 40.5       |           |      | 2.0      |      |      | 2.2   |      |
| Approach LOS                      |      | D    |              |       | D          |           |      | А        |      |      | А     |      |
| Intersection Summary              |      |      |              |       |            |           |      |          |      |      |       |      |
| HCM Average Control Delay         |      |      | 7.6          | H     | CM Level   | of Servic | e    |          | A    |      |       |      |
| HCM Volume to Capacity ratio      |      |      | 0.38         |       |            |           |      |          |      |      |       |      |
| Actuated Cycle Length (s)         |      |      | 90.0         | Sı    | um of lost | time (s)  |      |          | 11.6 |      |       |      |
| Intersection Capacity Utilization |      |      | 45.4%        |       | U Level o  |           |      |          | Α    |      |       |      |
| Analysis Period (min)             |      |      | 15           |       |            |           |      |          |      |      |       |      |
| c Critical Lane Group             |      |      |              |       |            |           |      |          |      |      |       |      |

|                                   | <u>_</u> |            | >     | 1     | 4          | ×.        | 4     | Î    | p    | \$   | Å     | 4    |
|-----------------------------------|----------|------------|-------|-------|------------|-----------|-------|------|------|------|-------|------|
| Movement                          | EBL      | EBT        | EBR   | WBL   | WBT        | WBR       | NBL   | NBT  | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | ሻ        | <b>ሰ</b> ኑ |       | ٣     | 作序         |           | ሻ     | ĥ    |      | ሻ    | ĥ     |      |
| Volume (vph)                      | 19       | 437        | 65    | 29    | 456        | 12        | 62    | 151  | 43   | 44   | 267   | 10   |
| Ideal Flow (vphpl)                | 2000     | 2000       | 2000  | 2000  | 2000       | 2000      | 2000  | 2000 | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)               | 6.0      | 6.0        |       | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6,0   |      |
| Lane Util. Factor                 | 1.00     | 0.95       |       | 1.00  | 0.95       |           | 1.00  | 1.00 |      | 1.00 | 1.00  |      |
| Frt                               | 1.00     | 0.98       |       | 1.00  | 1.00       |           | 1.00  | 0.97 |      | 1.00 | 0.99  |      |
| Flt Protected                     | 0.95     | 1.00       |       | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (prot)                 | 1863     | 3653       |       | 1863  | 3711       |           | 1863  | 1896 |      | 1863 | 1950  |      |
| Flt Permitted                     | 0.95     | 1.00       |       | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |      |
| Satd. Flow (perm)                 | 1863     | 3653       |       | 1863  | 3711       |           | 1863  | 1896 |      | 1863 | 1950  |      |
| Peak-hour factor, PHF             | 0.79     | 0.79       | 0.79  | 0.70  | 0.70       | 0.70      | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81 |
| Adj. Flow (vph)                   | 24       | 553        | 82    | 41    | 651        | 17        | 65    | 159  | 45   | 54   | 330   | 12   |
| RTOR Reduction (vph)              | 0        | 11         | 0     | 0     | 2          | 0         | 0     | 12   | 0    | 0    | 2     | 0    |
| Lane Group Flow (vph)             | 24       | 624        | 0     | 41    | 666        | 0         | 65    | 192  | 0    | 54   | 340   | 0    |
| Turn Type                         | Prot     |            |       | Prot  |            |           | Prot  |      |      | Prot |       |      |
| Protected Phases                  | 5        | 2          |       | 1     | 6          |           | 3     | 8    |      | 7    | 4     |      |
| Permitted Phases                  |          |            |       |       |            |           |       |      |      |      |       |      |
| Actuated Green, G (s)             | 3.0      | 33.1       |       | 4.7   | 34.8       |           | 7.3   | 21.2 |      | 7.0  | 20.9  |      |
| Effective Green, g (s)            | 3.0      | 33.1       |       | 4.7   | 34.8       |           | 7.3   | 21.2 |      | 7.0  | 20.9  |      |
| Actuated g/C Ratio                | 0.03     | 0.37       |       | 0.05  | 0.39       |           | 0.08  | 0.24 |      | 0.08 | 0.23  |      |
| Clearance Time (s)                | 6.0      | 6.0        |       | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |      |
| Vehicle Extension (s)             | 3.0      | 3.0        |       | 3.0   | 3.0        |           | 3.0   | 3.0  |      | 3.0  | 3.0   |      |
| Lane Grp Cap (vph)                | 62       | 1343       |       | 97    | 1435       |           | 151   | 447  |      | 145  | 453   |      |
| v/s Ratio Prot                    | 0.01     | 0.17       |       | c0.02 | c0.18      |           | c0.03 | 0.10 |      | 0.03 | c0.17 |      |
| v/s Ratio Perm                    |          |            |       |       |            |           |       |      |      |      |       |      |
| v/c Ratio                         | 0.39     | 0.46       |       | 0.42  | 0.46       |           | 0.43  | 0.43 |      | 0.37 | 0.75  |      |
| Uniform Delay, d1                 | 42.6     | 21.7       |       | 41.3  | 20.6       |           | 39.4  | 29.3 |      | 39.4 | 32.1  |      |
| Progression Factor                | 1.00     | 1.00       |       | 0.82  | 0.71       |           | 1.04  | 1.13 |      | 1.00 | 1.00  |      |
| Incremental Delay, d2             | 4.0      | 1.2        |       | 2.4   | 0.9        |           | 1.9   | 0.7  |      | 1.6  | 6.9   |      |
| Delay (s)                         | 46.6     | 22.9       |       | 36.5  | 15.6       |           | 43.0  | 33.7 |      | 41.0 | 39.0  |      |
| Level of Service                  | D        | С          |       | D     | В          |           | D     | С    |      | D    | D     |      |
| Approach Delay (s)                |          | 23.7       |       |       | 16.8       |           |       | 36.0 |      |      | 39.3  |      |
| Approach LOS                      |          | С          |       |       | В          |           |       | D    |      |      | D     |      |
| Intersection Summary              |          |            |       |       |            |           |       |      |      |      |       |      |
| HCM Average Control Delay         |          |            | 26.0  | Н     | CM Level   | of Servic | e     |      | С    |      |       |      |
| HCM Volume to Capacity ratio      |          |            | 0.51  |       |            |           |       |      |      |      |       |      |
| Actuated Cycle Length (s)         |          |            | 90.0  |       | um of lost |           |       |      | 18.0 |      |       |      |
| Intersection Capacity Utilization |          |            | 57.7% | IC    | CU Level c | f Service |       |      | В    |      |       |      |
| Analysis Period (min)             |          |            | 15    |       |            |           |       |      |      |      |       |      |
| c Critical Lane Group             |          |            |       |       |            |           |       |      |      |      |       |      |

| 4 (<br>00 2(<br>12<br>5.1<br>00 0<br>00 1<br>95 1 | BT<br>12<br>000<br>12<br>6.1<br>95<br>00  | EBR<br>7<br>2000<br>12  | WBL<br>117<br>2000<br>12<br>6.1  | WBT<br>642<br>2000<br>12                             | WBR<br><b>ř</b><br>116<br>2000  | NBL<br><b>Ť</b><br>8  | NBT<br><b>†</b><br>13  | NBR<br><b>ř</b><br>244   | SBL   | SBT<br>Þ  | SBR  |
|---|---|---|--|--|---|---|--|--|---|---|--|
| 4 (<br>00 2(<br>12<br>5.1<br>00 0<br>00 1<br>95 1 | 512<br>000<br>12<br>6.1<br>.95  | 2000  | 117<br>2000<br>12<br>6.1   | 642<br>2000  | 116   | 8   |  |  |   |   |  |
| 00 20<br>12<br>5.1<br>00 0<br>00 1<br>95 1        | )00<br>12<br>6.1<br>.95   | 2000  | 2000<br>12<br>6.1  | 2000   |   |   | 13   | 244  | 100   |   |  |
| 12<br>5.1<br>00 0<br>00 1<br>95 1                 | 12<br>6.1<br>.95  |   | 12<br>6.1  | et an a state and a start of a start of              | 2000  |   |  | <u> </u>   | 182   | 21  | 10   |
| 5.1<br>2000<br>2011<br>9511                       | 6.1<br>.95  | 12  | 6.1  | 12   |   | 2000  | 2000   | 2000   | 2000  | 2000  | 2000   |
| 00 0<br>00 1<br>95 1                              | .95   |   |  |  | 12  | 11  | 11   | 11   | 12  | 12  | 12   |
| 00 1<br>95 1                                      |   |   | en de la composition | 6.1  | 6.1   | 6.0   | 6.0  | 6.0  | 6.0   | 6.0   |  |
| 95 1  | .00   |   | 1.00   | 1.00   | 1.00  | 1.00  | 1.00   | 1.00   | 1.00  | 1.00  |  |
|   |   |   | 1.00   | 1.00   | 0.85  | 1.00  | 1.00   | 0.85   | 1.00  | 0.95  |  |
| 22 27   | .00   |   | 0.95   | 1.00   | 1.00  | 0.95  | 1.00   | 1.00   | 0.95  | 1.00  |  |
| ມີ  | '19   |   | 1863   | 1961   | 1500  | 1801  | 1895   | 1611   | 1863  | 1868  |  |
| 21 1  | .00   |   | 0.17   | 1.00   | 1.00  | 0.73  | 1.00   | 1.00   | 0.57  | 1.00  |  |
|   |   |   | 341  | 1961   | 1500  | 1384  | 1895   | 1611   | 1125  | 1868  |  |
| 76 0  | 76  | 0.76  | 0.83   | 0.83   | 0.83  | 0.83  | 0.83   | 0.83   | 0.75  | 0.75  | 0.75   |
|   |   |   |  |  |   |   |  |  | and the second  |   | 13   |
|   | 1   |   |  |  |   |   |  |  |   |   | 0  |
|   | 13  |   |  |  |   |   |  |  |   |   | 0  |
|   |   | 0   |  |  | 0   |   |  |  |   |   |  |
| m   |   |   | pm+pt  |  | Perm  | Perm  |  | Perm   | pm+pt   |   |  |
|   | 2   |   | <b>!</b> ]   | 6  |   |   | 8  |  | · 7   | 4   |  |
| 2   | 1 I I. e  |   | 6  |  | 6   | 8   |  | 8  | 4   |   |  |
|   | 1.1   |   |  | 45.0   | the second se   |   | 19.9   | 19.9   | 32.9  | 32.9  |  |
|   |   |   |  |  |   |   |  |  |   | 32.9  |  |
|   |   |   | 0.50   | 0.50   | 0.50  | 0.22  | 0.22   | 0.22   | 0.37  | 0.37  |  |
|   |   |   |  |  |   | 6.0   |  |  |   | 6.0   |  |
|   |   |   | 3.0  | 3.0  | 3.0   | 3.0   | 3.0  |  | 3.0   | 3.0   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  | 0.05  | 0.01  |  | c0.18  |   |   |  |
|   | 63  |   |  | 0.79   |   |   | 0.04   |  |   | 0.05  |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   | С   |   |  | С  |   |   | D  |  |   | С   |  |
|   |   |   |  |  |   |   |  |  |   |   |  |
|   |   | 26.8  | Н  | CM Level   | of Servic   | e   |  | С  |   |   |  |
|   |   | 0.79  |  |  |   |   |  |  |   |   |  |
|   |   | 90.0  | S  | um of los  | time (s)  |   |  | 18.1   |   |   |  |
|   | 7   | 1.8%  | IC   | U Level o  | of Service  |   |  | С  |   |   |  |
|   |   | 15  |  |  |   |   |  |  |   |   |  |
|   | 21 1.<br>05 37<br>76 0.<br>5 8<br>0<br>5 0<br>5 8<br>0<br>5 0<br>5 0<br>5 0<br>5 0<br>5 0<br>5 0<br>5 0 | 21 1.00<br>05 3719<br>76 0.76<br>5 805<br>0 1<br>5 813<br>77<br>2<br>2<br>.1 31.1<br>.1 31.1<br>.35 0.35<br>.1 6.1<br>.0 3.0<br>40 1285<br>0.22<br>01<br>04 0.63<br>.5 24.7<br>34 1.01<br>.5 2.3<br>.9 27.2<br>B C<br>27.1<br>C | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 21         1.00         0.17         1.00           05 $3719$ $341$ 1961           76         0.76         0.76         0.83         0.83           5         805         9         141         773           0         1         0         0         0           5         813         0         141         773           0         1         0         0         0           5         813         0         141         773           0         1         0         0         0           76         0.76         0.83         0.83         0.83           0         1         0         0         0         0           5         813         0         141         773           0         7         6         6         1           1         31.1         45.0         45.0         30           .1         31.1         45.0         45.0         30           .1         6.1         6.1         6.1         6.1           .0.3.0         3.0         3.0         3.0         3.0 | 21         1.00         0.17         1.00         1.00           05         3719         341         1961         1500           76         0.76         0.76         0.83         0.83         0.83           5         805         9         141         773         140           0         1         0         0         0         70           5         813         0         141         773         70           0         0         0         70         70           0         0         0         0         70           5         813         0         141         773         70           0         0         0         0         70         70           131.1         45.0         45.0         45.0         45.0           35         0.35         0.50         0.50         0.50           36         0.35         302         981         750           0.22         0.04         c0.39         70         0.09           0.4         0.63         0.47         0.79         0.09           0.5         2.3         1.1 | 21       1.00       0.17       1.00       1.00       0.73         05       3719       341       1961       1500       1384         76       0.76       0.76       0.83       0.83       0.83       0.83         5       805       9       141       773       140       10         0       1       0       0       70       0         5       813       0       141       773       70       10         0       1       0       0       70       0       0         5       813       0       141       773       70       10         0       0       0       0       70       0       0         70       10       0       0       0       0       0         70       10       0       0       0       0       0       0         70       10       0       0       0       0       0       0       0       0       19.9         1.1       45.0       45.0       45.0       19.9       0       0       0       2       2       14.5       16.1       6.1 | 21       1.00       0.17       1.00       1.00       0.73       1.00         05       3719       341       1961       1500       1384       1895         76       0.76       0.83       0.83       0.83       0.83       0.83       0.83         5       805       9       141       773       140       10       16         0       1       0       0       0       70       0       0         5       813       0       141       773       70       10       16         0       0       0       0       0       0       0       0         70       10       16       0       0       0       0       0         70       10       16       6       8       1       31.1       45.0       45.0       19.9       10.1       10.1       10.1       10.1       10.1       10.1       10 | 21         1.00         0.17         1.00         1.00         0.73         1.00         1.00           05         3719         341         1961         1500         1384         1895         1611           76         0.76         0.76         0.83 | 21       1.00       0.17       1.00       1.00       0.73       1.00       1.00       0.57         05       3719       341       1961       1500       1384       1895       1611       1125         76       0.76       0.76       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.83       0.75         5       805       9       141       773       140       10       16       294       243         0       1       0       0       0       70       0       0       0       0         5       813       0       141       773       70       10       16       294       243         0       0       0       0       0       0       0       0       0         72       6       6       8       8       4       1       31.1       45.0       45.0       19.9       19.9       19.9       32.9       32.9       35       0.50       0.50       0.22       0.22       0.22       0.22       0.22       0.22       0.22       0.22       0.22 | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ |

|  | ٨                                    |      | 7     | 1    |                        | Ł          | ٩              | Ť           | p          | 1    | ļ                    | ~    |
|--|--------------------------------------|------|-------|------|------------------------|------------|----------------|-------------|------------|------|----------------------|------|
| Movement                                       | EBL                                  | EBT  | EBR   | WBL  | WBT                    | WBR        | NBL            | NBT         | NBR        | SBL  | SBT                  | SBR  |
| Lane Configurations                            | ኻኻ                                   | ∱    | ۴     | ኻኻ   | Ł                      | ŕ          | ሻ              | <b>∱</b> ĵ≽ |            | ሻ    | 个个                   | 7    |
| Volume (vph)                                   | 621                                  | 55   | 329   | 155  | 46                     | 0          | 75             | 404         | 44         | 0    | 600                  | 132  |
| Ideal Flow (vphpl)                             | 2000                                 | 2000 | 2000  | 2000 | 2000                   | 2000       | 2000           | 2000        | 2000       | 2000 | 2000                 | 2000 |
| Total Lost time (s)                            | 6.0                                  | 6.0  | 6.0   | 6.0  | 6.0                    |            | 6.6            | 6.6         |            |      | 6.6                  | 6.6  |
| Lane Util. Factor                              | 0.97                                 | 1.00 | 1.00  | 0.97 | 1.00                   |            | 1.00           | 0.95        |            |      | 0.95                 | 1.00 |
| Frt  | 1.00                                 | 1.00 | 0.85  | 1.00 | 1.00                   |            | 1.00           | 0.99        |            |      | 1.00                 | 0.85 |
| Flt Protected                                  | 0.95                                 | 1.00 | 1.00  | 0.95 | 1.00                   |            | 0.95           | 1.00        |            |      | 1.00                 | 1.00 |
| Satd. Flow (prot)                              | 3614                                 | 1961 | 1667  | 3614 | 1961                   |            | 1863           | 3670        |            |      | 3725                 | 1667 |
| Flt Permitted                                  | 0.95                                 | 1.00 | 1.00  | 0.95 | 1.00                   |            | 0.35           | 1.00        |            |      | 1.00                 | 1.00 |
| Satd. Flow (perm)                              | 3614                                 | 1961 | 1667  | 3614 | 1961                   |            | 677            | 3670        |            |      | 3725                 | 1667 |
| Peak-hour factor, PHF                          | 0.92                                 | 0.92 | 0.92  | 0.92 | 0.92                   | 0.92       | 0.92           | 0.92        | 0.92       | 0.92 | 0.92                 | 0.92 |
| Adj. Flow (vph)                                | 675                                  | 60   | 358   | 168  | 50                     | 0          | 82             | 439         | 48         | 0    | 652                  | 143  |
| RTOR Reduction (vph)                           | 0                                    | 0    | 151   | 0    | 0                      | 0          | 0              | 9           | 0          | 0    | 0                    | 76   |
| Lane Group Flow (vph)                          | 675                                  | 60   | 207   | 168  | 50                     | 0          | 82             | 478         | 0          | Ō    | 652                  | 67   |
| Turn Type                                      | Prot                                 |      | Perm  | Prot |                        | Perm       | Perm           |             |            | Perm |                      | Perm |
| Protected Phases                               | 7                                    | 4    |       | 3    | 8                      |            |                | 2           |            |      | 6                    |      |
| Permitted Phases                               | anta dalah dan bahara                |      | 4     |      | ya a sa ya ba ay bada. | 8          | 2              |             |            | 6    | e os a contraista da | 6    |
| Actuated Green, G (s)                          | 21.1                                 | 18.8 | 18.8  | 8.9  | 6.6                    |            | 29.7           | 29.7        |            |      | 29.7                 | 29.7 |
| Effective Green, g (s)                         | 21.1                                 | 18.8 | 18.8  | 8.9  | 6.6                    |            | 29.7           | 29.7        |            |      | 29.7                 | 29.7 |
| Actuated g/C Ratio                             | 0.28                                 | 0.25 | 0.25  | 0.12 | 0.09                   |            | 0.39           | 0.39        |            |      | 0.39                 | 0.39 |
| Clearance Time (s)                             | 6.0                                  | 6.0  | 6.0   | 6.0  | 6.0                    |            | 6.6            | 6.6         |            |      | 6.6                  | 6.6  |
| Vehicle Extension (s)                          | 3.0                                  | 3.0  | 3.0   | 3.0  | 3.0                    |            | 3.0            | 3.0         |            |      | 3.0                  | 3.0  |
| Lane Grp Cap (vph)                             | 1003                                 | 485  | 412   | 423  | 170                    |            | 265            | 1434        |            |      | 1456                 | 651  |
| v/s Ratio Prot                                 | c0.19                                | 0.03 |       | 0.05 | 0.03                   |            |                | 0.13        |            |      | c0.18                |      |
| v/s Ratio Perm                                 |                                      |      | c0.12 |      |                        |            | 0.12           |             |            |      |                      | 0.04 |
| v/c Ratio                                      | 0.67                                 | 0.12 | 0.50  | 0.40 | 0.29                   |            | 0.31           | 0.33        |            |      | 0.45                 | 0.10 |
| Uniform Delay, d1                              | 24.4                                 | 22.2 | 24.6  | 31.1 | 32.5                   |            | 16.0           | 16.2        |            |      | 17.1                 | 14.7 |
| Progression Factor                             | 1.00                                 | 1.00 | 1.00  | 1.00 | 1.00                   |            | 1.00           | 1.00        |            |      | 1.00                 | 1.00 |
| Incremental Delay, d2                          | 1.8                                  | 0.1  | 1.0   | 0.6  | 1.0                    |            | 3.0            | 0.6         |            |      | 1.0                  | 0.3  |
| Delay (s)                                      | 26.2                                 | 22.3 | 25.6  | 31.7 | 33.5                   |            | 19.1           | 16.8        |            |      | 18.1                 | 15.0 |
| Level of Service                               | C                                    | C    | C     | С    | C                      |            | В              | В           |            |      | В                    | В    |
| Approach Delay (s)                             |                                      | 25.8 |       |      | 32.1                   |            |                | 17.2        |            |      | 17.5                 |      |
| Approach LOS                                   | an an an Arail Anaich<br>An Anaichte | C    |       |      | C                      |            | an dhara da dh | B           |            |      | В                    |      |
| Intersection Summary                           |                                      |      |       |      |                        |            |                |             |            |      |                      |      |
| HCM Average Control Delay                      | у                                    |      | 22.0  | Н    | CM Level               | of Servic  | e              |             | С          |      |                      |      |
| HCM Volume to Capacity ra                      | atio                                 |      | 0.51  |      |                        |            |                |             |            |      |                      |      |
| Actuated Cycle Length (s)                      |                                      |      | 76.0  | Sı   | im of lost             | time (s)   |                |             | 12.6       |      |                      |      |
| Intersection Capacity Utiliza                  | ition                                |      | 63.6% | IC   | U Level c              | of Service |                |             | В          |      |                      |      |
| Analysis Period (min)<br>c Critical Lane Group |                                      |      | 15    |      |                        |            |                |             | N - Nya Ka |      |                      |      |

|                               | ٨                     |           | $\mathbf{i}$ | ¥           | 4          |                          | 4                    | Î             | p         | \$        | Ť         | 1         |
|-------------------------------|-----------------------|-----------|--------------|-------------|------------|--------------------------|----------------------|---------------|-----------|-----------|-----------|-----------|
| Movement                      | EBL                   | EBT       | EBR          | WBL         | WBT        | WBR                      | NBL                  | NBT           | NBR       | SBL       | SBT       | SBR       |
| Lane Configurations           | ሻ                     | ŕ         | ŕ            | ሻ           | ĥ          |                          | ĥ                    | ¢1            |           | ሻ         | ት         | ř         |
| Volume (vph)                  | 110                   | 158       | 243          | 142         | 268        | 4                        | 249                  | 595           | 60        | 3         | 348       | 144       |
| Ideal Flow (vphpl)            | 2000                  | 2000      | 2000         | 2000        | 2000       | 2000                     | 2000                 | 2000          | 2000      | 2000      | 2000      | 2000      |
| Total Lost time (s)           | 6.1                   | 6.1       | 6.1          | 6.1         | 6.1        |                          | 5.9                  | 5.9           |           | 5.9       | 5.9       | 5.9       |
| Lane Util. Factor             | 1.00                  | 1.00      | 1.00         | 1.00        | 1.00       |                          | 1.00                 | 1.00          |           | 1.00      | 1.00      | 1.00      |
| Frt                           | 1.00                  | 1.00      | 0.85         | 1.00        | 1.00       |                          | 1.00                 | 0.99          |           | 1.00      | 1.00      | 0.85      |
| Fit Protected                 | 0.95                  | 1.00      | 1.00         | 0.95        | 1.00       |                          | 0.95                 | 1.00          |           | 0.95      | 1.00      | 1.00      |
| Satd. Flow (prot)             | 1881                  | 2000      | 1619         | 1863        | 1938       |                          | 1743                 | 1922          |           | 1900      | 1980      | 1650      |
| Flt Permitted                 | 0.24                  | 1.00      | 1.00         | 0.56        | 1.00       |                          | 0.40                 | 1.00          |           | 0.13      | 1.00      | 1.00      |
| Satd. Flow (perm)             | 478                   | 2000      | 1619         | 1094        | 1938       |                          | 741                  | 1922          |           | 263       | 1980      | 1650      |
| Peak-hour factor, PHF         | 0.83                  | 0.83      | 0.83         | 0.80        | 0.80       | 0.80                     | 0.90                 | 0.90          | 0.90      | 0.95      | 0.95      | 0.95      |
| Adj. Flow (vph)               | 133                   | 190       | 293          | 178         | 335        | 5                        | 277                  | 661           | 67        | 3         | 366       | 152       |
| RTOR Reduction (vph)          | 0                     | 0         | 189          | 0           | 1          | 0                        | 0                    | 4             | 0         | 0         | 0         | 101       |
| Lane Group Flow (vph)         | 133                   | 190       | 104          | 178         | 339        | Ō                        | 277                  | 724           | Ō         | 3         | 366       | 51        |
| Heavy Vehicles (%)            | 1%                    | 0%        | 5%           | 2%          | 3%         | 0%                       | 9%                   | 2%            | 9%        | 0%        | 1%        | 3%        |
| Turn Type                     | pm+pt                 |           | Perm         | pm+pt       |            |                          | pm+pt                |               |           | Perm      |           | Perm      |
| Protected Phases              | 7                     | 4         |              | 3           | 8          |                          | 5 pm                 | 2             |           |           | 6         |           |
| Permitted Phases              | 4                     |           | 4            | 8           |            |                          | 2                    |               |           | 6         |           | 6         |
| Actuated Green, G (s)         | 25.5                  | 18.6      | 18.6         | 25.5        | 18.6       |                          | 46.4                 | 46.4          |           | 30.4      | 30.4      | 30.4      |
| Effective Green, g (s)        | 25.5                  | 18.6      | 18.6         | 25.5        | 18.6       |                          | 46.4                 | 46.4          |           | 30.4      | 30.4      | 30.4      |
| Actuated g/C Ratio            | 0.28                  | 0.21      | 0.21         | 0.28        | 0.21       | us a pagagana.           | 0.52                 | 0.52          |           | 0.34      | 0.34      | 0.34      |
| Clearance Time (s)            | 6.1                   | 6.1       | 6.1          | 6.1         | 6.1        |                          | 5.9                  | 5.9           |           | 5.9       | 5.9       | 5.9       |
| Vehicle Extension (s)         | 3.0                   | 3.0       | 3.0          | 3.0         | 3.0        | al en Veren en           | 3.0                  | 3.0           |           | 3.0       | 3.0       | 3.0       |
| Lane Grp Cap (vph)            | 243                   | 413       | 335          | 369         | 401        | 4.855.83                 | 494                  | 991           |           | 89        | 669       | 557       |
| v/s Ratio Prot                | c0.04                 | 0.10      | 000          | 0.04        | c0.18      |                          | 0.06                 | c0.38         |           | 03        | 0.18      | 001       |
| v/s Ratio Perm                | 0.11                  | 0.10      | 0.06         | 0.04        | 00.10      |                          | 0.00                 |               |           | 0.01      | 0.10      | 0.03      |
| v/c Ratio                     | 0.55                  | 0.46      | 0.31         | 0.10        | 0.85       |                          | 0.20                 | 0.73          |           | 0.03      | 0.55      | 0.09      |
| Uniform Delay, d1             | 25.6                  | 31.3      | 30.3         | 25.6        | 34.3       |                          | 21.5                 | 16.9          |           | 20.0      | 24.2      | 20.4      |
| Progression Factor            | 1.00                  | 1.00      | 1.00         | 1.00        | 1.00       |                          | 1.00                 | 1.00          |           | 1.16      | 1.21      | 1.79      |
| Incremental Delay, d2         | 2.5                   | 0.8       | 0.5          | 1.0         | 15.1       |                          | 1.00                 | 4.7           |           | 0.7       | 3.1       | 0.3       |
| Delay (s)                     | 28.1                  | 32.1      | 30.8         | 26.6        | 49.4       |                          | 23.0                 | 21.7          |           | 23.9      | 32.4      | 36.8      |
| Level of Service              | 20.1<br>C             | 52.1<br>C | 50.0<br>C    | 20.0<br>C   | -5.4<br>D  |                          | 20.0<br>C            | 21.7<br>C     |           | 20.0<br>C | 52.4<br>C | 50.0<br>D |
| Approach Delay (s)            | ni kineli <b>M</b> ah | 30.6      |              | U           | 41.5       |                          |                      | 22.0          |           | U         | 33.7      | <b>-</b>  |
| Approach LOS                  |                       | 00.0<br>C |              |             | т<br>D     |                          |                      | 22.0<br>C     |           |           | 55.7<br>C |           |
| Intersection Summary          |                       |           |              |             |            |                          |                      |               |           |           |           |           |
| HCM Average Control Dela      | ٩V                    |           | 30.1         | H           | CM Level   | of Servic                | :e                   |               | C         |           |           |           |
| HCM Volume to Capacity r      |                       |           | 0.74         | nevî derdî. |            | 51 001 410               | 🕶 gan period         | n inder solid |           |           |           |           |
| Actuated Cycle Length (s)     |                       | <u></u>   | 90.0         | ۹           | um of losi | time (s)                 | 0.38534.2            |               | 18.1      | 1787 S.A. |           |           |
| Intersection Capacity Utiliza | ation                 |           | 81.0%        |             | U Level (  | deneral relation and the | ang 3067 (B. A.<br>N |               | 10.1<br>D |           |           |           |
| Analysis Period (min)         |                       |           | 15           |             |            |                          |                      |               |           |           |           |           |

|  | ▲    |      | ¥           | 1     | <b>4</b> — | Ł          | ٩        | Î     | 1    | 1    | Ť    | 4    |
|--|------|------|-------------|-------|------------|------------|----------|-------|------|------|------|------|
| Movement   | EBL  | EBT  | EBR         | WBL   | WBT        | WBR        | NBL      | NBT   | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations  | ሻ    | ∱≯   |             | ሻ     | ₽          |            | ኻ        | ₿     |      | ሻ    | ዯ    | ሻ    |
| Volume (vph)   | 20   | 20   | 100         | 190   | 20         | 60         | 20       | 430   | 80   | 10   | 420  | 30   |
| Ideal Flow (vphpl)   | 2000 | 2000 | 2000        | 2000  | 2000       | 2000       | 2000     | 2000  | 2000 | 2000 | 2000 | 2000 |
| Total Lost time (s)  | 5.8  | 5.8  |             | 5.8   | 5.8        |            | 5.8      | 5.8   |      | 5.8  | 5.8  | 5.8  |
| Lane Util. Factor  | 1.00 | 1.00 |             | 1.00  | 1.00       |            | 1.00     | 1.00  |      | 1.00 | 1.00 | 1.00 |
| Frt  | 1.00 | 0.88 |             | 1.00  | 0.89       |            | 1.00     | 0.98  |      | 1.00 | 1.00 | 0.85 |
| Flt Protected  | 0.95 | 1.00 |             | 0.95  | 1.00       |            | 0.95     | 1.00  |      | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot)  | 1863 | 1716 |             | 1863  | 1741       |            | 1863     | 1915  |      | 1863 | 1961 | 1667 |
| Flt Permitted  | 0.70 | 1.00 |             | 0.67  | 1.00       |            | 0.46     | 1.00  |      | 0.39 | 1.00 | 1.00 |
| Satd. Flow (perm)  | 1374 | 1716 |             | 1320  | 1741       |            | 901      | 1915  |      | 774  | 1961 | 1667 |
| Peak-hour factor, PHF                                      | 0.92 | 0.92 | 0.92        | 0.92  | 0.92       | 0.92       | 0.92     | 0.92  | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph)  | 22   | 22   | 109         | 207   | 22         | 65         | 22       | 467   | 87   | 11   | 457  | 33   |
| RTOR Reduction (vph)                                       | 0    | 86   | 0           | 0     | 51         | 0          | 0        | 6     | 0    | 0    | 0    | 11   |
| Lane Group Flow (vph)                                      | 22   | 45   | 0           | 207   | 36         | 0          | 22       | 548   | 0    | 11   | 457  | 22   |
| Turn Type  | Perm |      |             | Perm  |            |            | Perm     |       |      | Perm |      | Perm |
| Protected Phases   |      | 4    |             |       | 8          |            |          | 2     |      |      | 6    |      |
| Permitted Phases   | 4    |      |             | 8     |            |            | 2        |       |      | 6    |      | 6    |
| Actuated Green, G (s)                                      | 19.4 | 19.4 |             | 19.4  | 19.4       |            | 59.0     | 59.0  |      | 59.0 | 59.0 | 59.0 |
| Effective Green, g (s)                                     | 19.4 | 19.4 |             | 19.4  | 19.4       |            | 59.0     | 59.0  |      | 59.0 | 59.0 | 59.0 |
| Actuated g/C Ratio   | 0.22 | 0.22 |             | 0.22  | 0.22       |            | 0.66     | 0.66  |      | 0.66 | 0.66 | 0.66 |
| Clearance Time (s)   | 5.8  | 5.8  |             | 5.8   | 5.8        |            | 5.8      | 5.8   |      | 5.8  | 5.8  | 5.8  |
| Vehicle Extension (s)                                      | 3.0  | 3.0  |             | 3.0   | 3.0        |            | 3.0      | 3.0   |      | 3.0  | 3.0  | 3.0  |
| Lane Grp Cap (vph)   | 296  | 370  |             | 285   | 375        |            | 591      | 1255  |      | 507  | 1286 | 1093 |
| v/s Ratio Prot   |      | 0.03 |             |       | 0.02       |            |          | c0.29 |      |      | 0.23 |      |
| v/s Ratio Perm   | 0.02 |      |             | c0.16 |            |            | 0.02     |       |      | 0.01 |      | 0.01 |
| v/c Ratio  | 0.07 | 0.12 |             | 0.73  | 0.10       |            | 0.04     | 0.44  |      | 0.02 | 0.36 | 0.02 |
| Uniform Delay, d1  | 28.1 | 28.4 |             | 32.8  | 28.3       |            | 5.5      | 7.5   |      | 5.4  | 7.0  | 5.4  |
| Progression Factor   | 1.00 | 1.00 |             | 1.00  | 1.00       |            | 0.78     | 1.00  |      | 0.73 | 0.57 | 0.63 |
| Incremental Delay, d2                                      | 0.1  | 0.1  |             | 8.9   | 0.1        |            | 0.1      | 1.0   |      | 0.1  | 0.7  | 0.0  |
| Delay (s)  | 28.2 | 28.6 |             | 41.7  | 28.4       |            | 4.4      | 8.5   |      | 4.0  | 4.6  | 3.4  |
| Level of Service   | С    | С    |             | D     | С          |            | А        | А     |      | А    | А    | А    |
| Approach Delay (s)   |      | 28.5 |             |       | 37.8       |            |          | 8.3   |      |      | 4.5  |      |
| Approach LOS   |      | С    |             |       | D          |            |          | Α     |      |      | А    |      |
| Intersection Summary                                       |      |      |             |       |            |            |          |       |      |      |      |      |
| HCM Average Control Delay                                  |      |      | 14.8        | H     | CM Level   | of Service | <b>)</b> |       | В    |      |      |      |
| HCM Volume to Capacity ratio                               |      |      | 0.51        |       |            |            |          |       |      |      |      |      |
| Actuated Cycle Length (s)                                  |      |      | 90.0        |       | um of lost |            |          |       | 11.6 |      |      |      |
| Intersection Capacity Utilization<br>Analysis Period (min) | 1.   |      | 52.4%<br>15 | IC    | U Level c  | of Service |          |       | А    |      |      |      |
| c Critical Lane Group                                      |      |      |             |       |            |            |          |       |      |      |      |      |

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|--------------------------------|------|-------------------------|--|-------|-----------------------|-----------|-------|------------------|------------------------|---|------|---------|
| Movement                       | EBL  | EBT                     | EBR  | WBL   | WBT                   | WBR       | NBL   | NBT              | NBR                    | SBL                                       | SBT  | SBR     |
| Lane Configurations            | ሻ    | <b>ት</b> ኈ              |  | ኻ     | <b>⋪</b> ኈ            |           | ሻ     | 4Î               |                        | ሻ   | \$   |         |
| Volume (vph)                   | 52   | 516                     | 75   | 66    | 510                   | 104       | 83    | 318              | 37                     | 68  | 282  | 18      |
| Ideal Flow (vphpl)             | 2000 | 2000                    | 2000   | 2000  | 2000                  | 2000      | 2000  | 2000             | 2000                   | 2000                                      | 2000 | 2000    |
| Total Lost time (s)            | 6.0  | 6.0                     |  | 6.0   | 6.0                   |           | 6.0   | 6.0              |                        | 6.0                                       | 6.0  |         |
| Lane Util. Factor              | 1.00 | 0.95                    |  | 1.00  | 0.95                  |           | 1.00  | 1.00             |                        | 1.00                                      | 1.00 |         |
| Frt                            | 1.00 | 0.98                    |  | 1.00  | 0.97                  |           | 1.00  | 0.98             |                        | 1.00                                      | 0.99 |         |
| Flt Protected                  | 0.95 | 1.00                    |  | 0.95  | 1.00                  |           | 0.95  | 1.00             |                        | 0.95                                      | 1.00 |         |
| Satd. Flow (prot)              | 1863 | 3655                    |  | 1863  | 3631                  |           | 1863  | 1930             |                        | 1863                                      | 1943 |         |
| Flt Permitted                  | 0.95 | 1.00                    |  | 0.95  | 1.00                  |           | 0.95  | 1.00             |                        | 0.95                                      | 1.00 |         |
| Satd. Flow (perm)              | 1863 | 3655                    |  | 1863  | 3631                  |           | 1863  | 1930             |                        | 1863                                      | 1943 |         |
| Peak-hour factor, PHF          | 0.90 | 0.90                    | 0.90   | 0.92  | 0.92                  | 0.92      | 0.89  | 0.89             | 0.89                   | 0.90                                      | 0.90 | 0.90    |
| Adj. Flow (vph)                | 58   | 573                     | 83   | 72    | 554                   | 113       | 93    | 357              | 42                     | 76  | 313  | 20      |
| RTOR Reduction (vph)           | 0    | 11                      | 0  | 0     | 16                    | 0         | 0     | 4                | 0                      | 0   | 2    | 0       |
| Lane Group Flow (vph)          | 58   | 645                     | 0  | 72    | 651                   | 0         | 93    | 395              | 0                      | 76  | 331  | 0       |
| Turn Type                      | Prot |                         |  | Prot  |                       |           | Prot  |                  |                        | Prot                                      |      |         |
| Protected Phases               | 5    | 2                       |  | 1     | 6                     |           | 3     | 8                |                        | 7   | 4    |         |
| Permitted Phases               |      | , characteristic († 200 |  |       | ang dia nisila (Tal G |           | .:    | nin na dhairtean |                        | ing ang ang ang ang ang ang ang ang ang a |      |         |
| Actuated Green, G (s)          | 6.6  | 25.4                    |  | 7.0   | 25.8                  |           | 8.6   | 25.7             |                        | 7.9                                       | 25.0 |         |
| Effective Green, g (s)         | 6.6  | 25.4                    |  | 7.0   | 25.8                  |           | 8.6   | 25.7             |                        | 7.9                                       | 25.0 |         |
| Actuated g/C Ratio             | 0.07 | 0.28                    |  | 0.08  | 0.29                  |           | 0.10  | 0.29             |                        | 0.09                                      | 0.28 |         |
| Clearance Time (s)             | 6.0  | 6.0                     |  | 6.0   | 6.0                   |           | 6.0   | 6.0              |                        | 6.0                                       | 6.0  |         |
| Vehicle Extension (s)          | 3.0  | 3.0                     |  | 3.0   | 3.0                   |           | 3.0   | 3.0              |                        | 3.0                                       | 3.0  |         |
| Lane Grp Cap (vph)             | 137  | 1032                    |  | 145   | 1041                  |           | 178   | 551              |                        | 164                                       | 540  | <u></u> |
| v/s Ratio Prot                 | 0.03 | 0.18                    |  | c0.04 | c0.18                 |           | c0.05 | c0.20            |                        | 0.04                                      | 0.17 |         |
| v/s Ratio Perm                 | 0.00 | 0.10                    |  | 00.01 | 00.10                 |           | 00.00 | 00.20            |                        | 0,01                                      | 0.17 |         |
| v/c Ratio                      | 0.42 | 0.63                    |  | 0.50  | 0.62                  |           | 0.52  | 0.72             |                        | 0.46                                      | 0.61 |         |
| Uniform Delay, d1              | 39.9 | 28.2                    |  | 39.8  | 27.9                  |           | 38.7  | 28.9             |                        | 39.0                                      | 28.3 |         |
| Progression Factor             | 1.00 | 1.00                    |  | 1.17  | 1.09                  |           | 1.35  | 0,63             |                        | 1.00                                      | 1.00 |         |
| Incremental Delay, d2          | 2.1  | 2.9                     |  | 2.3   | 2.5                   |           | 2.6   | 4.2              |                        | 2.1                                       | 2.1  |         |
| Delay (s)                      | 42.0 | 31.0                    |  | 48.9  | 32.8                  |           | 54.8  | 22.5             |                        | 41.1                                      | 30.3 |         |
| Level of Service               | D    | С                       |  | D     | C                     |           | D     | C                |                        | D   | C    |         |
| Approach Delay (s)             |      | 31.9                    |  |       | 34.3                  |           |       | 28.6             |                        |   | 32.3 |         |
| Approach LOS                   |      | C C                     |  |       | C C                   |           |       | 20.0<br>C        |                        |   | C    |         |
|                                |      |                         | The state of the s |       |                       |           |       | <b>.</b>         | Statesco Planta Contra |   | •    |         |
| Intersection Summary           |      |                         |  |       |                       |           |       |                  |                        |   |      |         |
| HCM Average Control Delay      |      |                         | 32.1   | Н     | CM Level              | of Servic | e     |                  | С                      |   |      |         |
| HCM Volume to Capacity rat     | io   |                         | 0.54   |       |                       |           |       |                  |                        |   |      |         |
| Actuated Cycle Length (s)      |      |                         | 90.0   |       | um of lost            |           |       |                  | 12.0                   |   |      |         |
| Intersection Capacity Utilizat | ion  |                         | 66.2%  | IC    | U Level o             | f Service |       |                  | С                      |   |      |         |
| Analysis Period (min)          |      |                         | 15   |       |                       |           |       |                  |                        |   |      |         |
| c Critical Lane Group          |      |                         |  |       |                       |           |       |                  |                        |   |      |         |

|  | ۶         |  | ¥     | 1         | 4        | ٨.          | 1    | Î            | Þ         | 1          | ţ                 | ~            |
|--|-----------|--|-------|-----------|----------|-------------|------|--------------|-----------|------------|-------------------|--------------|
| Movement   | EBL       | EBT  | EBR   | WBL       | WBT      | WBR         | NBL  | NBT          | NBR       | SBL        | SBT               | SBF          |
| Lane Configurations  | ሻ         | 飰  |       | ሻ         | <b>∱</b> | 7           | ሻ    | <del>۴</del> | ሻ         | ሻ          | \$                |              |
| Volume (vph)   | 15        | 845  | 17    | 274       | 754      | 400         | 43   | 55           | 287       | 296        | 122               | 35           |
| Ideal Flow (vphpl)   | 2000      | 2000   | 2000  | 2000      | 2000     | 2000        | 2000 | 2000         | 2000      | 2000       | 2000              | 2000         |
| Lane Width   | 12        | 12   | 12    | 12        | 12       | 12          | 11   | 11           | 11        | 12         | 12                | 12           |
| Total Lost time (s)  | 6.1       | 6.1  |       | 6.1       | 6.1      | 6.0         | 6.0  | 6.0          | 6.1       | 6.0        | 6.0               |              |
| Lane Util. Factor  | 1.00      | 0.95   |       | 1.00      | 1.00     | 1.00        | 1.00 | 1.00         | 1.00      | 1.00       | 1.00              |              |
| Frt  | 1.00      | 1.00   |       | 1.00      | 1.00     | 0.85        | 1.00 | 1.00         | 0.85      | 1.00       | 0.97              |              |
| Fit Protected  | 0.95      | 1.00   |       | 0.95      | 1.00     | 1.00        | 0.95 | 1.00         | 1.00      | 0.95       | 1.00              |              |
| Satd. Flow (prot)  | 1863      | 3715   |       | 1863      | 1961     | 1500        | 1801 | 1895         | 1611      | 1863       | 1895              |              |
| Flt Permitted  | 0.32      | 1.00   |       | 0.12      | 1.00     | 1.00        | 0.65 | 1.00         | 1.00      | 0.45       | 1.00              |              |
| Satd. Flow (perm)  | 636       | 3715   |       | 227       | 1961     | 1500        | 1230 | 1895         | 1611      | 884        | 1895              | ala ann an a |
| Peak-hour factor, PHF                                      | 0.88      | 0.88   | 0.88  | 0.92      | 0.92     | 0.92        | 0.94 | 0.94         | 0.94      | 0.92       | 0.92              | 0.92         |
| Adj. Flow (vph)  | 17        | 960  | 19    | 298       | 820      | 435         | 46   | 59           | 305       | 322        | 133               | 38           |
| RTOR Reduction (vph)                                       | 0         | 1  | 0     | 0         | 0        | 136         | 0    | 0            | 0         |            | 13                | 0            |
| Lane Group Flow (vph)                                      | 17        | 978  | 0     | 298       | 820      | 299         | 46   | 59           | 305       | 322        | 158               | 0            |
| Parking (#/hr)   |           |  | 0     |           |          | 0           |      |              |           |            |                   |              |
| Turn Type  | Perm      | and the second |       | pm+pt     |          | pm+ov       | Perm |              | pm+ov     | pm+pt      |                   |              |
| Protected Phases   |           | 2  |       | - Pin Pi  | 6        | 7           |      | 8            | 1         | рш р.<br>7 | 4                 |              |
| Permitted Phases   | 2         | 2300800.000 <del>7</del> 0   |       | 6         |          | 6           | 8    |              | 8         | 4          | n Alberta Mallera |              |
| Actuated Green, G (s)                                      | 28.5      | 28.5   |       | 51.8      | 51.8     | 61.8        | 10.1 | 10.1         | 27.3      | 26.1       | 26.1              |              |
| Effective Green, g (s)                                     | 28.5      | 28.5   |       | 51.8      | 51.8     | 61.8        | 10.1 | 10.1         | 27.3      | 26.1       | 26.1              |              |
| Actuated g/C Ratio   | 0.32      | 0.32   |       | 0.58      | 0.58     | 0.69        | 0.11 | 0.11         | 0.30      | 0.29       | 0.29              |              |
| Clearance Time (s)   | 6.1       | 6.1  |       | 6.1       | 6.1      | 6.0         | 6.0  | 6.0          | 6.1       | 6.0        | 6.0               |              |
| Vehicle Extension (s)                                      | 3.0       | 3.0  |       | 3.0       | 3.0      | 3.0         | 3.0  | 3.0          | 3.0       | 3.0        | 3.0               |              |
| Lane Grp Cap (vph)   | 201       | 1176   |       | 443       | 1129     | 1030        | 138  | 213          | 489       | 365        | 550               |              |
| v/s Ratio Prot   | 201       | c0.26  |       | 0.13      | c0.42    | 0.03        | 100  | 0.03         | 0.12      | c0.10      | 0.08              |              |
| v/s Ratio Perm   | 0.03      | 00.20  |       | 0.26      | 00.12    | 0.00        | 0.04 | 0.00         | 0.12      | c0.16      | 0.00              |              |
| v/c Ratio  | 0.08      | 0.83   |       | 0.67      | 0.73     | 0.29        | 0.33 | 0.28         | 0.62      | 0.88       | 0.29              |              |
| Uniform Delay, d1  | 21.6      | 28.5   |       | 19.1      | 13.9     | 5.5         | 36.8 | 36.6         | 26.9      | 29.2       | 24.7              |              |
| Progression Factor   | 1.16      | 0.92   |       | 1.00      | 1.00     | 1.00        | 1.00 | 1.00         | 1.00      | 1.00       | 1.00              |              |
| Incremental Delay, d2                                      | 0.8       | 6.7  |       | 4.0       | 4.1      | 0.2         | 1.4  | 0.7          | 2.5       | 21.3       | 0.3               |              |
| Delay (s)  | 25.8      | 33.1   |       | 23.1      | 18.0     | 5.7         | 38.3 | 37.3         | 29.4      | 50.5       | 25.0              |              |
| Level of Service   | 20.0<br>С | 00.1<br>C  |       | 20.1<br>C | В        | A           | D    | 07.0<br>D    | 20.4<br>C | 00.0<br>D  | 20.0<br>C         |              |
| Approach Delay (s)   |           | 33.0   |       |           | 15.5     |             |      | 31.5         |           |            | 41.7              |              |
| Approach LOS   |           | C  |       |           | B        |             |      | 01.0<br>C    |           |            | D                 |              |
| Intersection Summary                                       |           |  |       |           |          |             |      |              |           |            |                   |              |
| HCM Average Control Delay                                  |           |  | 26.2  | Н         | CM Leve  | l of Servic | е    |              | С         |            |                   |              |
| HCM Volume to Capacity ratio                               |           |  | 0.84  |           |          |             |      |              |           |            |                   |              |
| Actuated Cycle Length (s)                                  |           |  | 90.0  |           |          | st time (s) |      |              | 18.2      |            |                   |              |
| Intersection Capacity Utilization<br>Analysis Period (min) |           |  | 90.1% | IC        | U Level  | of Service  |      |              | E         |            |                   |              |
| c Critical Lane Group                                      |           |  | 15    |           |          |             |      |              |           |            |                   |              |

|  | ٨  |                 | *     | <b>*</b> | 4          | Ł          | ٩     | Î          | Þ                                     | 6     | ţ    | 4    |
|--|--|-----------------|-------|----------|------------|------------|-------|------------|---------------------------------------|-------|------|------|
| Movement                                       | EBL  | EBT             | EBR   | WBL      | WBT        | WBR        | NBL   | NBT        | NBR                                   | SBL   | SBT  | SBR  |
| Lane Configurations                            | ኻኻ   | ዯ               | ۲     | ኻኻ       | 个          | ሻ          | ĥ     | <b>ት</b> ኁ |                                       | ሻ     | 个个   | ሻ    |
| Volume (vph)                                   | 247  | 159             | 100   | 157      | 44         | 85         | 105   | 402        | 294                                   | 366   | 738  | 109  |
| Ideal Flow (vphpl)                             | 2000   | 2000            | 2000  | 2000     | 2000       | 2000       | 2000  | 2000       | 2000                                  | 2000  | 2000 | 2000 |
| Total Lost time (s)                            | 6.0  | 6.0             | 6.0   | 6.0      | 6.0        | 6.0        | 6.6   | 6.6        |                                       | 6.6   | 6.6  | 6.6  |
| Lane Util. Factor                              | 0.97   | 1.00            | 1.00  | 0.97     | 1.00       | 1.00       | 1.00  | 0.95       |                                       | 1.00  | 0.95 | 1.00 |
| Frt  | 1.00   | 1.00            | 0.85  | 1.00     | 1.00       | 0.85       | 1.00  | 0.94       |                                       | 1.00  | 1.00 | 0.85 |
| Fit Protected                                  | 0.95   | 1.00            | 1.00  | 0.95     | 1.00       | 1.00       | 0.95  | 1.00       |                                       | 0.95  | 1.00 | 1.00 |
| Satd. Flow (prot)                              | 3614   | 1961            | 1667  | 3614     | 1961       | 1667       | 1863  | 3489       |                                       | 1863  | 3725 | 1667 |
| Flt Permitted                                  | 0.95   | 1.00            | 1.00  | 0.95     | 1.00       | 1.00       | 0.19  | 1.00       |                                       | 0.21  | 1.00 | 1.00 |
| Satd. Flow (perm)                              | 3614   | 1961            | 1667  | 3614     | 1961       | 1667       | 375   | 3489       |                                       | 410   | 3725 | 1667 |
| Peak-hour factor, PHF                          | 0.92   | 0.92            | 0.92  | 0.92     | 0.92       | 0.92       | 0.92  | 0.92       | 0.92                                  | 0.92  | 0.92 | 0.92 |
| Adj. Flow (vph)                                | 268  | 173             | 109   | 171      | 48         | 92         | 114   | 437        | 320                                   | 398   | 802  | 118  |
| RTOR Reduction (vph)                           | 0  | 0               | 93    | 0        | 0          | 84         | 0     | 145        | 0                                     | 0     | 0    | 53   |
| Lane Group Flow (vph)                          | 268  | 173             | 16    | 171      | 48         | 8          | 114   | 612        | 0                                     | 398   | 802  | 65   |
| Turn Type                                      | Prot   | <u> </u>        | Perm  | Prot     |            | Perm       | pm+pt |            |                                       | pm+pt |      | Perm |
| Protected Phases                               | 7  | 4               |       | 3        | 8          |            | 5     | 2          |                                       | 1     | 6    |      |
| Permitted Phases                               |  |                 | 4     |          |            | 8          | 2     |            |                                       | 6     |      | 6    |
| Actuated Green, G (s)                          | 14.3   | 12.8            | 12.8  | 9.3      | 7.8        | 7.8        | 27.4  | 21.5       |                                       | 46.1  | 33.6 | 33.6 |
| Effective Green, g (s)                         | 14.3   | 12.8            | 12.8  | 9.3      | 7.8        | 7.8        | 27.4  | 21.5       |                                       | 46.1  | 33.6 | 33.6 |
| Actuated g/C Ratio                             | 0.16   | 0.15            | 0.15  | 0.11     | 0.09       | 0.09       | 0.32  | 0.25       |                                       | 0.53  | 0.39 | 0.39 |
| Clearance Time (s)                             | 6.0  | 6.0             | 6.0   | 6.0      | 6.0        | 6.0        | 6.6   | 6.6        |                                       | 6.6   | 6.6  | 6.6  |
| Vehicle Extension (s)                          | 3.0  | 3.0             | 3.0   | 3.0      | 3.0        | 3.0        | 3.0   | 3.0        |                                       | 3.0   | 3.0  | 3.0  |
| Lane Grp Cap (vph)                             | 595  | 289             | 246   | 387      | 176        | 150        | 220   | 864        |                                       | 519   | 1442 | 645  |
| v/s Ratio Prot                                 | c0.07  | c0.09           |       | 0.05     | 0.02       |            | 0.04  | 0.18       |                                       | c0.16 | 0.22 |      |
| v/s Ratio Perm                                 | A, 90 - 7 T - 7 A - 6  | 0.010T.7.07.7.7 | 0.01  |          |            | 0.00       | 0.13  |            |                                       | c0.25 |      | 0.04 |
| v/c Ratio                                      | 0.45   | 0.60            | 0.07  | 0.44     | 0.27       | 0.06       | 0.52  | 0.71       |                                       | 0.77  | 0.56 | 0.10 |
| Uniform Delay, d1                              | 32.7   | 34.6            | 31.9  | 36.3     | 36.9       | 36.1       | 32.3  | 29.8       |                                       | 23.4  | 20.8 | 17.0 |
| Progression Factor                             | 1.00   | 1.00            | 1.00  | 1.00     | 1.00       | 1.00       | 1.00  | 1.00       |                                       | 1.00  | 1.00 | 1,00 |
| incremental Delay, d2                          | 0.5  | 3.3             | 0.1   | 0.8      | 0.8        | 0.2        | 2.1   | 4.9        | al le dia di educatione<br>Internetta | 6.7   | 1.6  | 0.3  |
| Delay (s)                                      | 33.2   | 37.9            | 32.0  | 37.1     | 37.7       | 36.3       | 34.4  | 34.7       |                                       | 30.1  | 22.3 | 17.3 |
| Level of Service                               | С  | D               | С     | D        | D          | D          | С     | С          |                                       | С     | С    | В    |
| Approach Delay (s)                             |  | 34.5            |       |          | 37.0       |            |       | 34.6       |                                       |       | 24.2 |      |
| Approach LOS                                   | an da da da serie da | С               |       |          | D          | ilite dia  |       | С          | * . *. 18 *. *.                       |       | С    |      |
| Intersection Summary                           |  |                 |       |          |            |            |       |            |                                       |       |      |      |
| HCM Average Control Delay                      |  |                 | 30.3  | H        | CM Level   | of Servic  | ce    |            | С                                     |       |      |      |
| HCM Volume to Capacity rate                    | tio  |                 | 0.69  |          |            |            |       |            |                                       |       |      |      |
| Actuated Cycle Length (s)                      |  |                 | 86.8  | Sı       | um of lost | time (s)   |       |            | 18.6                                  |       |      |      |
| Intersection Capacity Utilizat                 | tion   |                 | 74.8% | IC       | U Level o  | of Service | •     |            | D                                     |       |      |      |
| Analysis Period (min)<br>c Critical Lane Group |  |                 | 15    |          |            |            |       |            |                                       |       |      |      |

|                                  | ٨     |      | $\mathbf{i}$ | *                     | <b>*</b>   | Ł         | 4      | Î      | p  | 1                       | ţ     | 4     |
|----------------------------------|-------|------|--------------|-----------------------|------------|-----------|--------|--------|--|-------------------------|-------|-------|
| Movement                         | EBL   | EBT  | EBR          | WBL                   | WBT        | WBR       | NBL    | NBT    | NBR  | SBL                     | SBT   | SBR   |
| Lane Configurations              | ሻ     | 个    | ሻ            | ×,                    | ĥ          |           | ሻ      | ٩<br>٩ |  | ካ                       | 个     | *     |
| Volume (vph)                     | 158   | 169  | 267          | 194                   | 75         | 71        | 168    | 413    | 59   | 2                       | 657   | 32    |
| Ideal Flow (vphpl)               | 2000  | 2000 | 2000         | 2000                  | 2000       | 2000      | 2000   | 2000   | 2000   | 2000                    | 2000  | 2000  |
| Total Lost time (s)              | 6.1   | 6.1  | 5.9          | 6.1                   | 6.1        |           | 5.9    | 5.9    |  | 5.9                     | 5.9   | 6.1   |
| Lane Util. Factor                | 1.00  | 1.00 | 1.00         | 1.00                  | 1.00       |           | 1.00   | 1.00   |  | 1.00                    | 1.00  | 1.00  |
| Frt                              | 1.00  | 1.00 | 0.85         | 1.00                  | 0.93       |           | 1.00   | 0.98   |  | 1.00                    | 1.00  | 0.85  |
| Flt Protected                    | 0.95  | 1.00 | 1.00         | 0.95                  | 1.00       |           | 0.95   | 1.00   |  | 0.95                    | 1.00  | 1.00  |
| Satd. Flow (prot)                | 1881  | 2000 | 1619         | 1863                  | 1826       |           | 1743   | 1907   |  | 1900                    | 1980  | 1650  |
| Flt Permitted                    | 0.45  | 1.00 | 1.00         | 0.41                  | 1.00       |           | 0.10   | 1.00   |  | 0.41                    | 1.00  | 1.00  |
| Satd. Flow (perm)                | 896   | 2000 | 1619         | 812                   | 1826       |           | 175    | 1907   |  | 820                     | 1980  | 1650  |
| Peak-hour factor, PHF            | 0.81  | 0.81 | 0.81         | 0.73                  | 0.73       | 0.73      | 0.74   | 0.74   | 0.74   | 0.84                    | 0.84  | 0.84  |
| Adj. Flow (vph)                  | 195   | 209  | 330          | 266                   | 103        | 97        | 227    | 558    | 80   | 2                       | 782   | 38    |
| RTOR Reduction (vph)             | 0     | 0    | 69           | 0                     | 38         | 0         | 0      | 6      | 0  | 0                       | 0     | 16    |
| Lane Group Flow (vph)            | 195   | 209  | 261          | 266                   | 162        | 0         | 227    | 632    | 0  | 2                       | 782   | 22    |
| Heavy Vehicles (%)               | 1%    | 0%   | 5%           | 2%                    | 3%         | 0%        | 9%     | 2%     | 9%   | 0%                      | 1%    | 3%    |
| Turn Type                        | pm+pt |      | pm+ov        | pm+pt                 |            |           | pm+pt  |        |  | Perm                    |       | pm+ov |
| Protected Phases                 |       | 4    | 5            | 3                     | 8          |           | 5      | 2      |  |                         | 6     | 7     |
| Permitted Phases                 | 4     |      | 4            | 8                     |            |           | 2      |        |  | 6                       |       | 6     |
| Actuated Green, G (s)            | 21.1  | 12.3 | 21.0         | 21.3                  | 12.4       |           | 50.7   | 50.7   |  | 36.1                    | 36.1  | 44.9  |
| Effective Green, g (s)           | 21.1  | 12.3 | 21.0         | 21.3                  | 12.4       |           | 50.7   | 50.7   |  | 36.1                    | 36.1  | 44.9  |
| Actuated g/C Ratio               | 0.23  | 0.14 | 0.23         | 0.24                  | 0.14       |           | 0.56   | 0.56   |  | 0.40                    | 0.40  | 0.50  |
| Clearance Time (s)               | 6.1   | 6.1  | 5.9          | 6.1                   | 6.1        |           | 5.9    | 5.9    |  | 5.9                     | 5.9   | 6.1   |
| Vehicle Extension (s)            | 3.0   | 3.0  | 3.0          | 3.0                   | 3.0        |           | 3.0    | 3.0    | ar na 17 a mini m  | 3.0                     | 3.0   | 3.0   |
| Lane Grp Cap (vph)               | 306   | 273  | 378          | 296                   | 252        |           | 250    | 1074   |  | 329                     | 794   | 823   |
| v/s Ratio Prot                   | 0.06  | 0.10 | 0.07         | c0.09                 | 0.09       |           | c0.09  | 0.33   |  | 1949 (S. & TATEUR, M.). | c0.39 | 0.00  |
| v/s Ratio Perm                   | 0.09  |      | 0.09         | c0.12                 |            |           | 0.42   |        |  | 0.00                    |       | 0.01  |
| v/c Ratio                        | 0.64  | 0.77 | 0.69         | 0.90                  | 0.64       |           | 0.91   | 0.59   |  | 0.01                    | 0.98  | 0.03  |
| Uniform Delay, d1                | 29.5  | 37.5 | 31.5         | 31.8                  | 36.7       |           | 23.9   | 12.8   |  | 16.2                    | 26.7  | 11.5  |
| Progression Factor               | 1.00  | 1.00 | 1.00         | 1.00                  | 1.00       |           | 1.00   | 1.00   |  | 0.76                    | 0.92  | 0.40  |
| Incremental Delay, d2            | 4.3   | 12.1 | 5.4          | 27.7                  | 5.5        |           | 33.1   | 2.4    |  | 0.0                     | 28.2  | 0.0   |
| Delay (s)                        | 33.8  | 49.5 | 36.9         | 59.4                  | 42.2       |           | 57.0   | 15.2   |  | 12.4                    | 52.9  | 4.6   |
| Level of Service                 | С     | D    | D            | Е                     | D          |           | Е      | В      |  | В                       | D     | Α     |
| Approach Delay (s)               |       | 39.7 |              | erite en chrecetairie | 52.0       |           |        | 26.2   | n de la defensión de la defensi<br>La defensión de la defensión de |                         | 50.5  |       |
| Approach LOS                     |       | D    |              |                       | D          |           |        | С      |  |                         | D     |       |
| Intersection Summary             |       |      |              |                       |            |           |        |        |  |                         |       |       |
| HCM Average Control Delay        |       |      | 40.7         | H                     | CM Level   | of Servic | e      |        | D  |                         |       |       |
| HCM Volume to Capacity ratio     | )     |      | 0.87         |                       |            |           |        |        |  |                         |       |       |
| Actuated Cycle Length (s)        |       |      | 90.0         | Si                    | um of lost | time (s)  |        |        | 17.9   |                         |       |       |
| Intersection Capacity Utilizatio | n     |      | 80.4%        |                       | U Level c  |           | )<br>} |        | D  |                         |       |       |
| Analysis Period (min)            |       |      | 15           |                       |            |           |        |        |  |                         |       |       |

|                                   | ٨    |      | $\mathbf{F}$ | *     | 4          | Ł         | ٩    | Ť    | M    | \$   | ţ     | ~    |
|-----------------------------------|------|------|--------------|-------|------------|-----------|------|------|------|------|-------|------|
| Movement                          | EBL  | EBT  | EBR          | WBL   | WBT        | WBR       | NBL  | NBT  | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations               | ኻ    | ۴Î   |              | ሻ     | A .        |           | ኻ    | 4Î   |      | ኻ    | ቶ     | ก้   |
| Volume (vph)                      | 10   | 10   | 80           | 40    | 10         | 10        | 20   | 300  | 60   | 10   | 540   | 10   |
| Ideal Flow (vphpl)                | 2000 | 2000 | 2000         | 2000  | 2000       | 2000      | 2000 | 2000 | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)               | 5.8  | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8  |      | 5.8  | 5.8   | 5.8  |
| Lane Util. Factor                 | 1.00 | 1.00 |              | 1.00  | 1.00       |           | 1.00 | 1.00 |      | 1.00 | 1.00  | 1.00 |
| Frt                               | 1.00 | 0.87 |              | 1.00  | 0.92       |           | 1.00 | 0.98 |      | 1.00 | 1.00  | 0.85 |
| Flt Protected                     | 0.95 | 1.00 |              | 0.95  | 1.00       |           | 0.95 | 1.00 |      | 0.95 | 1.00  | 1.00 |
| Satd. Flow (prot)                 | 1863 | 1700 |              | 1863  | 1814       |           | 1863 | 1912 |      | 1863 | 1961  | 1667 |
| FIt Permitted                     | 0.74 | 1.00 |              | 0.69  | 1.00       |           | 0.42 | 1.00 |      | 0.53 | 1.00  | 1.00 |
| Satd. Flow (perm)                 | 1457 | 1700 |              | 1360  | 1814       |           | 828  | 1912 |      | 1041 | 1961  | 1667 |
| Peak-hour factor, PHF             | 0.92 | 0.92 | 0.92         | 0.92  | 0.92       | 0.92      | 0.92 | 0.92 | 0.92 | 0.92 | 0.92  | 0.92 |
| Adj. Flow (vph)                   | 11   | 11   | 87           | 43    | 11         | 11        | 22   | 326  | 65   | 11   | 587   | 11   |
| RTOR Reduction (vph)              | 0    | 80   | 0            | 0     | 10         | 0         | 0    | 4    | 0    | 0    | 0     | 2    |
| Lane Group Flow (vph)             | 11   | 18   | 0            | 43    | 12         | 0         | 22   | 387  | 0    | 11   | 587   | 9    |
| Turn Type                         | Perm |      |              | Perm  |            |           | Perm |      |      | Perm |       | Perm |
| Protected Phases                  |      | 4    |              |       | 8          |           |      | 2    |      |      | 6     |      |
| Permitted Phases                  | 4    |      |              | 8     |            |           | 2    |      |      | 6    |       | 6    |
| Actuated Green, G (s)             | 7.3  | 7.3  |              | 7.3   | 7.3        |           | 71.1 | 71.1 |      | 71.1 | 71.1  | 71.1 |
| Effective Green, g (s)            | 7.3  | 7.3  |              | 7.3   | 7.3        |           | 71.1 | 71.1 |      | 71.1 | 71.1  | 71.1 |
| Actuated g/C Ratio                | 0.08 | 0.08 |              | 0.08  | 0.08       |           | 0.79 | 0.79 |      | 0.79 | 0.79  | 0.79 |
| Clearance Time (s)                | 5.8  | 5.8  |              | 5.8   | 5.8        |           | 5.8  | 5.8  |      | 5.8  | 5.8   | 5.8  |
| Vehicle Extension (s)             | 3.0  | 3.0  |              | 3.0   | 3.0        |           | 3.0  | 3.0  |      | 3.0  | 3.0   | 3.0  |
| Lane Grp Cap (vph)                | 118  | 138  |              | 110   | 147        |           | 654  | 1510 |      | 822  | 1549  | 1317 |
| v/s Ratio Prot                    |      | 0.01 |              |       | 0.01       |           |      | 0,20 |      |      | c0.30 |      |
| v/s Ratio Perm                    | 0.01 |      |              | c0.03 |            |           | 0.03 |      |      | 0.01 |       | 0.01 |
| v/c Ratio                         | 0.09 | 0.13 |              | 0.39  | 0.08       |           | 0.03 | 0.26 |      | 0.01 | 0.38  | 0.01 |
| Uniform Delay, d1                 | 38.3 | 38.4 |              | 39.2  | 38.2       |           | 2.0  | 2.5  |      | 2.0  | 2.8   | 2.0  |
| Progression Factor                | 1.00 | 1.00 |              | 1.00  | 1.00       |           | 1.19 | 1.49 |      | 0.46 | 0.49  | 0.31 |
| Incremental Delay, d2             | 0.3  | 0.4  |              | 2.3   | 0.2        |           | 0.1  | 0.3  |      | 0.0  | 0.4   | 0.0  |
| Delay (s)                         | 38.6 | 38.8 |              | 41.5  | 38.5       |           | 2.5  | 4.1  |      | 0.9  | 1.8   | 0.6  |
| Level of Service                  | D    | D    |              | D     | D          |           | А    | А    |      | А    | А     | Α    |
| Approach Delay (s)                |      | 38.8 |              |       | 40.5       |           |      | 4.0  |      |      | 1.8   |      |
| Approach LOS                      |      | D    |              |       | D          |           |      | А    |      |      | А     |      |
| Intersection Summary              |      |      |              |       |            |           |      |      |      |      |       |      |
| HCM Average Control Delay         |      |      | 8.0          | H     | CM Level   | of Servic | e    |      | А    |      |       |      |
| HCM Volume to Capacity ratio      |      |      | 0.38         |       |            |           |      |      |      |      |       |      |
| Actuated Cycle Length (s)         |      |      | 90.0         |       | im of lost |           |      |      | 11.6 |      |       |      |
| Intersection Capacity Utilization | 1    |      | 45.4%        | IC    | U Level o  | f Service |      |      | Α    |      |       |      |
| Analysis Period (min)             |      |      | 15           |       |            |           |      |      |      |      |       |      |
| c Critical Lane Group             |      |      |              |       |            |           |      |      |      |      |       |      |

#### HCM Signalized Intersection Capacity Analysis 1004: Grand River & Michigan

|  |       |         | ¥           | 1     | <b>4</b>   | <b>A</b>  | ٩     | Ť    | P    | 1    | Ļ     | 4             |
|--|-------|---------|-------------|-------|------------|-----------|-------|------|------|------|-------|---------------|
| Movement   | EBL   | EBT     | EBR         | WBL   | WBT        | WBR       | NBL   | NBT  | NBR  | SBL  | SBT   | SBR           |
| Lane Configurations  | ሻ     | <u></u> |             | ሻ     | <b>ት</b> ኈ |           | ٩     | \$⊧  |      | ሻ    | ₽     |               |
| Volume (vph)   | 19    | 591     | 103         | 29    | 501        | 12        | 72    | 191  | 43   | 44   | 418   | 10            |
| Ideal Flow (vphpl)   | 2000  | 2000    | 2000        | 2000  | 2000       | 2000      | 2000  | 2000 | 2000 | 2000 | 2000  | 2000          |
| Total Lost time (s)  | 6.0   | 6.0     |             | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |               |
| Lane Util. Factor  | 1.00  | 0.95    |             | 1.00  | 0.95       |           | 1.00  | 1.00 |      | 1.00 | 1.00  |               |
| Frt  | 1.00  | 0.98    |             | 1.00  | 1.00       |           | 1.00  | 0.97 |      | 1.00 | 1.00  |               |
| Flt Protected  | 0.95  | 1.00    |             | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |               |
| Satd. Flow (prot)  | 1863  | 3643    |             | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |               |
| Flt Permitted  | 0.95  | 1.00    |             | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |               |
| Satd. Flow (perm)  | 1863  | 3643    |             | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |               |
| Peak-hour factor, PHF                                      | 0.79  | 0.79    | 0.79        | 0.70  | 0.70       | 0.70      | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81          |
| Adj. Flow (vph)  | 24    | 748     | 130         | 41    | 716        | 17        | 76    | 201  | 45   | 54   | 516   | 12            |
| RTOR Reduction (vph)                                       | 0     | 14      | 0           | 0     | 1          | 0         | 0     | 9    | 0    | 0    | 1     | 0             |
| Lane Group Flow (vph)                                      | 24    | 864     | 0           | 41    | 732        | 0         | 76    | 237  | 0    | 54   | 527   | 0             |
| Turn Type  | Prot  |         |             | Prot  |            |           | Prot  |      |      | Prot |       |               |
| Protected Phases   | 5     | 2       |             | 1     | 6          |           | 3     | 8    |      | 7    | 4     |               |
| Permitted Phases   |       |         |             |       |            |           |       |      |      |      |       |               |
| Actuated Green, G (s)                                      | 2.8   | 29.1    |             | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |               |
| Effective Green, g (s)                                     | 2.8   | 29.1    |             | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |               |
| Actuated g/C Ratio   | 0.03  | 0.32    |             | 0.05  | 0.34       |           | 0.06  | 0.30 |      | 0.06 | 0.30  |               |
| Clearance Time (s)   | 6.0   | 6.0     |             | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |               |
| Vehicle Extension (s)                                      | 3.0   | 3.0     |             | 3.0   | 3.0        |           | 3.0   | 3.0  |      | 3.0  | 3.0   |               |
| Lane Grp Cap (vph)   | 58    | 1178    |             | 87    | 1258       |           | 116   | 574  |      | 116  | 588   |               |
| v/s Ratio Prot   | 0.01  | c0.24   |             | c0.02 | 0.20       |           | c0.04 | 0.12 |      | 0.03 | c0.27 |               |
| v/s Ratio Perm   |       |         |             |       |            |           |       |      |      |      |       |               |
| v/c Ratio  | 0.41  | 0.73    |             | 0.47  | 0.58       |           | 0.66  | 0.41 |      | 0.47 | 0.90  |               |
| Uniform Delay, d1  | 42.8  | 27.0    |             | 41.8  | 24.5       |           | 41.3  | 25.1 |      | 40.8 | 30.1  |               |
| Progression Factor   | 1.00  | 1.00    |             | 1.08  | 1.20       |           | 0.82  | 0.84 |      | 1.00 | 1.00  |               |
| Incremental Delay, d2                                      | 4.7   | 4.1     |             | 3.4   | 1.7        |           | 12.4  | 0.5  |      | 2.9  | 16.2  |               |
| Delay (s)  | 47.5  | 31.1    |             | 48.7  | 31.0       |           | 46.1  | 21.5 |      | 43.7 | 46.3  |               |
| Level of Service   | D     | С       |             | D     | С          |           | D     | С    |      | D    | D     |               |
| Approach Delay (s)   |       | 31.5    |             |       | 32.0       |           |       | 27.3 |      |      | 46.1  |               |
| Approach LOS   |       | С       |             |       | С          |           |       | С    |      |      | D     |               |
| Intersection Summary                                       |       |         |             |       |            |           |       |      |      |      |       |               |
| HCM Average Control Delay                                  |       |         | 34.4        | H     | CM Level   | of Servic | e     |      | С    |      |       |               |
| HCM Volume to Capacity ratio                               |       |         | 0.78        |       |            |           |       |      |      |      |       |               |
| Actuated Cycle Length (s)                                  |       |         | 90.0        |       | um of lost |           |       |      | 24.0 |      |       | na Frank Stra |
| Intersection Capacity Utilization<br>Analysis Period (min) | 1.560 |         | 65.2%<br>15 | IC    | U Level c  | t Service |       |      | C    |      |       |               |
| c Critical Lane Group                                      |       |         |             |       |            |           |       |      |      |      |       |               |

#### HCM Signalized Intersection Capacity Analysis 1004: Grand River & Michigan

|  |       |         | ¥           | 1     | <b>4</b>   | <b>A</b>  | ٩     | Ť    | P    | 1    | Ļ     | 4             |
|--|-------|---------|-------------|-------|------------|-----------|-------|------|------|------|-------|---------------|
| Movement   | EBL   | EBT     | EBR         | WBL   | WBT        | WBR       | NBL   | NBT  | NBR  | SBL  | SBT   | SBR           |
| Lane Configurations  | ሻ     | <u></u> |             | ሻ     | <b>ት</b> ኈ |           | ٩     | \$⊧  |      | ሻ    | ₽     |               |
| Volume (vph)   | 19    | 591     | 103         | 29    | 501        | 12        | 72    | 191  | 43   | 44   | 418   | 10            |
| Ideal Flow (vphpl)   | 2000  | 2000    | 2000        | 2000  | 2000       | 2000      | 2000  | 2000 | 2000 | 2000 | 2000  | 2000          |
| Total Lost time (s)  | 6.0   | 6.0     |             | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |               |
| Lane Util. Factor  | 1.00  | 0.95    |             | 1.00  | 0.95       |           | 1.00  | 1.00 |      | 1.00 | 1.00  |               |
| Frt  | 1.00  | 0.98    |             | 1.00  | 1.00       |           | 1.00  | 0.97 |      | 1.00 | 1.00  |               |
| Flt Protected  | 0.95  | 1.00    |             | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |               |
| Satd. Flow (prot)  | 1863  | 3643    |             | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |               |
| Flt Permitted  | 0.95  | 1.00    |             | 0.95  | 1.00       |           | 0.95  | 1.00 |      | 0.95 | 1.00  |               |
| Satd. Flow (perm)  | 1863  | 3643    |             | 1863  | 3713       |           | 1863  | 1907 |      | 1863 | 1954  |               |
| Peak-hour factor, PHF                                      | 0.79  | 0.79    | 0.79        | 0.70  | 0.70       | 0.70      | 0.95  | 0.95 | 0.95 | 0.81 | 0.81  | 0.81          |
| Adj. Flow (vph)  | 24    | 748     | 130         | 41    | 716        | 17        | 76    | 201  | 45   | 54   | 516   | 12            |
| RTOR Reduction (vph)                                       | 0     | 14      | 0           | 0     | 1          | 0         | 0     | 9    | 0    | 0    | 1     | 0             |
| Lane Group Flow (vph)                                      | 24    | 864     | 0           | 41    | 732        | 0         | 76    | 237  | 0    | 54   | 527   | 0             |
| Turn Type  | Prot  |         |             | Prot  |            |           | Prot  |      |      | Prot |       |               |
| Protected Phases   | 5     | 2       |             | 1     | 6          |           | 3     | 8    |      | 7    | 4     |               |
| Permitted Phases   |       |         |             |       |            |           |       |      |      |      |       |               |
| Actuated Green, G (s)                                      | 2.8   | 29.1    |             | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |               |
| Effective Green, g (s)                                     | 2.8   | 29.1    |             | 4.2   | 30.5       |           | 5.6   | 27.1 |      | 5.6  | 27.1  |               |
| Actuated g/C Ratio   | 0.03  | 0.32    |             | 0.05  | 0.34       |           | 0.06  | 0.30 |      | 0.06 | 0.30  |               |
| Clearance Time (s)   | 6.0   | 6.0     |             | 6.0   | 6.0        |           | 6.0   | 6.0  |      | 6.0  | 6.0   |               |
| Vehicle Extension (s)                                      | 3.0   | 3.0     |             | 3.0   | 3.0        |           | 3.0   | 3.0  |      | 3.0  | 3.0   |               |
| Lane Grp Cap (vph)   | 58    | 1178    |             | 87    | 1258       |           | 116   | 574  |      | 116  | 588   |               |
| v/s Ratio Prot   | 0.01  | c0.24   |             | c0.02 | 0.20       |           | c0.04 | 0.12 |      | 0.03 | c0.27 |               |
| v/s Ratio Perm   |       |         |             |       |            |           |       |      |      |      |       |               |
| v/c Ratio  | 0.41  | 0.73    |             | 0.47  | 0.58       |           | 0.66  | 0.41 |      | 0.47 | 0.90  |               |
| Uniform Delay, d1  | 42.8  | 27.0    |             | 41.8  | 24.5       |           | 41.3  | 25.1 |      | 40.8 | 30.1  |               |
| Progression Factor   | 1.00  | 1.00    |             | 1.08  | 1.20       |           | 0.82  | 0.84 |      | 1.00 | 1.00  |               |
| Incremental Delay, d2                                      | 4.7   | 4.1     |             | 3.4   | 1.7        |           | 12.4  | 0.5  |      | 2.9  | 16.2  |               |
| Delay (s)  | 47.5  | 31.1    |             | 48.7  | 31.0       |           | 46.1  | 21.5 |      | 43.7 | 46.3  |               |
| Level of Service   | D     | С       |             | D     | С          |           | D     | С    |      | D    | D     |               |
| Approach Delay (s)   |       | 31.5    |             |       | 32.0       |           |       | 27.3 |      |      | 46.1  |               |
| Approach LOS   |       | С       |             |       | С          |           |       | С    |      |      | D     |               |
| Intersection Summary                                       |       |         |             |       |            |           |       |      |      |      |       |               |
| HCM Average Control Delay                                  |       |         | 34.4        | H     | CM Level   | of Servic | e     |      | С    |      |       |               |
| HCM Volume to Capacity ratio                               |       |         | 0.78        |       |            |           |       |      |      |      |       |               |
| Actuated Cycle Length (s)                                  |       |         | 90.0        |       | um of lost |           |       |      | 24.0 |      |       | na Frank Stra |
| Intersection Capacity Utilization<br>Analysis Period (min) | 1.560 |         | 65.2%<br>15 | IC    | U Level c  | t Service |       |      | C    |      |       |               |
| c Critical Lane Group                                      |       |         |             |       |            |           |       |      |      |      |       |               |

|                                  | ٨    | <b>\$</b> | $\mathbf{i}$ | ¥     | - <b>@</b> | Ł          | ٩    | Å    | p     | \$    | ¥    | ~    |
|----------------------------------|------|-----------|--------------|-------|------------|------------|------|------|-------|-------|------|------|
| Movement                         | EBL  | EBT       | EBR          | WBL   | WBT        | WBR        | NBL  | NBT  | NBR   | SBL   | SBT  | SBF  |
| Lane Configurations              | ሻ    | 朴ኈ        |              | ĥ     | ŕ          | ሻ          | ሻ    | Å    | ሻ     | ٢     | \$⇒  |      |
| Volume (vph)                     | 4    | 612       | 161          | 203   | 642        | 116        | 53   | 21   | 217   | 182   | 41   | 10   |
| Ideal Flow (vphpl)               | 2000 | 2000      | 2000         | 2000  | 2000       | 2000       | 2000 | 2000 | 2000  | 2000  | 2000 | 2000 |
| Lane Width                       | 12   | 12        | 12           | 12    | 12         | 12         | 11   | 11   | 11    | 12    | 12   | 12   |
| Total Lost time (s)              | 6.1  | 6.1       |              | 6.1   | 6.1        | 6.1        | 6.0  | 6.0  | 6.0   | 6.0   | 6.0  |      |
| Lane Util. Factor                | 1.00 | 0.95      |              | 1.00  | 1.00       | 1.00       | 1.00 | 1.00 | 1.00  | 1.00  | 1.00 |      |
| Frt                              | 1.00 | 0.97      |              | 1.00  | 1.00       | 0.85       | 1.00 | 1.00 | 0.85  | 1.00  | 0.97 |      |
| Flt Protected                    | 0.95 | 1.00      |              | 0.95  | 1.00       | 1.00       | 0.95 | 1.00 | 1.00  | 0.95  | 1.00 |      |
| Satd. Flow (prot)                | 1863 | 3609      |              | 1863  | 1961       | 1500       | 1801 | 1895 | 1611  | 1863  | 1905 |      |
| Flt Permitted                    | 0.25 | 1.00      |              | 0.11  | 1.00       | 1.00       | 0.71 | 1.00 | 1.00  | 0.56  | 1.00 |      |
| Satd. Flow (perm)                | 483  | 3609      |              | 220   | 1961       | 1500       | 1351 | 1895 | 1611  | 1099  | 1905 |      |
| Peak-hour factor, PHF            | 0.76 | 0.76      | 0.76         | 0.83  | 0.83       | 0.83       | 0.83 | 0.83 | 0.83  | 0.75  | 0.75 | 0.75 |
| Adj. Flow (vph)                  | 5    | 805       | 212          | 245   | 773        | 140        | 64   | 25   | 261   | 243   | 55   | 13   |
| RTOR Reduction (vph)             | 0    | 25        | 0            | 0     | 0          | 68         | 0    | 0    | 0     | 0     | 8    | 0    |
| Lane Group Flow (vph)            | 5    | 992       | 0            | 245   | 773        | 72         | 64   | 25   | 261   | 243   | 60   | 0    |
| Parking (#/hr)                   |      |           | 0            |       |            | 0          |      |      |       |       |      |      |
| Turn Type                        | Perm |           |              | pm+pt |            | Perm       | Perm |      | Perm  | pm+pt |      |      |
| Protected Phases                 |      | 2         |              | ो 1   | 6          |            |      | 8    |       | 7     | 4    |      |
| Permitted Phases                 | 2    |           |              | 6     |            | 6          | 8    |      | 8     | 4     |      |      |
| Actuated Green, G (s)            | 29.5 | 29.5      |              | 46.3  | 46.3       | 46.3       | 18.6 | 18.6 | 18.6  | 31.6  | 31.6 |      |
| Effective Green, g (s)           | 29.5 | 29.5      |              | 46.3  | 46.3       | 46.3       | 18.6 | 18.6 | 18.6  | 31.6  | 31.6 |      |
| Actuated g/C Ratio               | 0.33 | 0.33      |              | 0.51  | 0.51       | 0.51       | 0.21 | 0.21 | 0.21  | 0.35  | 0.35 |      |
| Clearance Time (s)               | 6.1  | 6.1       |              | 6.1   | 6.1        | 6.1        | 6.0  | 6.0  | 6.0   | 6.0   | 6.0  |      |
| Vehicle Extension (s)            | 3.0  | 3.0       |              | 3.0   | 3.0        | 3.0        | 3.0  | 3.0  | 3.0   | 3.0   | 3.0  |      |
| Lane Grp Cap (vph)               | 158  | 1183      |              | 309   | 1009       | 772        | 279  | 392  | 333   | 445   | 669  |      |
| v/s Ratio Prot                   |      | 0.27      |              | 0.09  | c0.39      |            |      | 0.01 |       | c0.04 | 0.03 |      |
| v/s Ratio Perm                   | 0.01 |           |              | c0.31 |            | 0.05       | 0.05 |      | c0.16 | 0.15  |      |      |
| v/c Ratio                        | 0.03 | 0.84      |              | 0.79  | 0.77       | 0.09       | 0.23 | 0.06 | 0.78  | 0.55  | 0.09 |      |
| Uniform Delay, d1                | 20.5 | 28.0      |              | 19.5  | 17.5       | 11.1       | 29.7 | 28.7 | 33.8  | 23.0  | 19.6 |      |
| Progression Factor               | 1.20 | 0.96      |              | 1.00  | 1.00       | 1.00       | 1.00 | 1.00 | 1.00  | 1.00  | 1.00 |      |
| Incremental Delay, d2            | 0.4  | 6.8       |              | 13.0  | 5.6        | 0.2        | 0.4  | 0.1  | 11.4  | 1.4   | 0.1  |      |
| Delay (s)                        | 25.1 | 33.9      |              | 32.5  | 23.1       | 11.4       | 30.2 | 28.8 | 45.2  | 24.4  | 19.6 |      |
| Level of Service                 | С    | С         |              | С     | С          | В          | С    | С    | D     | С     | В    |      |
| Approach Delay (s)               |      | 33.8      |              |       | 23.7       |            |      | 41.3 |       |       | 23.3 |      |
| Approach LOS                     |      | С         |              |       | С          |            |      | D    |       |       | С    |      |
| Intersection Summary             |      |           |              |       |            |            |      |      |       |       |      |      |
| HCM Average Control Delay        |      |           | 29.5         | Н     | CM Level   | of Servic  | е    |      | С     |       |      |      |
| HCM Volume to Capacity ratio     |      |           | 0.78         |       |            |            |      |      |       |       |      |      |
| Actuated Cycle Length (s)        |      |           | 90.0         |       | um of lost |            |      |      | 18.1  |       |      |      |
| ntersection Capacity Utilization |      |           | 71.8%        | IC    | U Level o  | of Service |      |      | С     |       |      |      |
| Analysis Period (min)            |      |           | 15           |       |            |            |      |      |       |       |      |      |
| c Critical Lane Group            |      |           |              |       |            |            |      |      |       |       |      |      |

|                               | ٨     |      | Ý     | *    | 4       | Ł          | ٩     | Î    | p    | \$    | ļ     | -    |
|-------------------------------|-------|------|-------|------|---------|------------|-------|------|------|-------|-------|------|
| Movement                      | EBL   | EBT  | EBR   | WBL  | WBT     | WBR        | NBL   | NBT  | NBR  | SBL   | SBT   | SBR  |
| Lane Configurations           | ሻሻ    | ቶ    | ř     | ኻኻ   | ŕ       | 7          | ሻ     | 个诤   |      | ሻ     | 个个    | ŕ    |
| Volume (vph)                  | 621   | 151  | 329   | 477  | 146     | 294        | 75    | 404  | 140  | 162   | 600   | 132  |
| Ideal Flow (vphpl)            | 2000  | 2000 | 2000  | 2000 | 2000    | 2000       | 2000  | 2000 | 2000 | 2000  | 2000  | 2000 |
| Total Lost time (s)           | 6.0   | 6.0  | 6.0   | 6.0  | 6.0     | 6.6        | 6.6   | 6.6  |      | 6.6   | 6.6   | 6.6  |
| Lane Util. Factor             | 0.97  | 1.00 | 1.00  | 0.97 | 1.00    | 1.00       | 1.00  | 0.95 |      | 1.00  | 0.95  | 1.00 |
| Frt                           | 1.00  | 1.00 | 0.85  | 1.00 | 1.00    | 0.85       | 1.00  | 0.96 |      | 1.00  | 1.00  | 0.85 |
| Fit Protected                 | 0.95  | 1.00 | 1.00  | 0.95 | 1.00    | 1.00       | 0.95  | 1.00 |      | 0.95  | 1.00  | 1.00 |
| Satd. Flow (prot)             | 3614  | 1961 | 1667  | 3614 | 1961    | 1667       | 1863  | 3582 |      | 1863  | 3725  | 1667 |
| Flt Permitted                 | 0.95  | 1.00 | 1.00  | 0.95 | 1.00    | 1.00       | 0.23  | 1.00 |      | 0.29  | 1.00  | 1.00 |
| Satd. Flow (perm)             | 3614  | 1961 | 1667  | 3614 | 1961    | 1667       | 453   | 3582 |      | 573   | 3725  | 1667 |
| Peak-hour factor, PHF         | 0.92  | 0.92 | 0.92  | 0.92 | 0.92    | 0.92       | 0.92  | 0.92 | 0.92 | 0.92  | 0.92  | 0.92 |
| Adj. Flow (vph)               | 675   | 164  | 358   | 518  | 159     | 320        | 82    | 439  | 152  | 176   | 652   | 143  |
| RTOR Reduction (vph)          | 0     | 0    | 178   | 0    | 0       | 22         | 0     | 37   | 0    | 0     | 0     | 77   |
| Lane Group Flow (vph)         | 675   | 164  | 180   | 518  | 159     | 298        | 82    | 554  | 0    | 176   | 652   | 66   |
| Turn Type                     | Prot  |      | Perm  | Prot |         | pm+ov      | pm+pt |      |      | pm+pt |       | Perm |
| Protected Phases              | 7     | 4    |       | 3    | 8       | 1          | 5     | 2    |      | 1     | 6     |      |
| Permitted Phases              |       |      | 4     |      |         | 8          | 2     |      |      | 6     |       | 6    |
| Actuated Green, G (s)         | 16.4  | 14.6 | 14.6  | 14.1 | 12.3    | 21.2       | 23.4  | 17.5 |      | 29.4  | 20.5  | 20.5 |
| Effective Green, g (s)        | 16.4  | 14.6 | 14.6  | 14.1 | 12.3    | 21.2       | 23.4  | 17.5 |      | 29.4  | 20.5  | 20.5 |
| Actuated g/C Ratio            | 0.20  | 0.18 | 0.18  | 0.18 | 0.15    | 0.26       | 0.29  | 0.22 |      | 0.37  | 0.26  | 0.26 |
| Clearance Time (s)            | 6.0   | 6.0  | 6.0   | 6.0  | 6.0     | 6.6        | 6.6   | 6.6  |      | 6.6   | 6.6   | 6.6  |
| Vehicle Extension (s)         | 3.0   | 3.0  | 3.0   | 3.0  | 3.0     | 3.0        | 3.0   | 3.0  |      | 3.0   | 3.0   | 3.0  |
| Lane Grp Cap (vph)            | 738   | 357  | 303   | 635  | 300     | 577        | 236   | 781  |      | 353   | 951   | 426  |
| v/s Ratio Prot                | c0.19 | 0.08 |       | 0.14 | 0.08    | c0.06      | 0.03  | 0.15 |      | 0.06  | c0.18 |      |
| v/s Ratio Perm                |       |      | c0.11 |      |         | 0.12       | 0.08  |      |      | 0.13  |       | 0.04 |
| v/c Ratio                     | 0.91  | 0.46 | 0.60  | 0.82 | 0.53    | 0.52       | 0.35  | 0.71 |      | 0.50  | 0.69  | 0.16 |
| Uniform Delay, d1             | 31.3  | 29.3 | 30.1  | 31.9 | 31.3    | 25.2       | 28.8  | 29.0 |      | 25.6  | 27.0  | 23.2 |
| Progression Factor            | 1.00  | 1.00 | 1.00  | 1.00 | 1.00    | 1.00       | 1.00  | 1.00 |      | 1.00  | 1.00  | 1.00 |
| Incremental Delay, d2         | 15.8  | 0.9  | 3.1   | 8.0  | 1.8     | 0.8        | 0.9   | 5.4  |      | 1.1   | 4.0   | 0.8  |
| Delay (s)                     | 47.1  | 30.3 | 33.3  | 39.8 | 33.1    | 26.0       | 29.7  | 34.5 |      | 26.7  | 31.0  | 24.0 |
| Level of Service              | D     | С    | С     | D    | С       | С          | С     | С    |      | С     | С     | С    |
| Approach Delay (s)            |       | 40.7 |       |      | 34.3    |            |       | 33.9 |      |       | 29.2  |      |
| Approach LOS                  |       | D    |       |      | С       |            |       | С    |      |       | С     |      |
| Intersection Summary          |       |      |       |      |         |            |       |      |      |       |       |      |
| HCM Average Control Dela      |       |      | 34.9  | H    | CM Leve | l of Servi | ce    |      | С    |       |       |      |
| HCM Volume to Capacity ra     | atio  |      | 0.73  |      |         |            |       |      |      |       |       |      |
| Actuated Cycle Length (s)     |       |      | 80.3  |      |         | t time (s) |       |      | 19.2 |       |       |      |
| Intersection Capacity Utiliza | ation |      | 69.5% | IC   | U Level | of Service | Э     |      | С    |       |       |      |
| Analysis Period (min)         |       |      | 15    |      |         |            |       |      |      |       |       |      |
| c Critical Lane Group         |       |      |       |      |         |            |       |      |      |       |       |      |

|                                   | ≯     |      | $\mathbf{i}$ | 1     | <b>4</b>   | Ł                     | 1                   | Î     | p                       | \$                     | ţ                     | 1             |
|-----------------------------------|-------|------|--------------|-------|------------|-----------------------|---------------------|-------|-------------------------|------------------------|-----------------------|---------------|
| Movement                          | EBL   | EBT  | EBR          | WBL   | WBT        | WBR                   | NBL                 | NBT   | NBR                     | SBL                    | SBT                   | SBR           |
| Lane Configurations               | ĥ     | 个    | <u>۴</u>     | ሻ     | \$         |                       | ሻ                   | 4     |                         | ሻ                      | 个                     | <del>آم</del> |
| Volume (vph)                      | 110   | 158  | 288          | 169   | 268        | 4                     | 323                 | 773   | 77                      | ંડ                     | 434                   | 144           |
| Ideal Flow (vphpl)                | 2000  | 2000 | 2000         | 2000  | 2000       | 2000                  | 2000                | 2000  | 2000                    | 2000                   | 2000                  | 2000          |
| Total Lost time (s)               | 6.1   | 6.1  | 5.9          | 6.1   | 6.1        |                       | 5.9                 | 5.9   |                         | 5.9                    | 5.9                   | 6.1           |
| Lane Util. Factor                 | 1.00  | 1.00 | 1.00         | 1.00  | 1.00       |                       | 1.00                | 1.00  |                         | 1.00                   | 1.00                  | 1.00          |
| Frt                               | 1.00  | 1.00 | 0.85         | 1.00  | 1.00       |                       | 1.00                | 0.99  |                         | 1.00                   | 1.00                  | 0.85          |
| Flt Protected                     | 0.95  | 1.00 | 1.00         | 0.95  | 1.00       |                       | 0.95                | 1.00  |                         | 0.95                   | 1.00                  | 1.00          |
| Satd. Flow (prot)                 | 1881  | 2000 | 1619         | 1863  | 1938       |                       | 1743                | 1922  |                         | 1900                   | 1980                  | 1650          |
| Flt Permitted                     | 0.23  | 1.00 | 1.00         | 0.55  | 1.00       |                       | 0.29                | 1.00  |                         | 0.14                   | 1.00                  | 1.00          |
| Satd. Flow (perm)                 | 454   | 2000 | 1619         | 1086  | 1938       |                       | 524                 | 1922  |                         | 277                    | 1980                  | 1650          |
| Peak-hour factor, PHF             | 0.83  | 0.83 | 0.83         | 0.80  | 0.80       | 0.80                  | 0.90                | 0.90  | 0.90                    | 0.95                   | 0.95                  | 0.95          |
| Adj. Flow (vph)                   | 133   | 190  | 347          | 211   | 335        | 5                     | 359                 | 859   | 86                      | 3                      | 457                   | 152           |
| RTOR Reduction (vph)              | 0     | 0    | 121          | 0     | 1          | 0                     | 0                   | 4     | 0                       | 0                      | 0                     | 87            |
| Lane Group Flow (vph)             | 133   | 190  | 226          | 211   | 339        | 0                     | 359                 | 941   | 0                       | 3                      | 457                   | 65            |
| Heavy Vehicles (%)                | 1%    | 0%   | 5%           | 2%    | 3%         | 0%                    | 9%                  | 2%    | 9%                      | 0%                     | 1%                    | 3%            |
| Turn Type                         | pm+pt |      | pm+ov        | pm+pt |            |                       | pm+pt               |       |                         | Perm                   |                       | pm+ov         |
| Protected Phases                  | 7     | 4    | 5            | 3     | 8          |                       | 5                   | 2     | Ate e adolf a Ate arit, | hangina ayaa ee        | 6                     | 7             |
| Permitted Phases                  | 4     |      | 4            | 8     |            |                       | 2                   |       |                         | 6                      |                       | 6             |
| Actuated Green, G (s)             | 25.0  | 18.1 | 30.2         | 25.0  | 18.1       |                       | 46.9                | 46.9  |                         | 28.9                   | 28.9                  | 35.8          |
| Effective Green, g (s)            | 25.0  | 18.1 | 30.2         | 25.0  | 18.1       |                       | 46.9                | 46.9  |                         | 28.9                   | 28.9                  | 35.8          |
| Actuated g/C Ratio                | 0.28  | 0.20 | 0.34         | 0.28  | 0.20       |                       | 0.52                | 0.52  |                         | 0.32                   | 0.32                  | 0.40          |
| Clearance Time (s)                | 6.1   | 6.1  | 5.9          | 6.1   | 6.1        |                       | 5.9                 | 5.9   |                         | 5.9                    | 5.9                   | 6.1           |
| Vehicle Extension (s)             | 3.0   | 3.0  | 3.0          | 3.0   | 3.0        | ah filika ana di sana | 3.0                 | 3.0   |                         | 3.0                    | 3.0                   | 3.0           |
| Lane Grp Cap (vph)                | 236   | 402  | 543          | 361   | 390        |                       | 437                 | 1002  |                         | 89                     | 636                   | 656           |
| v/s Ratio Prot                    | 0.04  | 0.10 | 0.06         | c0.04 | c0.17      |                       | 0.11                | c0.49 |                         | 2011 - 2013 - 2014<br> | 0.23                  | 0.01          |
| v/s Ratio Perm                    | 0.11  |      | 0.08         | 0.12  |            |                       | 0.32                |       |                         | 0.01                   |                       | 0.03          |
| v/c Ratio                         | 0.56  | 0.47 | 0.42         | 0.58  | 0.87       |                       | 0.82                | 0.94  |                         | 0.03                   | 0.72                  | 0.10          |
| Uniform Delay, d1                 | 26.0  | 31.7 | 23.1         | 26.9  | 34.8       |                       | 26.3                | 20.2  |                         | 21.0                   | 27.0                  | 17.0          |
| Progression Factor                | 1.00  | 1.00 | 1.00         | 1.00  | 1.00       |                       | 1.00                | 1.00  |                         | 1.10                   | 1.11                  | 1.63          |
| Incremental Delay, d2             | 3.1   | 0.9  | 0.5          | 2.4   | 18.2       |                       | 11.8                | 17.1  |                         | 0.7                    | 6.7                   | 0.1           |
| Delay (s)                         | 29.0  | 32.6 | 23.6         | 29.3  | 53.0       |                       | 38.0                | 37.3  |                         | 23.7                   | 36.6                  | 27.8          |
| Level of Service                  | С     | С    | С            | С     | D          |                       | D                   | D     |                         | С                      | D                     | С             |
| Approach Delay (s)                |       | 27.2 |              |       | 44.0       |                       | с                   | 37.5  |                         |                        | 34.3                  |               |
| Approach LOS                      |       | С    |              |       | D          |                       |                     | D     |                         |                        | С                     |               |
| Intersection Summary              |       |      |              |       |            |                       |                     |       |                         |                        |                       |               |
| HCM Average Control Delay         |       |      | 35.8         | H     | CM Level   | of Servic             | e                   |       | D                       |                        |                       |               |
| HCM Volume to Capacity ratio      |       |      | 0.89         |       |            |                       |                     |       |                         |                        |                       |               |
| Actuated Cycle Length (s)         |       |      | 90.0         | Sı    | um of lost | time (s)              |                     |       | 18.1                    |                        |                       |               |
| Intersection Capacity Utilization | 1     |      | 90.9%        |       | U Level o  |                       | • • • • • • • • • • | ·     | E                       |                        | an en ar e traine e e |               |
| Analysis Period (min)             |       |      | 15           |       |            |                       |                     |       |                         |                        |                       |               |

|                                   | <u>_</u>       | >          | >          | 1  | <b></b>    |           | ٩       | Î     | Þ                    | 1    | Ť    | 4   |
|-----------------------------------|----------------|------------|------------|--|------------|-----------|---------|-------|----------------------|------|------|---|
| Movement                          | EBL            | EBT        | EBR        | WBL                                      | WBT        | WBR       | NBL     | NBT   | NBR                  | SBL  | SBT  | SBR   |
| Lane Configurations               | ሻ              | <b>ቶ</b> ₽ |            | ኻ  | <b>ቶ</b> ጮ |           | ۳.<br>۲ | \$≽   |                      | ሻ    | ĥ    |   |
| Volume (vph)                      | 52             | 586        | 91         | 66                                       | 656        | 104       | 105     | 405   | 37                   | 68   | 345  | 18  |
| Ideal Flow (vphpl)                | 2000           | 2000       | 2000       | 2000                                     | 2000       | 2000      | 2000    | 2000  | 2000                 | 2000 | 2000 | 2000  |
| Total Lost time (s)               | 6.0            | 6.0        |            | 6.0                                      | 6.0        |           | 6.0     | 6.0   |                      | 6.0  | 6.0  |   |
| Lane Util. Factor                 | 1.00           | 0.95       |            | 1.00                                     | 0.95       |           | 1.00    | 1.00  |                      | 1.00 | 1.00 |   |
| Frt                               | 1.00           | 0.98       |            | 1.00                                     | 0.98       |           | 1.00    | 0.99  |                      | 1.00 | 0.99 |   |
| Flt Protected                     | 0.95           | 1.00       |            | 0.95                                     | 1.00       |           | 0.95    | 1.00  |                      | 0.95 | 1.00 |   |
| Satd. Flow (prot)                 | 1863           | 3650       |            | 1863                                     | 3649       |           | 1863    | 1936  |                      | 1863 | 1946 |   |
| Flt Permitted                     | 0.95           | 1.00       |            | 0.95                                     | 1.00       |           | 0.95    | 1.00  |                      | 0.95 | 1.00 |   |
| Satd. Flow (perm)                 | 1863           | 3650       |            | 1863                                     | 3649       |           | 1863    | 1936  |                      | 1863 | 1946 |   |
| Peak-hour factor, PHF             | 0.90           | 0.90       | 0.90       | 0.92                                     | 0.92       | 0.92      | 0.89    | 0.89  | 0.89                 | 0.90 | 0.90 | 0.90  |
| Adj. Flow (vph)                   | 58             | 651        | 101        | 72                                       | 713        | 113       | 118     | 455   | 42                   | 76   | 383  | 20  |
| RTOR Reduction (vph)              | 0              | 13         | 0          | 0  | 13         | 0         | 0       | 3     | 0                    | 0    | 2    | 0   |
| Lane Group Flow (vph)             | 58             | 739        | 0          | 72                                       | 813        | 0         | 118     | 494   | 0                    | 76   | 401  | 0   |
| Turn Type                         | Prot           |            |            | Prot                                     |            |           | Prot    |       |                      | Prot |      |   |
| Protected Phases                  | 5              | 2          |            | 1  | 6          |           | 3       | 8     |                      | 7    | 4    |   |
| Permitted Phases                  |                |            |            |  |            |           |         |       |                      |      |      |   |
| Actuated Green, G (s)             | 5.6            | 25.2       |            | 5.7                                      | 25.3       |           | 9.9     | 27.5  |                      | 7.6  | 25.2 |   |
| Effective Green, g (s)            | 5.6            | 25.2       |            | 5.7                                      | 25.3       |           | 9.9     | 27.5  |                      | 7.6  | 25.2 |   |
| Actuated g/C Ratio                | 0.06           | 0.28       |            | 0.06                                     | 0.28       |           | 0.11    | 0.31  |                      | 0.08 | 0.28 |   |
| Clearance Time (s)                | 6.0            | 6.0        |            | 6.0                                      | 6.0        |           | 6.0     | 6.0   |                      | 6.0  | 6.0  |   |
| Vehicle Extension (s)             | 3.0            | 3.0        |            | 3.0                                      | 3.0        |           | 3.0     | 3.0   |                      | 3.0  | 3.0  |   |
| Lane Grp Cap (vph)                | 116            | 1022       |            | 118                                      | 1026       |           | 205     | 592   |                      | 157  | 545  |   |
| v/s Ratio Prot                    | 0.03           | 0.20       |            | c0.04                                    | c0.22      |           | c0.06   | c0.25 |                      | 0.04 | 0.21 |   |
| v/s Ratio Perm                    |                |            |            |  |            |           |         |       |                      |      |      |   |
| v/c Ratio                         | 0.50           | 0.72       |            | 0.61                                     | 0.79       |           | 0.58    | 0.83  |                      | 0.48 | 0.74 |   |
| Uniform Delay, d1                 | 40.8           | 29.3       | 14 - A - A | 41.1                                     | 29.9       |           | 38.1    | 29.1  |                      | 39.3 | 29.4 |   |
| Progression Factor                | 1.00           | 1.00       |            | 1.10                                     | 1.11       |           | 1.33    | 0.64  |                      | 1.00 | 1.00 |   |
| incremental Delay, d2             | 3.4            | 4.4        |            | 6.8                                      | 4.8        |           | 3.7     | 9.4   |                      | 2.3  | 5.1  |   |
| Delay (s)                         | 44.2           | 33.7       |            | 51.9                                     | 38.0       |           | 54.2    | 28.0  |                      | 41.7 | 34.5 |   |
| Level of Service                  | D              | С          |            | D  | D          |           | D       | С     |                      | D    | С    |   |
| Approach Delay (s)                |                | 34.4       |            |  | 39.1       |           |         | 33.0  |                      |      | 35.6 |   |
| Approach LOS                      |                | С          |            |  | D          |           |         | С     |                      |      | D    |   |
| Intersection Summary              |                |            |            |  |            |           |         |       |                      |      |      |   |
| HCM Average Control Delay         |                |            | 35.8       | Н  | CM Level   | of Servic | e       |       | D                    |      |      | in production of the second |
| HCM Volume to Capacity ratio      |                |            | 0.67       |  |            |           |         |       |                      |      |      |   |
| Actuated Cycle Length (s)         |                |            | 90.0       | si s | um of lost | time (s)  |         |       | 12.0                 |      |      |   |
| Intersection Capacity Utilization |                |            | 74.4%      |  | U Level o  |           |         |       | 12.0<br>D            |      |      |   |
| Analysis Period (min)             | n da data ad M |            | 15         | trata du d <b>i S</b>                    | 5 _5 101 0 |           |         |       | n ener <b>z</b> iele |      |      |   |
| c Critical Lane Group             |                |            |            |  |            |           |         |       |                      |      |      |   |

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|--|------|----------------------|--------------|---------|---------------|-------------|-------|----------|-----------|-----------|---------------------------------------|------|
| Movement   | EBL  | EBT                  | EBR          | WBL     | WBT           | WBR         | NBL   | NBT      | NBR       | SBL       | SBT                                   | SBR  |
| Lane Configurations  | ሻ    | <b>ተ</b> ጉ           |              | ኻ       | 个             | ក៏          | ሻ     | 个        | ŕ         | ሻ         | ۹Ţ<br>۱                               |      |
| Volume (vph)   | 15   | 845                  | 87           | 239     | 754           | 400         | 189   | 70       | 323       | 296       | 134                                   | 35   |
| Ideal Flow (vphpi)   | 2000 | 2000                 | 2000         | 2000    | 2000          | 2000        | 2000  | 2000     | 2000      | 2000      | 2000                                  | 2000 |
| Lane Width   | 12   | 12                   | 12           | 12      | 12            | 12          | 11    | 11       | 11        | 12        | 12                                    | 12   |
| Total Lost time (s)  | 6.1  | 6.1                  |              | 6.1     | 6.1           | 6.0         | 6.0   | 6.0      | 6.1       | 6.0       | 6.0                                   |      |
| Lane Util. Factor  | 1.00 | 0.95                 |              | 1.00    | 1.00          | 1.00        | 1.00  | 1.00     | 1.00      | 1.00      | 1.00                                  |      |
| Frt  | 1.00 | 0.99                 |              | 1.00    | 1.00          | 0.85        | 1.00  | 1.00     | 0.85      | 1.00      | 0.97                                  |      |
| Flt Protected  | 0.95 | 1.00                 |              | 0.95    | 1.00          | 1.00        | 0.95  | 1.00     | 1.00      | 0,95      | 1.00                                  |      |
| Satd. Flow (prot)  | 1863 | 3673                 |              | 1863    | 1961          | 1500        | 1801  | 1895     | 1611      | 1863      | 1900                                  |      |
| Flt Permitted  | 0.16 | 1.00                 |              | 0.12    | 1.00          | 1.00        | 0.64  | 1.00     | 1.00      | 0.54      | 1.00                                  |      |
| Satd. Flow (perm)  | 314  | 3673                 |              | 236     | 1961          | 1500        | 1216  | 1895     | 1611      | 1051      | 1900                                  |      |
| Peak-hour factor, PHF                                      | 0.88 | 0.88                 | 0.88         | 0.92    | 0.92          | 0.92        | 0.94  | 0.94     | 0.94      | 0.92      | 0.92                                  | 0.92 |
| Adj. Flow (vph)  | 17   | 960                  | 99           | 260     | 820           | 435         | 201   | 74       | 344       | 322       | 146                                   | 38   |
| RTOR Reduction (vph)                                       | 0    | 8                    | 0            | 0       | 0             | 177         | 0     | 0        | 0         | 0         | 11                                    | 0    |
| Lane Group Flow (vph)                                      | 17   | 1051                 | 0            | 260     | 820           | 258         | 201   | 74       | 344       | 322       | 173                                   | 0    |
| Parking (#/hr)   |      |                      | 0            |         |               | 0           |       |          |           |           |                                       |      |
| Turn Type  | Perm |                      |              | pm+pt   |               | pm+ov       | Perm  | <u></u>  | pm+ov     | pm+pt     |                                       |      |
| Protected Phases   |      | 2                    |              | <u></u> | 6             | 7           |       | 8        | 1         | 7         | 4                                     |      |
| Permitted Phases   | 2    | i si shƙi ƙalƙali ta |              | 6       | ulus d'Aultes | 6           | 8     |          | 8         | 4         | Ng sing pingging.<br>Ng sing pingging |      |
| Actuated Green, G (s)                                      | 27.1 | 27.1                 |              | 44.3    | 44.3          | 53.3        | 18.6  | 18.6     | 29.7      | 33.6      | 33.6                                  |      |
| Effective Green, g (s)                                     | 27.1 | 27.1                 |              | 44.3    | 44.3          | 53.3        | 18.6  | 18.6     | 29.7      | 33.6      | 33.6                                  |      |
| Actuated g/C Ratio   | 0.30 | 0.30                 |              | 0.49    | 0.49          | 0.59        | 0.21  | 0.21     | 0.33      | 0.37      | 0.37                                  |      |
| Clearance Time (s)   | 6.1  | 6.1                  |              | 6.1     | 6.1           | 6.0         | 6.0   | 6.0      | 6.1       | 6.0       | 6.0                                   |      |
| Vehicle Extension (s)                                      | 3.0  | 3.0                  |              | 3.0     | 3.0           | 3.0         | 3.0   | 3.0      | 3.0       | 3.0       | 3.0                                   |      |
| Lane Grp Cap (vph)   | 95   | 1106                 |              | 317     | 965           | 888         | 251   | 392      | 532       | 474       | 709                                   |      |
| v/s Ratio Prot   |      | c0.29                |              | 0.10    | c0.42         | 0.03        | 201   | 0.04     | 0.08      | c0.07     | 0.09                                  |      |
| v/s Ratio Perm   | 0.05 | 00.20                |              | 0.30    | 00.12         | 0.00        | c0.17 | 0.01     | 0.00      | 0.19      | 0.00                                  |      |
| v/c Ratio  | 0.18 | 0.95                 |              | 0.82    | 0.85          | 0.29        | 0.80  | 0.19     | 0.65      | 0.68      | 0.24                                  |      |
| Uniform Delay, d1  | 23.2 | 30.8                 |              | 20.6    | 19.9          | 9.0         | 33.9  | 29.5     | 25.7      | 22.9      | 19.4                                  |      |
| Progression Factor   | 1.17 | 0.99                 |              | 1.00    | 1.00          | 1.00        | 1.00  | 1.00     | 1.00      | 1.00      | 1.00                                  |      |
| incremental Delay, d2                                      | 3.9  | 16.8                 |              | 15.5    | 9.3           | 0.2         | 16.5  | 0.2      | 2.7       | 3.9       | 0.2                                   |      |
| Delay (s)  | 31.1 | 47.2                 |              | 36.1    | 29.2          | 9.2         | 50.5  | 29.7     | 28.4      | 26.7      | 19.6                                  |      |
| Level of Service   | C    | D                    |              | D       | C             | A.          | D     | <u>с</u> | 20.1<br>C | 20.7<br>C | В                                     |      |
| Approach Delay (s)   | Ŭ    | 46.9                 |              |         | 24.6          |             |       | 35.7     |           |           | 24.1                                  |      |
| Approach LOS   |      | D                    | Geoleantea.  |         | C C           |             |       | D        |           |           | 2 л.1<br>С                            |      |
| Intersection Summary                                       |      |                      |              |         |               |             |       |          |           |           |                                       |      |
| HCM Average Control Delay                                  |      |                      | 32.9         | Н       | CM Leve       | l of Servic | e     |          | С         |           |                                       |      |
| HCM Volume to Capacity ratio                               |      |                      | 0.92         |         |               |             |       |          |           |           |                                       |      |
| Actuated Cycle Length (s)                                  |      |                      | 90.0         |         |               | t time (s)  |       |          | 24.2      |           |                                       |      |
| Intersection Capacity Utilization<br>Analysis Period (min) | 1 AV |                      | 90.1%<br>15  | lC      | U Level       | of Service  |       |          | E         |           |                                       |      |
| c Critical Lane Group                                      |      |                      |              |         |               |             |       |          |           |           |                                       |      |

|                                | هر       |                             | $\mathbf{i}$ | 1               |            | Ł                                       | 4                          | Å            | p    | 1    | <b>P</b> | 4    |
|--------------------------------|----------|-----------------------------|--------------|-----------------|------------|---|----------------------------|--------------|------|------|----------|------|
| Movement                       | EBL      | EBT                         | EBR          | WBL             | WBT        | WBR                                     | NBL                        | NBT          | NBR  | SBL  | SBT      | SBR  |
| Lane Configurations            | ሻ        | \$⇒                         |              | ሻ               | <b>Å</b>   | ٦                                       |                            | <b>€</b> Î}> |      |      | đ,       | ۲    |
| Volume (vph)                   | 287      | 185                         | 125          | 182             | 51         | 99                                      | 122                        | 467          | 341  | 425  | 923      | 136  |
| Ideal Flow (vphpl)             | 2000     | 2000                        | 2000         | 2000            | 2000       | 2000                                    | 2000                       | 2000         | 2000 | 2000 | 2000     | 2000 |
| Total Lost time (s)            | 6.0      | 6.0                         |              | 6.0             | 6.0        | 6.0                                     |                            | 6.6          |      |      | 6.6      | 6.6  |
| Lane Util. Factor              | 1.00     | 1.00                        |              | 1.00            | 1.00       | 1.00                                    |                            | 0.95         |      |      | 1.00     | 1.00 |
| Frt                            | 1.00     | 0.94                        |              | 1.00            | 1.00       | 0.85                                    |                            | 0.95         |      |      | 1.00     | 0.85 |
| Flt Protected                  | 0.95     | 1.00                        |              | 0.95            | 1.00       | 1.00                                    |                            | 0.99         |      |      | 0.98     | 1.00 |
| Satd. Flow (prot)              | 1863     | 1842                        |              | 1863            | 1961       | 1667                                    |                            | 3498         |      |      | 1930     | 1667 |
| Flt Permitted                  | 0.95     | 1.00                        |              | 0.95            | 1.00       | 1.00                                    |                            | 0.51         |      |      | 0.37     | 1.00 |
| Satd. Flow (perm)              | 1863     | 1842                        |              | 1863            | 1961       | 1667                                    |                            | 1799         |      |      | 730      | 1667 |
| Peak-hour factor, PHF          | 0.92     | 0.92                        | 0.92         | 0.92            | 0.92       | 0.92                                    | 0.92                       | 0.92         | 0.92 | 0.92 | 0.92     | 0.92 |
| Adj. Flow (vph)                | 312      | 201                         | 136          | 198             | 55         | 108                                     | 133                        | 508          | 371  | 462  | 1003     | 148  |
| RTOR Reduction (vph)           | 0        | 27                          | 0            | 0               | 0          | 93                                      | 0                          | 93           | 0    | 0    | 0        | 45   |
| Lane Group Flow (vph)          | 312      | 310                         | 0            | 198             | 55         | 15                                      | 0                          | 919          | 0    | 0    | 1465     | 103  |
| Turn Type                      | Prot     |                             |              | Prot            |            | Perm                                    | Perm                       |              |      | Perm |          | Perm |
| Protected Phases               | 7        | 4                           |              | 3               | 8          |   |                            | 2            |      |      | 6        |      |
| Permitted Phases               |          | a nationale le ferrar de la |              |                 |            | 8                                       | 2                          |              |      | 6    |          | 6    |
| Actuated Green, G (s)          | 14.4     | 17.2                        |              | 10.0            | 12.8       | 12.8                                    |                            | 45.4         |      |      | 45.4     | 45.4 |
| Effective Green, g (s)         | -14.4    | 17.2                        |              | 10.0            | 12.8       | 12.8                                    |                            | 45.4         |      |      | 45.4     | 45.4 |
| Actuated g/C Ratio             | 0.16     | 0.19                        |              | 0.11            | 0.14       | 0,14                                    |                            | 0.50         |      |      | 0.50     | 0.50 |
| Clearance Time (s)             | 6.0      | 6.0                         |              | 6.0             | 6.0        | 6.0                                     |                            | 6.6          |      |      | 6.6      | 6.6  |
| Vehicle Extension (s)          | 3.0      | 3.0                         |              | 3.0             | 3.0        | 3.0                                     |                            | 3.0          |      |      | 3.0      | 3.0  |
| Lane Grp Cap (vph)             | 294      | 347                         |              | 204             | 275        | 234                                     |                            | 896          |      |      | 363      | 830  |
| v/s Ratio Prot                 | c0.17    | c0.17                       |              | 0.11            | 0.03       |   |                            |              |      |      |          |      |
| v/s Ratio Perm                 |          |                             |              |                 |            | 0.01                                    |                            | 0.51         |      |      | c2.01    | 0.06 |
| v/c Ratio                      | 1.06     | 0.89                        |              | 0.97            | 0.20       | 0.06                                    |                            | 1.03         |      |      | 4.04     | 0.12 |
| Uniform Delay, d1              | 38.4     | 36.1                        |              | 40.5            | 34.7       | 34.0                                    |                            | 22.9         |      |      | 22.9     | 12.3 |
| Progression Factor             | 1.00     | 1.00                        |              | 1.00            | 1.00       | 1.00                                    |                            | 1.00         |      |      | 1.00     | 1.00 |
| Incremental Delay, d2          | 69.6     | 24.0                        |              | 54.3            | 0.4        | 0.1                                     |                            | 36.8         |      |      | 1372.7   | 0.3  |
| Delay (s)                      | 108.0    | 60.1                        |              | 94.8            | 35.0       | 34.1                                    |                            | 59.7         |      |      | 1395.6   | 12.6 |
| Level of Service               | F        | Е                           |              | F               | D          | С                                       |                            | E            |      |      | F        | В    |
| Approach Delay (s)             |          | 83.1                        |              |                 | 67.5       |   |                            | 59.7         |      |      | 1268.7   |      |
| Approach LOS                   |          | F                           |              |                 | E          |   |                            | Е            |      |      | F        |      |
| Intersection Summary           |          |                             |              |                 |            | <u></u>                                 |                            |              | F    |      |          |      |
| HCM Average Control Delay      |          |                             | 601.1        | H(              |            | of Service                              | <b>)</b><br>               |              | F    |      |          |      |
| HCM Volume to Capacity ra      | lio      |                             | 2.93         |                 |            | (1) (1) (1) (1) (1) (1) (1) (1) (1) (1) |                            |              | 10.0 |      |          |      |
| Actuated Cycle Length (s)      | elimetro |                             | 91.2         |                 | um of lost |   | an gan an                  |              | 18.6 |      |          |      |
| Intersection Capacity Utilizat | uon      |                             | 141.6%       | lC and a second | U Level (  | of Service                              |                            |              | H    |      |          |      |
| Analysis Period (min)          |          |                             | 15           |                 |            |   | 9.9.0.9.9.9<br>9.9.0.9.9.9 |              |      |      |          |      |
| c Critical Lane Group          |          |                             |              |                 |            |   |                            |              |      |      | 상영원문문    |      |

|   | ٨     | >        | $\mathbf{i}$ | 1     | <b>4</b>   | Ł         | ٩     | Ť    | p           | 1                       | Ļ     | 4    |
|---|-------|----------|--------------|-------|------------|-----------|-------|------|-------------|-------------------------|-------|------|
| Movement                                | EBL   | EBT      | EBR          | WBL   | WBT        | WBR       | NBL   | NBT  | NBR         | SBL                     | SBT   | SBR  |
| Lane Configurations                     | ሻ     | <b>þ</b> | <u></u>      | ٢     | \$         |           | ሻ     | Þ    |             | ሻ                       | 个     | 7    |
| Volume (vph)                            | 183   | 196      | 311          | 225   | 87         | 82        | 195   | 480  | 69          | 3                       | 767   | 37   |
| Ideal Flow (vphpl)                      | 2000  | 2000     | 2000         | 2000  | 2000       | 2000      | 2000  | 2000 | 2000        | 2000                    | 2000  | 2000 |
| Total Lost time (s)                     | 6.1   | 6.1      |              | 6.1   | 6.1        |           | 5.9   | 5.9  |             | 5.9                     | 5.9   | 5.9  |
| Lane Util. Factor                       | 1.00  | 1.00     |              | 1.00  | 1.00       |           | 1.00  | 1.00 |             | 1.00                    | 1.00  | 1.00 |
| Frt                                     | 1.00  | 0.91     |              | 1.00  | 0.93       |           | 1.00  | 0.98 |             | 1.00                    | 1.00  | 0.85 |
| Flt Protected                           | 0.95  | 1.00     |              | 0.95  | 1.00       |           | 0.95  | 1.00 | 11. at 14.5 | 0.95                    | 1.00  | 1.00 |
| Satd. Flow (prot)                       | 1881  | 1762     |              | 1863  | 1826       |           | 1743  | 1908 |             | 1900                    | 1980  | 1650 |
| Fit Permitted                           | 0.46  | 1.00     |              | 0.22  | 1.00       |           | 0.11  | 1.00 |             | 0.12                    | 1.00  | 1.00 |
| Satd. Flow (perm)                       | 910   | 1762     |              | 438   | 1826       |           | 193   | 1908 |             | 249                     | 1980  | 1650 |
| Peak-hour factor, PHF                   | 0.81  | 0.81     | 0.81         | 0.73  | 0.73       | 0.73      | 0.74  | 0.74 | 0.74        | 0.84                    | 0.84  | 0.84 |
| Adj. Flow (vph)                         | 226   | 242      | 384          | 308   | 119        | 112       | 264   | 649  | 93          | 4                       | 913   | 44   |
| RTOR Reduction (vph)                    | 0     | 63       | 0            | 0     | 38         | 0         | 0     | 5    | 0           | 0                       | 0     | 7    |
| Lane Group Flow (vph)                   | 226   | 563      | 0            | 308   | 193        | 0         | 264   | 737  | 0           | 4                       | 913   | 37   |
| Heavy Vehicles (%)                      | 1%    | 0%       | 5%           | 2%    | 3%         | 0%        | 9%    | 2%   | 9%          | 0%                      | 1%    | 3%   |
| Turn Type                               | pm+pt |          |              | pm+pt |            |           | pm+pt |      |             | Perm                    |       | Perm |
| Protected Phases                        | 7     | 4        |              | 3     | 8          |           | 5     | 2    |             | h hall a tao a sa t sta | 6     |      |
| Permitted Phases                        | 4     |          |              | 8     |            |           | 2     |      |             | 6                       |       | 6    |
| Actuated Green, G (s)                   | 26.8  | 17.9     |              | 26.8  | 17.9       |           | 45.1  | 45.1 |             | 32.1                    | 32.1  | 32.1 |
| Effective Green, g (s)                  | 26.8  | 17.9     |              | 26.8  | 17.9       |           | 45.1  | 45.1 |             | 32.1                    | 32.1  | 32.1 |
| Actuated g/C Ratio                      | 0.30  | 0.20     |              | 0.30  | 0.20       |           | 0.50  | 0.50 |             | 0.36                    | 0.36  | 0.36 |
| Clearance Time (s)                      | 6.1   | 6.1      |              | 6.1   | 6.1        |           | 5.9   | 5.9  |             | 5.9                     | 5.9   | 5.9  |
| Vehicle Extension (s)                   | 3.0   | 3.0      |              | 3.0   | 3.0        |           | 3.0   | 3.0  |             | 3.0                     | 3.0   | 3.0  |
| Lane Grp Cap (vph)                      | 367   | 350      |              | 271   | 363        |           | 219   | 956  |             | 89                      | 706   | 589  |
| v/s Ratio Prot                          | 0.06  | c0.32    |              | c0.11 | 0.11       |           | c0.10 | 0.39 |             |                         | 0.46  |      |
| v/s Ratio Perm                          | 0.12  |          |              | 0.23  |            |           | c0.51 |      |             | 0.02                    |       | 0.02 |
| v/c Ratio                               | 0.62  | 1.61     |              | 1.14  | 0.53       |           | 1.21  | 0.77 |             | 0.04                    | 1.29  | 0.06 |
| Uniform Delay, d1                       | 25.4  | 36.0     |              | 29.2  | 32.3       |           | 37.4  | 18.2 |             | 18.9                    | 28.9  | 19.1 |
| Progression Factor                      | 1.00  | 1.00     |              | 1.00  | 1.00       |           | 1.00  | 1.00 |             | 0.85                    | 0.93  | 0.82 |
| Incremental Delay, d2                   | 3.1   | 286.5    |              | 96.6  | 1.5        |           | 127.4 | 6.0  |             | 0.9                     | 142.1 | 0.2  |
| Delay (s)                               | 28.4  | 322.5    |              | 125.8 | 33.8       |           | 164.9 | 24.2 |             | 17.1                    | 169.1 | 15.8 |
| Level of Service                        | С     | F        |              | E.    | С          |           | F     | С    |             | В                       | F     | В    |
| Approach Delay (s)                      |       | 244.5    |              |       | 86.4       |           |       | 61.1 |             |                         | 161.5 |      |
| Approach LOS                            |       | E E      |              |       | E          |           |       | E    |             |                         | S E C |      |
| Intersection Summary                    |       |          |              |       |            |           |       |      |             |                         |       |      |
| HCM Average Control Delay               |       |          | 140.4        | H     | CM Level   | of Servic | )e    |      | F           |                         |       |      |
| HCM Volume to Capacity ratio            |       |          | 1.26         |       |            |           |       |      |             |                         |       |      |
| Actuated Cycle Length (s)               |       |          | 90.0         | Sı    | um of lost | time (s)  |       |      | 18.1        |                         |       |      |
| Intersection Capacity Utilization       | 1     |          | 108.4%       |       | U Level o  |           | )     |      | G           |                         |       |      |
| Analysis Period (min)                   |       |          | 15           |       |            |           |       |      |             |                         |       |      |
| <ul> <li>Oritical Lana Crown</li> </ul> |       |          |              |       |            |           |       |      |             |                         |       |      |

|                                   | ٨            |            | $\mathbf{F}$ | 1     | <b>4</b>   | Ł                    | 4     | Î    | Þ         | 6    | ţ     | 1               |
|-----------------------------------|--------------|------------|--------------|-------|------------|----------------------|-------|------|-----------|------|-------|-----------------|
| Movement                          | EBL          | EBT        | EBR          | WBL   | WBT        | WBR                  | NBL   | NBT  | NBR       | SBL  | SBT   | SBR             |
| Lane Configurations               | ሻ            | <b>ቶ</b> ኈ |              | ሻ     | <b>ት</b> ጮ |                      | ሻ     | Þ    |           | ሻ    | β     |                 |
| Volume (vph)                      | 22           | 687        | 120          | 34    | 582        | 14                   | 83    | 222  | 50        | 51   | 486   | 12              |
| Ideal Flow (vphpl)                | 2000         | 2000       | 2000         | 2000  | 2000       | 2000                 | 2000  | 2000 | 2000      | 2000 | 2000  | 2000            |
| Total Lost time (s)               | 6.0          | 6.0        |              | 6.0   | 6.0        |                      | 6.0   | 6.0  |           | 6.0  | 6.0   |                 |
| Lane Util. Factor                 | 1.00         | 0.95       |              | 1.00  | 0.95       |                      | 1.00  | 1.00 |           | 1.00 | 1.00  |                 |
| Frt                               | 1.00         | 0.98       |              | 1.00  | 1.00       |                      | 1.00  | 0.97 |           | 1.00 | 1.00  |                 |
| Fit Protected                     | 0.95         | 1.00       |              | 0.95  | 1.00       |                      | 0.95  | 1.00 |           | 0.95 | 1.00  |                 |
| Satd. Flow (prot)                 | 1863         | 3642       |              | 1863  | 3712       |                      | 1863  | 1906 |           | 1863 | 1954  |                 |
| Flt Permitted                     | 0.95         | 1.00       |              | 0.95  | 1.00       |                      | 0.95  | 1.00 |           | 0.95 | 1.00  |                 |
| Satd. Flow (perm)                 | 1863         | 3642       |              | 1863  | 3712       |                      | 1863  | 1906 |           | 1863 | 1954  |                 |
| Peak-hour factor, PHF             | 0.79         | 0.79       | 0.79         | 0.70  | 0.70       | 0.70                 | 0.95  | 0.95 | 0.95      | 0.81 | 0.81  | 0.81            |
| Adj. Flow (vph)                   | 28           | 870        | 152          | 49    | 831        | 20                   | 87    | 234  | 53        | 63   | 600   | 15              |
| RTOR Reduction (vph)              | 0            | 15         | 0            | 0     | 1          | 0                    | 0     | 9    | 0         | 0    | 1     | 0               |
| Lane Group Flow (vph)             | 28           | 1007       | 0            | 49    | 850        | 0                    | 87    | 278  | 0         | 63   | 614   | 0               |
| Turn Type                         | Prot         |            |              | Prot  |            |                      | Prot  |      |           | Prot |       |                 |
| Protected Phases                  | 5            | 2          |              | 1     | 6          |                      | 3     | 8    |           | 7    | 4     |                 |
| Permitted Phases                  |              |            |              |       |            |                      |       |      |           |      |       |                 |
| Actuated Green, G (s)             | 2.8          | 25.8       |              | 4.2   | 27.2       |                      | 6.4   | 29.8 |           | 6.2  | 29.6  |                 |
| Effective Green, g (s)            | 2.8          | 25.8       |              | 4.2   | 27.2       |                      | 6.4   | 29.8 |           | 6.2  | 29.6  |                 |
| Actuated g/C Ratio                | 0.03         | 0.29       |              | 0.05  | 0.30       |                      | 0.07  | 0.33 |           | 0.07 | 0.33  |                 |
| Clearance Time (s)                | 6.0          | 6.0        |              | 6.0   | 6.0        |                      | 6.0   | 6.0  |           | 6.0  | 6.0   |                 |
| Vehicle Extension (s)             | 3.0          | 3.0        |              | 3.0   | 3.0        |                      | 3.0   | 3.0  |           | 3.0  | 3.0   |                 |
| Lane Grp Cap (vph)                | 58           | 1044       |              | 87    | 1122       |                      | 132   | 631  |           | 128  | 643   |                 |
| v/s Ratio Prot                    | 0.02         | c0.28      |              | c0.03 | 0.23       |                      | c0.05 | 0.15 |           | 0.03 | c0.31 |                 |
| v/s Ratio Perm                    |              |            |              |       |            | tatana kinata data : |       |      |           |      |       |                 |
| v/c Ratio                         | 0.48         | 0.96       |              | 0.56  | 0.76       |                      | 0.66  | 0.44 |           | 0.49 | 0.95  |                 |
| Uniform Delay, d1                 | 42.9         | 31.6       |              | 42.0  | 28.4       |                      | 40.7  | 23.6 |           | 40.4 | 29.5  |                 |
| Progression Factor                | 1.00         | 1.00       |              | 1.07  | 1.31       |                      | 1.01  | 0.91 |           | 1.00 | 1.00  |                 |
| Incremental Delay, d2             | 6.2          | 20.5       |              | 5.9   | 3.5        |                      | 11.0  | 0.5  |           | 3.0  | 24.5  | an na staine de |
| Delay (s)                         | 49.1         | 52.2       |              | 50.8  | 40.9       |                      | 52.3  | 21.8 |           | 43.3 | 54.1  |                 |
| Level of Service                  | D            | D          |              | D     | D          |                      | D     | С    |           | D    | D     |                 |
| Approach Delay (s)                |              | 52.1       |              |       | 41.4       |                      |       | 28.9 |           |      | 53.1  |                 |
| Approach LOS                      |              | D          |              |       | D          |                      |       | С    |           |      | D     |                 |
| Intersection Summary              |              |            |              |       |            |                      |       |      |           |      |       |                 |
| HCM Average Control Delay         |              |            | 46.2         | H     | CM Level   | of Servic            | e     |      | D         |      |       |                 |
| HCM Volume to Capacity ratio      |              |            | 0.90         |       |            | 01 001110            |       |      |           |      |       |                 |
| Actuated Cycle Length (s)         |              |            | 90.0         | Si    | im of lost | time (s)             |       |      | 24.0      |      |       | t destables.    |
| Intersection Capacity Utilization | 12000        |            | 72.7%        |       | U Level o  |                      |       |      | 24.0<br>C |      |       |                 |
| Analysis Period (min)             | tun ten Alle |            | 15           | 10    |            |                      |       |      |           |      |       |                 |
| c Critical Lane Group             |              |            | vi<br>Vacate |       |            |                      |       |      |           |      |       |                 |

| EBT<br><b>†1</b><br>711<br>2000<br>12<br>6.1<br>0.95<br>0.97<br>1.00<br>3610<br>1.00<br>2010 | EBR<br>186<br>2000<br>12  | WBL<br>235<br>2000<br>12<br>6.1<br>1.00           | WBT<br>746<br>2000<br>12<br>6.1  | WBR<br>135<br>2000<br>12  | NBL<br><b>ř</b><br>61<br>2000<br>11  | NBT<br>₽⇒<br>25<br>2000   | NBR<br>251<br>2000  | SBL<br><b>أ</b><br>212  | SBT<br>₽<br>48  | SBR   |
|--|---|---|--|---|--|---|---|---|---|---|
| 711<br>2000<br>12<br>6.1<br>0.95<br>0.97<br>1.00<br>3610<br>1.00                             | 2000  | 235<br>2000<br>12<br>6.1<br>1.00                  | 746<br>2000<br>12<br>6.1   | 135<br>2000<br>12   | 61<br>2000   | 25<br>2000  |   | 212   |   |   |
| 711<br>2000<br>12<br>6.1<br>0.95<br>0.97<br>1.00<br>3610<br>1.00                             | 2000  | 2000<br>12<br>6.1<br>1.00                         | 746<br>2000<br>12<br>6.1   | 2000<br>12  | 61<br>2000   | 25<br>2000  |   |   |   |   |
| 12<br>6.1<br>0.95<br>0.97<br>1.00<br>3610<br>1.00  |   | 12<br>6.1<br>1.00                                 | 12<br>6.1  | 12  |  |   | 2000  |   | τu  | 12  |
| 6.1<br>0.95<br>0.97<br>1.00<br>3610<br>1.00  | 12  | 6.1<br>1.00                                       | 6.1  |   | 11   |   |   | 2000  | 2000  | 2000  |
| 0.95<br>0.97<br>1.00<br>3610<br>1.00   |   | 1.00  | A CONTRACTOR OF A CONTRACTOR OFTA CONTRACTOR O | <b>∩</b> 4  |  | 11  | 11  | 12  | 12  | 12  |
| 0.97<br>1.00<br>3610<br>1.00   |   |   | apage apage a san an   | 6.1   | 6.0  | 6.0   |   | 6.0   | 6.0   |   |
| 0.97<br>1.00<br>3610<br>1.00   |   |   | 1.00   | 1.00  | 1.00   | 1.00  |   | 1.00  | 1.00  |   |
| 1.00<br>3610<br>1.00   |   | 1.00  | 1.00   | 0.85  | 1.00   | 0.86  |   | 1.00  | 0.97  |   |
| 3610<br>1.00   |   | 0.95  | 1.00   | 1.00  | 0.95   | 1.00  |   | 0.95  | 1.00  |   |
| 1.00   |   | 1863  | 1961   | 1500  | 1801   | 1637  |   | 1863  | 1902  |   |
|  |   | 0.12  | 1.00   | 1.00  | 0.70   | 1.00  |   | 0.23  | 1.00  |   |
| 3610   |   | 238   | 1961   | 1500  | 1336   | 1637  |   | 457   | 1902  |   |
| 0.76   | 0.76  | 0.83  | 0.83   | 0.83  | 0.83   | 0.83  | 0.83  | 0.75  | 0.75  | 0.75  |
| 936  | 245   | 283   | 899  | 163   | 73   | 30  | 302   | 283   | 64  | 16  |
| 26   | - 10  |   | 0  | 78  | .0   | Ő   | 0   | 0   | 10  | 0   |
| 1155   | 0   | 283   | 899  | 85  | 73   | 332   | 0   | 283   | 70  | 0   |
| 1100   | Õ   | 200   | 000  | Ő   | 10   | 002   |   | 200   |   |   |
|  |   | pm+pt   |  | Perm  | Perm   |   |   | pm+pt   |   | <u>,</u>  |
| 2  |   | p p.<br>1   | 6  |   |  | 8   |   | 7   | 4   |   |
| Albana (n. 🛲 da  |   | 6   |  | 6   | 8  |   |   | 4   | batta barri.  |   |
| 26.9   |   | 43.1  | 43.1   | 43.1  | 20.8   | 20.8  |   | 34.8  | 34.8  |   |
| 26.9   |   | 43.1  | 43.1   | 43.1  | 20.8   | 20.8  | ne Friedrich (d. 1949)<br>Alf   | 34.8  | 34.8  |   |
| 0.30   |   | 0.48  | 0.48   | 0.48  | 0.23   | 0.23  |   | 0.39  | 0.39  |   |
| 6.1  |   | 6.1   | 6.1  | 6.1   | 6.0  | 6.0   |   | 6.0   | 6.0   |   |
| 3.0  |   | 3.0   | 3.0  | 3.0   | 3.0  | 3.0   |   | 3.0   | 3.0   |   |
| 1079   |   | 296   | 939  | 718   | 309  | 378   |   | 302   | 735   | <u></u>   |
|  |   |   |  | 7 10  |  |   |   |   |   |   |
| 00.02  |   |   | 00.40  | 0.06  | 0.05   | 0.20  |   |   | 0.04  |   |
| 1 07   |   |   | 0.06   |   |  | 0.88  |   |   | 0.10  |   |
|  |   |   |  |   |  |   |   |   |   |   |
|  |   |   |  |   |  |   |   |   |   |   |
|  |   |   |  |   |  |   |   |   |   |   |
|  |   |   |  |   |  |   |   |   |   |   |
|  |   |   |  |   |  |   |   |   |   |   |
|  |   |   |  | P   | U I  |   |   | <b>드</b><br>2013년(2013)   |   |   |
|  |   |   |  |   |  |   |   |   |   |   |
| L.   | construction and sold   |   | U  |   |  | U   |   |   | U   |   |
|  |   |   | <u></u>  | - <u></u>   |  |   | -   |   |   |   |
|  |   | H<br>Reserves                                     |  | OT SELVICE  | <b>)</b><br>(()))))))))  |   | <b>L</b><br>1970-1970-1970  |   |   | i de la come  |
|  |   | isteret (   |  | 44442 (44)<br>41  |  |   | 40.0  |   |   |   |
|  |   |   |  |   |  |   |   |   | and the second  |   |
|  |   | IC a set of the                                   | U Level c  | or Service  |  |   | ter (Pres   |   |   |   |
|  | 15  |   |  |   |  |   |   |   |   |   |
| - 1997   | c0.32<br>1.07<br>31.6<br>0.94<br>47.1<br>76.9<br>E<br>76.6<br>E | 1.07<br>31.6<br>0.94<br>47.1<br>76.9<br>E<br>76.6 | 0.35<br>1.07 0.96<br>31.6 23.1<br>0.94 1.00<br>47.1 40.2<br>76.9 63.3<br>E E<br>76.6<br>E<br>57.0 H<br>1.00<br>90.0 Si<br>92.9% IC   | 0.35<br>1.07 0.96 0.96<br>31.6 23.1 22.6<br>0.94 1.00 1.00<br>47.1 40.2 20.7<br>76.9 63.3 43.3<br>E E D<br>76.6 43.9<br>E D<br>76.6 43.9<br>E D<br>76.6 43.9<br>E D | 0.35         0.06           1.07         0.96         0.96         0.12           31.6         23.1         22.6         13.0           0.94         1.00         1.00         1.00           47.1         40.2         20.7         0.3           76.9         63.3         43.3         13.3           E         E         D         B           76.6         43.9         E         D           57.0         HCM Level of Service           1.00         90.0         Sum of lost time (s)           92.9%         ICU Level of Service | 0.35         0.06         0.05           1.07         0.96         0.96         0.12         0.24           31.6         23.1         22.6         13.0         28.1           0.94         1.00         1.00         1.00         1.00           47.1         40.2         20.7         0.3         0.4           76.9         63.3         43.3         13.3         28.5           E         E         D         B         C           76.6         43.9         E         D           F           57.0         HCM Level of Service           1.00         90.0         Sum of lost time (s)           92.9%         ICU Level of Service | 0.35         0.06         0.05           1.07         0.96         0.96         0.12         0.24         0.88           31.6         23.1         22.6         13.0         28.1         33.4           0.94         1.00         1.00         1.00         1.00         1.00           47.1         40.2         20.7         0.3         0.4         20.0           76.9         63.3         43.3         13.3         28.5         53.3           E         E         D         B         C         D           76.6         43.9         48.9         E         D         D           57.0         HCM Level of Service           1.00         90.0         Sum of lost time (s)         92.9%         ICU Level of Service | 0.35         0.06         0.05           1.07         0.96         0.96         0.12         0.24         0.88           31.6         23.1         22.6         13.0         28.1         33.4           0.94         1.00         1.00         1.00         1.00         1.00           47.1         40.2         20.7         0.3         0.4         20.0           76.9         63.3         43.3         13.3         28.5         53.3           E         E         D         B         C         D           76.6         43.9         48.9         D         D           Z         D         D         D         D         D           76.6         43.9         48.9         D         D         D           76.6         43.9         D         D         D         D           76.6         90.0         Sum of lost time (s)         18.2         1.00           90.0         Sum of lost time (s)         18.2         92.9%         ICU Level of Service         F | 0.35         0.06         0.05         c0.28           1.07         0.96         0.96         0.12         0.24         0.88         0.94           31.6         23.1         22.6         13.0         28.1         33.4         24.4           0.94         1.00         1.00         1.00         1.00         1.00         1.00           47.1         40.2         20.7         0.3         0.4         20.0         35.2           76.9         63.3         43.3         13.3         28.5         53.3         59.5           E         E         D         B         C         D         E           76.6         43.9         48.9         D         D         D         D           76.6         43.9         48.9         D         D         D         E           76.6         43.9         B         D         D         D         D         E           90.0         Sum of lost time (s)         18.2         18.2         18.2         18.2         18.2           92.9%         ICU Level of Service         F         F         160         160         160         160         160         160 | 0.35         0.06         0.05         c0.28           1.07         0.96         0.96         0.12         0.24         0.88         0.94         0.10           31.6         23.1         22.6         13.0         28.1         33.4         24.4         17.6           0.94         1.00         1.00         1.00         1.00         1.00         1.00           47.1         40.2         20.7         0.3         0.4         20.0         35.2         0.1           76.9         63.3         43.3         13.3         28.5         53.3         59.5         17.6           E         E         D         B         C         D         E         B           76.6         43.9         48.9         50.3         53.3         59.5         17.6           E         D         D         D         D         D         D         D           76.6         43.9         48.9         50.3         50.3         59.5         17.6           E         D         D         D         D         D         D         D           90.0         Sum of lost time (s)         18.2         18.2         12 |

|                               | <u>_</u> |       | >             | 1     | <b>4</b>   | Ł                            | 1    | Â    | p               | 1                             | Ť     | 4      |
|-------------------------------|----------|-------|---------------|-------|------------|------------------------------|------|------|-----------------|-------------------------------|-------|--------|
| Movement                      | EBL      | EBT   | EBR           | WBL   | WBT        | WBR                          | NBL  | NBT  | NBR             | SBL                           | SBT   | SBR    |
| Lane Configurations           | ሻ        | 4Î    |               | ሻ     | 个          | ศึ                           |      | ፋኈ   |                 |                               | र्स   | ŕ      |
| Volume (vph)                  | 721      | 175   | 411           | 554   | 170        | 341                          | 87   | 469  | 163             | 188                           | 750   | 165    |
| Ideal Flow (vphpl)            | 2000     | 2000  | 2000          | 2000  | 2000       | 2000                         | 2000 | 2000 | 2000            | 2000                          | 2000  | 2000   |
| Total Lost time (s)           | 6.0      | 6.0   |               | 6.0   | 6.0        | 6.0                          |      | 6.6  |                 |                               | 6.6   | 6.6    |
| Lane Util. Factor             | 1.00     | 1.00  |               | 1.00  | 1.00       | 1.00                         |      | 0.95 |                 |                               | 1.00  | 1.00   |
| Frt                           | 1.00     | 0.89  |               | 1.00  | 1.00       | 0.85                         |      | 0.97 |                 |                               | 1.00  | 0.85   |
| Flt Protected                 | 0.95     | 1.00  |               | 0.95  | 1.00       | 1.00                         |      | 0.99 |                 |                               | 0.99  | 1.00   |
| Satd. Flow (prot)             | 1863     | 1754  |               | 1863  | 1961       | 1667                         |      | 3577 |                 |                               | 1941  | 1667   |
| Flt Permitted                 | 0.95     | 1.00  |               | 0.95  | 1.00       | 1.00                         |      | 0.51 |                 |                               | 0.54  | 1.00   |
| Satd. Flow (perm)             | 1863     | 1754  |               | 1863  | 1961       | 1667                         |      | 1829 |                 |                               | 1060  | 1667   |
| Peak-hour factor, PHF         | 0.92     | 0.92  | 0.92          | 0.92  | 0.92       | 0.92                         | 0.92 | 0.92 | 0.92            | 0.92                          | 0.92  | 0.92   |
| Adj. Flow (vph)               | 784      | 190   | 447           | 602   | 185        | 371                          | 95   | 510  | 177             | 204                           | 815   | 179    |
| RTOR Reduction (vph)          | 0        | 51    | 0             | 0     | 0          | 132                          | 0    | 30   | 0               | 0                             | 0     | 77     |
| Lane Group Flow (vph)         | 784      | 586   | 0             | 602   | 185        | 239                          | 0    | 752  | 0               | 0                             | 1019  | 102    |
| Turn Type                     | Prot     |       |               | Prot  |            | Perm                         | Perm |      |                 | Perm                          |       | Perm   |
| Protected Phases              | 7        | 4     |               | 3     | 8          |                              |      | 2    |                 |                               | 6     |        |
| Permitted Phases              |          |       |               |       |            | 8                            | 2    |      |                 | 6                             |       | 6      |
| Actuated Green, G (s)         | 15.0     | 18.0  |               | 15.0  | 18.0       | 18.0                         |      | 38.4 |                 |                               | 38.4  | 38.4   |
| Effective Green, g (s)        | 15.0     | 18.0  |               | 15.0  | 18.0       | 18.0                         |      | 38.4 |                 |                               | 38.4  | 38.4   |
| Actuated g/C Ratio            | 0.17     | 0.20  |               | 0.17  | 0.20       | 0.20                         |      | 0.43 |                 |                               | 0.43  | 0.43   |
| Clearance Time (s)            | 6.0      | 6.0   |               | 6.0   | 6.0        | 6.0                          |      | 6.6  |                 |                               | 6.6   | 6.6    |
| Vehicle Extension (s)         | 3.0      | 3.0   |               | 3.0   | 3.0        | 3.0                          |      | 3.0  |                 |                               | 3.0   | 3.0    |
| Lane Grp Cap (vph)            | 311      | 351   |               | 311   | 392        | 333                          |      | 780  |                 |                               | 452   | 711    |
| v/s Ratio Prot                | c0.42    | c0.33 |               | 0.32  | 0.09       |                              |      |      |                 |                               |       |        |
| v/s Ratio Perm                |          |       |               |       |            | 0.14                         |      | 0.41 |                 |                               | c0.96 | 0.06   |
| v/c Ratio                     | 2.52     | 1.67  |               | 1.94  | 0.47       | 0.72                         |      | 0.96 |                 |                               | 2.25  | 0.14   |
| Uniform Delay, d1             | 37.5     | 36.0  |               | 37.5  | 31.8       | 33.6                         |      | 25.1 |                 |                               | 25.8  | 15.8   |
| Progression Factor            | 1.00     | 1.00  |               | 1.00  | 1.00       | 1.00                         |      | 1.00 |                 |                               | 1.00  | 1.00   |
| Incremental Delay, d2         | 693.9    | 313.3 |               | 432.7 | 0.9        | 7.2                          |      | 24.5 |                 |                               | 571.6 | 0.4    |
| Delay (s)                     | 731.4    | 349.3 |               | 470.2 | 32.7       | 40.8                         |      | 49.6 |                 |                               | 597.4 | 16.2   |
| Level of Service              | F        | F     |               | F     | С          | D                            |      | D    |                 |                               | F     | В      |
| Approach Delay (s)            |          | 560.1 |               |       | 262.8      |                              |      | 49.6 |                 |                               | 510.5 |        |
| Approach LOS                  |          | F     | a disatiri si |       | F          | i Marina, Angelanda (kabaga) | 2    | D    | 2623-11264, 201 | n an Anna Anna Anna Anna<br>A | F     | na ang |
| Intersection Summary          |          |       |               |       |            |                              |      |      |                 |                               |       |        |
| HCM Average Control Dela      | у        |       | 384.0         | H     | CM Level   | of Service                   |      |      | F               |                               |       | -      |
| HCM Volume to Capacity ra     | atio     |       | 2.16          |       |            |                              |      |      |                 |                               |       |        |
| Actuated Cycle Length (s)     |          |       | 90.0          | Su    | um of lost | time (s)                     |      |      | 18.6            |                               |       |        |
| Intersection Capacity Utiliza | ition    |       | 149.9%        | IC    | U Level o  | of Service                   |      |      | Н               |                               |       |        |
| Analysis Period (min)         |          |       | 15            |       |            |                              |      |      |                 |                               |       |        |
| c Critical Lane Group         |          |       |               |       |            |                              |      |      |                 |                               |       |        |

|                                  | ٨                                      |       | 7      | *     | <b>-</b>   | Ł         | ٩     | Î     | p    | \$                       | ţ    | 1    |
|----------------------------------|--|-------|--------|-------|------------|-----------|-------|-------|------|--------------------------|------|------|
| Movement                         | EBL                                    | EBT   | EBR    | WBL   | WBT        | WBR       | NBL   | NBT   | NBR  | SBL                      | SBT  | SBR  |
| Lane Configurations              | Ϋ́ς                                    | ĥ     |        | Ϋ́ς   | ₽          |           | ሻ     | ĥ     |      | ٣                        | ተ    | ŕ    |
| Volume (vph)                     | 128                                    | 183   | 334    | 197   | 312        | 5         | 374   | 897   | 89   | 4                        | 504  | 167  |
| Ideal Flow (vphpl)               | 2000                                   | 2000  | 2000   | 2000  | 2000       | 2000      | 2000  | 2000  | 2000 | 2000                     | 2000 | 2000 |
| Total Lost time (s)              | 6.1                                    | 6.1   |        | 6.1   | 6.1        |           | 5.9   | 5.9   |      | 5.9                      | 5.9  | 5.9  |
| Lane Util. Factor                | 1.00                                   | 1.00  |        | 1.00  | 1.00       |           | 1.00  | 1.00  |      | 1.00                     | 1.00 | 1.00 |
| Frt                              | 1.00                                   | 0.90  |        | 1.00  | 1.00       |           | 1.00  | 0.99  |      | 1.00                     | 1.00 | 0.85 |
| Flt Protected                    | 0.95                                   | 1.00  |        | 0.95  | 1.00       |           | 0.95  | 1.00  |      | 0.95                     | 1.00 | 1.00 |
| Satd. Flow (prot)                | 1881                                   | 1750  |        | 1863  | 1938       |           | 1743  | 1922  |      | 1900                     | 1980 | 1650 |
| Flt Permitted                    | 0.20                                   | 1.00  |        | 0.19  | 1.00       |           | 0.18  | 1.00  |      | 0.15                     | 1.00 | 1.00 |
| Satd. Flow (perm)                | 389                                    | 1750  |        | 372   | 1938       |           | 326   | 1922  |      | 295                      | 1980 | 1650 |
| Peak-hour factor, PHF            | 0.83                                   | 0.83  | 0.83   | 0.80  | 0.80       | 0.80      | 0.90  | 0.90  | 0.90 | 0.95                     | 0.95 | 0.95 |
| Adj. Flow (vph)                  | 154                                    | 220   | 402    | 246   | 390        | 6         | 416   | 997   | 99   | 4                        | 531  | 176  |
| RTOR Reduction (vph)             | 0                                      | 73    | 0      | 0     | 1          | 0         | 0     | 4     | 0    | 0                        | 0    | 48   |
| Lane Group Flow (vph)            | 154                                    | 549   | Ō      | 246   | 395        | Ō         | 416   | 1092  | 0    | 4                        | 531  | 128  |
| Heavy Vehicles (%)               | 1%                                     | 0%    | 5%     | 2%    | 3%         | 0%        | 9%    | 2%    | 9%   | 0%                       | 1%   | 3%   |
| Turn Type                        | pm+pt                                  |       |        | pm+pt |            |           | pm+pt |       |      | Perm                     |      | Perm |
| Protected Phases                 | 7                                      | 4     |        | 3     | 8          |           | 5     | 2     |      |                          | 6    |      |
| Permitted Phases                 | 4                                      |       |        | 8     |            |           | 2     |       |      | 6                        |      | 6    |
| Actuated Green, G (s)            | 28.6                                   | 20.9  |        | 29.0  | 21.1       |           | 43.1  | 43.1  |      | 27.1                     | 27.1 | 27.1 |
| Effective Green, g (s)           | 28.6                                   | 20.9  |        | 29.0  | 21.1       |           | 43.1  | 43.1  |      | 27.1                     | 27.1 | 27.1 |
| Actuated g/C Ratio               | 0.32                                   | 0.23  |        | 0.32  | 0.23       |           | 0.48  | 0.48  |      | 0.30                     | 0.30 | 0.30 |
| Clearance Time (s)               | 6.1                                    | 6.1   |        | 6.1   | 6.1        |           | 5.9   | 5.9   |      | 5.9                      | 5.9  | 5.9  |
| Vehicle Extension (s)            | 3.0                                    | 3.0   |        | 3.0   | 3.0        |           | 3.0   | 3.0   |      | 3.0                      | 3.0  | 3.0  |
| Lane Grp Cap (vph)               | 251                                    | 406   |        | 251   | 454        |           | 315   | 920   |      | 89                       | 596  | 497  |
| v/s Ratio Prot                   | 0.05                                   | c0.31 |        | c0.09 | 0.20       |           | 0.15  | c0.57 |      |                          | 0.27 |      |
| v/s Ratio Perm                   | 0.14                                   |       |        | 0.23  |            |           | c0.48 |       |      | 0.01                     |      | 0.08 |
| v/c Ratio                        | 0.61                                   | 1.35  |        | 0.98  | 0.87       |           | 1.32  | 1.19  |      | 0.04                     | 0.89 | 0.26 |
| Uniform Delay, d1                | 23.9                                   | 34.6  |        | 27.6  | 33.1       |           | 32.5  | 23.4  |      | 22.3                     | 30.0 | 23.8 |
| Progression Factor               | 1.00                                   | 1.00  |        | 1.00  | 1.00       |           | 1.00  | 1.00  |      | 1.00                     | 1.03 | 1.02 |
| Incremental Delay, d2            | 4.4                                    | 174.1 |        | 51.0  | 16.5       |           | 164.9 | 95.0  |      | 0.9                      | 17.6 | 1.2  |
| Delay (s)                        | 28.3                                   | 208.6 |        | 78.7  | 49.6       |           | 197.4 | 118.5 |      | 23.1                     | 48.6 | 25.5 |
| Level of Service                 | С                                      | F     |        | E     | D          |           | - F   | F     |      | С                        | D    | С    |
| Approach Delay (s)               |  | 172.8 |        |       | 60.7       |           |       | 140.2 |      | a da cana a dana da sa k | 42.7 |      |
| Approach LOS                     |  | F     |        |       | E          |           |       | F     |      |                          | D    |      |
| Intersection Summary             |  |       |        |       |            |           |       |       |      |                          |      |      |
| HCM Average Control Delay        |  |       | 114.1  | H     | CM Level   | of Servic | e     |       | F    |                          |      |      |
| HCM Volume to Capacity ratio     | , ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |       | 1.27   |       |            |           |       |       |      |                          |      |      |
| Actuated Cycle Length (s)        |  |       | 90,0   | SI    | um of lost | time (s)  |       |       | 18.1 |                          |      |      |
| Intersection Capacity Utilizatio | n                                      |       | 117.3% |       | U Level o  |           |       |       | Н    |                          |      |      |
| Analysis Period (min)            |  |       | 15     |       |            |           |       |       |      |                          |      |      |
| - Oritical Lana Orayan           |  |       |        |       |            |           |       |       |      |                          |      |      |

|                                  | ≯    |              | ¥     | 1     |                | ×.                    | ٩     | Â     | p    | 1                   | Ļ    | 1    |
|----------------------------------|------|--------------|-------|-------|----------------|-----------------------|-------|-------|------|---------------------|------|------|
| Movement                         | EBL  | EBT          | EBR   | WBL   | WBT            | WBR                   | NBL   | NBT   | NBR  | SBL                 | SBT  | SBR  |
| Lane Configurations              | ሻ    | <b>ት</b> ፞፞፞ |       | ሻ     | <b>ት</b> ፞፞፞፝፝ |                       | ሻ     | Þ     |      | ኻ                   | 4    |      |
| Volume (vph)                     | 60   | 680          | 106   | 77    | 762            | 121                   | 122   | 470   | 43   | 80                  | 400  | 21   |
| Ideal Flow (vphpl)               | 2000 | 2000         | 2000  | 2000  | 2000           | 2000                  | 2000  | 2000  | 2000 | 2000                | 2000 | 2000 |
| Total Lost time (s)              | 6.0  | 6.0          |       | 6.0   | 6.0            |                       | 6.0   | 6.0   |      | 6.0                 | 6.0  |      |
| Lane Util. Factor                | 1.00 | 0.95         |       | 1.00  | 0.95           |                       | 1.00  | 1.00  |      | 1.00                | 1.00 |      |
| Frt                              | 1.00 | 0.98         |       | 1.00  | 0.98           |                       | 1.00  | 0.99  |      | 1.00                | 0.99 |      |
| Flt Protected                    | 0.95 | 1.00         |       | 0.95  | 1.00           |                       | 0.95  | 1.00  |      | 0.95                | 1.00 |      |
| Satd. Flow (prot)                | 1863 | 3650         |       | 1863  | 3649           |                       | 1863  | 1936  |      | 1863                | 1946 |      |
| Flt Permitted                    | 0.95 | 1.00         |       | 0.95  | 1.00           |                       | 0.95  | 1.00  |      | 0.95                | 1.00 |      |
| Satd. Flow (perm)                | 1863 | 3650         |       | 1863  | 3649           |                       | 1863  | 1936  |      | 1863                | 1946 |      |
| Peak-hour factor, PHF            | 0.90 | 0.90         | 0.90  | 0.92  | 0.92           | 0.92                  | 0.89  | 0.89  | 0.89 | 0.90                | 0.90 | 0.90 |
| Adj. Flow (vph)                  | 67   | 756          | 118   | 84    | 828            | 132                   | 137   | 528   | 48   | 89                  | 444  | 23   |
| RTOR Reduction (vph)             | 0    | 14           | 0     | 0     | 14             | 0                     | 0     | 4     | 0    | 0                   | 2    | 0    |
| Lane Group Flow (vph)            | 67   | 860          | 0     | 84    | 946            | 0                     | 137   | 572   | 0    | 89                  | 465  | 0    |
| Turn Type                        | Prot |              |       | Prot  |                |                       | Prot  |       |      | Prot                |      |      |
| Protected Phases                 | 5    | 2            |       | 1     | 6              |                       | 3     | 8     |      | 7                   | 4    |      |
| Permitted Phases                 |      |              |       |       |                |                       |       |       |      |                     |      |      |
| Actuated Green, G (s)            | 6.3  | 25.4         |       | 6.4   | 25.5           |                       | 9.5   | 26.6  |      | 7.6                 | 24.7 |      |
| Effective Green, g (s)           | 6.3  | 25.4         |       | 6.4   | 25.5           |                       | 9.5   | 26.6  |      | 7.6                 | 24.7 |      |
| Actuated g/C Ratio               | 0.07 | 0.28         |       | 0.07  | 0.28           |                       | 0.11  | 0.30  |      | 0.08                | 0.27 |      |
| Clearance Time (s)               | 6.0  | 6.0          |       | 6.0   | 6.0            |                       | 6.0   | 6.0   |      | 6.0                 | 6.0  |      |
| Vehicle Extension (s)            | 3.0  | 3.0          |       | 3.0   | 3.0            |                       | 3.0   | 3.0   |      | 3.0                 | 3.0  |      |
| Lane Grp Cap (vph)               | 130  | 1030         |       | 132   | 1034           |                       | 197   | 572   |      | 157                 | 534  |      |
| v/s Ratio Prot                   | 0.04 | 0.24         |       | c0.05 | c0.26          |                       | c0.07 | c0.30 |      | 0.05                | 0.24 |      |
| v/s Ratio Perm                   |      |              |       |       |                |                       |       |       |      |                     |      |      |
| v/c Ratio                        | 0.52 | 0.84         |       | 0.64  | 0.91           |                       | 0.70  | 1.00  |      | 0.57                | 0.87 |      |
| Uniform Delay, d1                | 40.4 | 30.3         |       | 40.7  | 31.2           |                       | 38.9  | 31.7  |      | 39.6                | 31.1 |      |
| Progression Factor               | 1.00 | 1.00         |       | 1.06  | 1.13           |                       | 1.34  | 0.68  |      | 1.00                | 1.00 |      |
| Incremental Delay, d2            | 3.4  | 8.0          |       | 6.2   | 9.5            |                       | 9.4   | 36.2  |      | 4.6                 | 14.4 |      |
| Delay (s)                        | 43.8 | 38.3         |       | 49.3  | 44.6           |                       | 61.4  | 57.7  |      | 44.2                | 45.5 |      |
| Level of Service                 | D    | D            |       | D     | D              |                       | Е     | Е     |      | D                   | D    |      |
| Approach Delay (s)               |      | 38.7         |       |       | 45.0           |                       |       | 58.4  |      |                     | 45.3 |      |
| Approach LOS                     |      | D            |       |       | D              |                       |       | Е     |      |                     | D    |      |
| Intersection Summary             |      |              |       |       |                |                       |       |       |      |                     |      |      |
| HCM Average Control Delay        |      |              | 46.2  | H     | CM Level       | of Servic             | e     |       | D    |                     |      |      |
| HCM Volume to Capacity ratio     |      |              | 0.78  |       |                |                       |       |       |      |                     |      |      |
| Actuated Cycle Length (s)        |      |              | 90.0  |       | um of lost     |                       |       |       | 12.0 | an yang ayaya sa sa |      |      |
| Intersection Capacity Utilizatio | n    |              | 81.3% | IC    | U Level c      | of Service            |       |       | D    |                     |      |      |
| Analysis Period (min)            |      |              | 15    |       |                | ta tini te strittirat |       |       |      |                     |      |      |
| c Critical Lane Group            |      |              |       |       |                |                       |       |       |      |                     |      |      |

|                                   | ٨    |                | $\mathbf{i}$ | <b>*</b> | 4             | Ł          | ٩    | Î            | p               | 1     | Ť     | 4    |
|-----------------------------------|------|----------------|--------------|----------|---------------|------------|------|--------------|-----------------|-------|-------|------|
| Movement                          | EBL  | EBT            | EBR          | WBL      | WBT           | WBR        | NBL  | NBT          | NBR             | SBL   | SBT   | SBR  |
| Lane Configurations               | ሻ    | 朴              |              | ሻ        | ŕ             | ٢          | ሻ    | <del>د</del> |                 | ሻ     | fə    |      |
| Volume (vph)                      | 18   | 982            | 101          | 261      | 876           | 464        | 220  | 82           | 323             | 344   | 156   | 40   |
| Ideal Flow (vphpl)                | 2000 | 2000           | 2000         | 2000     | 2000          | 2000       | 2000 | 2000         | 2000            | 2000  | 2000  | 2000 |
| Lane Width                        | 12   | 12             | 12           | 12       | 12            | 12         | 11   | 11           | 11              | 12    | 12    | 12   |
| Total Lost time (s)               | 6.1  | 6.1            |              | 6.1      | 6.1           | 6.1        | 6.0  | 6.0          |                 | 6.0   | 6.0   |      |
| Lane Util. Factor                 | 1.00 | 0.95           | 문문문          | 1.00     | 1.00          | 1.00       | 1.00 | 1.00         |                 | 1.00  | 1.00  |      |
| Frt                               | 1.00 | 0.99           |              | 1.00     | 1.00          | 0.85       | 1.00 | 0.88         |                 | 1.00  | 0.97  |      |
| Flt Protected                     | 0.95 | 1.00           |              | 0.95     | 1.00          | 1.00       | 0.95 | 1.00         |                 | 0.95  | 1.00  |      |
| Satd. Flow (prot)                 | 1863 | 3673           |              | 1863     | 1961          | 1500       | 1801 | 1669         |                 | 1863  | 1901  |      |
| Flt Permitted                     | 0.13 | 1.00           |              | 0.11     | 1.00          | 1.00       | 0.62 | 1.00         |                 | 0.14  | 1.00  |      |
| Satd. Flow (perm)                 | 262  | 3673           |              | 218      | 1961          | 1500       | 1184 | 1669         |                 | 280   | 1901  |      |
| Peak-hour factor, PHF             | 0.88 | 0.88           | 0.88         | 0.92     | 0.92          | 0.92       | 0.94 | 0.94         | 0.94            | 0.92  | 0.92  | 0.92 |
| Adj. Flow (vph)                   | 20   | 1116           | 115          | 284      | 952           | 504        | 234  | 87           | 344             | 374   | 170   | 43   |
| RTOR Reduction (vph)              | 0    | 9              | 0            | 0        | 0             | 233        | 0    | 0            | 0               | 0     | 10    | 0    |
| Lane Group Flow (vph)             | 20   | 1222           | 0            | 284      | 952           | 271        | 234  | 431          | 0               | 374   | 203   | 0    |
| Parking (#/hr)                    |      | 61913 <u>8</u> | 0            |          |               | 0          |      |              |                 |       |       |      |
| Turn Type                         | Perm |                |              | pm+pt    |               | Perm       | Perm |              |                 | pm+pt |       |      |
| Protected Phases                  |      | 2              |              | 1        | 5             |            |      | 8            |                 | ່ 7   | 4     |      |
| Permitted Phases                  | 2    |                |              | 5        |               | 5          | 8    |              | naatin talaalah | 4     |       |      |
| Actuated Green, G (s)             | 29.9 | 29.9           |              | 44.9     | 44.9          | 44.9       | 22.0 | 22.0         |                 | 33.0  | 33.0  |      |
| Effective Green, g (s)            | 29.9 | 29.9           |              | 44.9     | 44.9          | 44.9       | 22.0 | 22.0         |                 | 33.0  | 33.0  |      |
| Actuated g/C Ratio                | 0.33 | 0.33           |              | 0.50     | 0.50          | 0.50       | 0.24 | 0.24         |                 | 0.37  | 0.37  |      |
| Clearance Time (s)                | 6.1  | 6.1            |              | 6.1      | 6.1           | 6.1        | 6.0  | 6.0          |                 | 6.0   | 6.0   |      |
| Vehicle Extension (s)             | 3.0  | 3.0            |              | 3.0      | 3.0           | 3.0        | 3.0  | 3.0          |                 | 3.0   | 3.0   |      |
| Lane Grp Cap (vph)                | 87   | 1220           |              | 271      | 978           | 748        | 289  | 408          |                 | 191   | 697   |      |
| v/s Ratio Prot                    |      | 0.33           |              | 0.10     | c0.49         |            |      | 0.26         |                 | c0.11 | 0.11  |      |
| v/s Ratio Perm                    | 0.08 | . 195655.0     |              | c0.42    | ALL DIMENTALI | 0.18       | 0.20 |              |                 | c0.61 |       |      |
| v/c Ratio                         | 0.23 | 1.00           |              | 1.05     | 0.97          | 0.36       | 0.81 | 1.06         |                 | 1.96  | 0.29  |      |
| Uniform Delay, d1                 | 21.7 | 30.1           |              | 24.0     | 22.0          | 13.8       | 32.0 | 34.0         |                 | 27.0  | 20.2  |      |
| Progression Factor                | 1.08 | 0.93           |              | 1.00     | 1.00          | 1.00       | 1.00 | 1.00         |                 | 1.00  | 1.00  |      |
| Incremental Delay, d2             | 5.6  | 25.2           |              | 67.8     | 22.4          | 0.3        | 15.3 | 60.2         |                 | 449.6 | 0.2   |      |
| Delay (s)                         | 29.1 | 53.1           |              | 91.8     | 44.3          | 14.1       | 47.3 | 94.2         |                 | 476.6 | 20.4  |      |
| Level of Service                  | С    | D              |              | F        | D             | В          | D    | F            |                 | F     | С     |      |
| Approach Delay (s)                |      | 52.7           |              |          | 43.3          |            |      | 77.7         |                 |       | 311.1 |      |
| Approach LOS                      |      | D              |              |          | D             |            |      | E            |                 |       | F     |      |
| Intersection Summary              |      |                |              |          |               |            |      |              |                 |       |       |      |
| HCM Average Control Delay         |      |                | 88.5         | Н        | CM Level      | of Servic  | e    |              | F               |       |       |      |
| HCM Volume to Capacity ratio      |      |                | 1.35         |          |               |            |      |              |                 |       |       |      |
| Actuated Cycle Length (s)         |      |                | 90.0         | S        | um of lost    | time (s)   |      |              | 12.1            |       |       |      |
| Intersection Capacity Utilization |      |                | 113.4%       | IC       | U Level o     | of Service |      |              | Н               |       |       |      |
| Analysis Period (min)             |      |                | 15           |          |               |            |      |              |                 |       |       |      |
| c Critical Lane Group             |      |                |              |          |               |            |      |              |                 |       | 걸렸다.  |      |

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|-------------------------------|-------|-------|-------|------|------------|------------|-------|------|------|-------|------|------|
| Movement                      | EBL   | EBT   | EBR   | WBL  | WBT        | WBR        | NBL   | NBT  | NBR  | SBL   | SBT  | SBR  |
| Lane Configurations           | ኻኻ    | 个     | ሻ     | ኻኻ   | f          | ŕ          | ሻ     | 朴    |      | ሻ     | ትት   | ۴    |
| Volume (vph)                  | 287   | 185   | 125   | 182  | 51         | 99         | 122   | 467  | 341  | 425   | 923  | 136  |
| Ideal Flow (vphpl)            | 2000  | 2000  | 2000  | 2000 | 2000       | 2000       | 2000  | 2000 | 2000 | 2000  | 2000 | 2000 |
| Total Lost time (s)           | 6.0   | 6.0   | 6.0   | 6.0  | 6.0        | 6.0        | 6.6   | 6.6  |      | 6.6   | 6.6  | 6.6  |
| Lane Util. Factor             | 0.97  | 1.00  | 1.00  | 0.97 | 1.00       | 1.00       | 1.00  | 0.95 |      | 1.00  | 0.95 | 1.00 |
| Frt                           | 1.00  | 1.00  | 0.85  | 1.00 | 1.00       | 0.85       | 1.00  | 0.94 |      | 1.00  | 1.00 | 0.85 |
| Flt Protected                 | 0.95  | 1.00  | 1.00  | 0.95 | 1.00       | 1.00       | 0.95  | 1.00 |      | 0.95  | 1.00 | 1.00 |
| Satd. Flow (prot)             | 3614  | 1961  | 1667  | 3614 | 1961       | 1667       | 1863  | 3490 |      | 1863  | 3725 | 1667 |
| Flt Permitted                 | 0.95  | 1.00  | 1.00  | 0.95 | 1.00       | 1.00       | 0.22  | 1.00 |      | 0.14  | 1.00 | 1.00 |
| Satd. Flow (perm)             | 3614  | 1961  | 1667  | 3614 | 1961       | 1667       | 440   | 3490 |      | 275   | 3725 | 1667 |
| Peak-hour factor, PHF         | 0.92  | 0.92  | 0.92  | 0.92 | 0.92       | 0.92       | 0.92  | 0.92 | 0.92 | 0.92  | 0.92 | 0.92 |
| Adj. Flow (vph)               | 312   | 201   | 136   | 198  | 55         | 108        | 133   | 508  | 371  | 462   | 1003 | 148  |
| RTOR Reduction (vph)          | 0     | 0     | 113   | 0    | 0          | 94         | 0     | 145  | 0    | 0     | 0    | 55   |
| Lane Group Flow (vph)         | 312   | 201   | 23    | 198  | 55         | 14         | 133   | 734  | 0    | 462   | 1003 | 93   |
| Turn Type                     | Prot  |       | Perm  | Prot |            | Perm       | pm+pt |      |      | pm+pt |      | Perm |
| Protected Phases              | 7     | 4     |       | 3    | 8          |            | 5     | 2    |      | 1     | 6    |      |
| Permitted Phases              |       |       | 4     |      |            | 8          | 2     |      |      | 6     |      | 6    |
| Actuated Green, G (s)         | 11.2  | 14.8  | 14.8  | 7.9  | 11.5       | 11.5       | 29.2  | 21.9 |      | 47.4  | 33.5 | 33.5 |
| Effective Green, g (s)        | 11.2  | 14.8  | 14.8  | 7.9  | 11.5       | 11.5       | 29.2  | 21.9 |      | 47.4  | 33.5 | 33.5 |
| Actuated g/C Ratio            | 0.13  | 0.17  | 0.17  | 0.09 | 0.13       | 0.13       | 0,33  | 0.25 |      | 0.53  | 0.38 | 0.38 |
| Clearance Time (s)            | 6.0   | 6.0   | 6.0   | 6.0  | 6.0        | 6.0        | 6.6   | 6.6  |      | 6.6   | 6.6  | 6.6  |
| Vehicle Extension (s)         | 3.0   | 3.0   | 3.0   | 3.0  | 3.0        | 3.0        | 3.0   | 3.0  |      | 3.0   | 3.0  | 3.0  |
| Lane Grp Cap (vph)            | 456   | 327   | 278   | 322  | 254        | 216        | 262   | 862  |      | 485   | 1407 | 630  |
| v/s Ratio Prot                | c0.09 | c0.10 |       | 0.05 | 0.03       |            | 0.04  | 0.21 |      | c0.20 | 0.27 |      |
| v/s Ratio Perm                |       |       | 0.01  |      |            | 0.01       | 0.13  |      |      | c0.31 |      | 0.06 |
| v/c Ratio                     | 0.68  | 0.61  | 0.08  | 0.61 | 0.22       | 0.06       | 0.51  | 0.85 |      | 0.95  | 0.71 | 0.15 |
| Uniform Delay, d1             | 37.1  | 34.3  | 31.2  | 38.9 | 34.6       | 33.9       | 21.7  | 31.8 |      | 24.2  | 23.5 | 18.2 |
| Progression Factor            | 1.00  | 1.00  | 1.00  | 1.00 | 1.00       | 1.00       | 1.00  | 1.00 |      | 1.00  | 1.00 | 1.00 |
| Incremental Delay, d2         | 4.2   | 3.4   | 0.1   | 3.5  | 0.4        | 0.1        | 1.5   | 10.3 |      | 29.0  | 3.1  | 0.5  |
| Delay (s)                     | 41.3  | 37.7  | 31.3  | 42.4 | 35.0       | 34.0       | 23.2  | 42.2 |      | 53.3  | 26.6 | 18.7 |
| Level of Service              | D     | D     | С     | D    | С          | С          | С     | D    |      | D     | С    | В    |
| Approach Delay (s)            |       | 38.1  |       |      | 38.8       |            |       | 39.7 |      |       | 33.5 |      |
| Approach LOS                  |       | D     |       |      | D          |            |       | D    |      |       | С    |      |
| Intersection Summary          |       |       |       |      | -          |            |       |      |      |       |      |      |
| HCM Average Control Delay     |       |       | 36.6  | H    | CM Level   | of Service | ce    |      | D    |       |      |      |
| HCM Volume to Capacity ra     | tio   |       | 0.84  |      |            |            |       |      |      |       |      |      |
| Actuated Cycle Length (s)     |       |       | 88.7  |      | um of lost |            |       |      | 18.6 |       |      |      |
| Intersection Capacity Utiliza | tion  |       | 82.1% | IC   | U Level o  | of Service | •     |      | Е    |       |      |      |
| Analysis Period (min)         |       |       | 15    |      |            |            |       |      |      |       |      |      |
| c Critical Lane Group         |       |       |       |      |            |            |       |      |      |       |      |      |

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|---------------------------------|-------------|-----------------|------------|-------------|------------|--------------------|------------|-----------------------|-------------------|---------------------------------------|------------|------|
| Movement                        | EBL         | EBT             | EBR        | WBL         | WBT        | WBR                | NBL        | NBT                   | NBR               | SBL                                   | SBT        | SBR  |
| Lane Configurations             | ۴           | ቶ               | ក៍         | ٢           | <b>Å</b>   |                    | ٢          | ₽                     |                   | ሻ                                     | Ť          | *    |
| Volume (vph)                    | 183         | 196             | 311        | 225         | 87         | 82                 | 195        | 480                   | 69                | 3                                     | 767        | 37   |
| Ideal Flow (vphpl)              | 2000        | 2000            | 2000       | 2000        | 2000       | 2000               | 2000       | 2000                  | 2000              | 2000                                  | 2000       | 2000 |
| Total Lost time (s)             | 6.1         | 6.1             | 5.9        | 6.1         | 6.1        |                    | 5.9        | 5.9                   |                   | 5.9                                   | 5.9        | 5.9  |
| Lane Util. Factor               | 1.00        | 1.00            | 1.00       | 1.00        | 1.00       |                    | 1.00       | 1.00                  |                   | 1.00                                  | 1.00       | 1.00 |
| Frt                             | 1.00        | 1.00            | 0.85       | 1.00        | 0.93       |                    | 1.00       | 0.98                  |                   | 1.00                                  | 1.00       | 0.85 |
| Flt Protected                   | 0.95        | 1.00            | 1.00       | 0.95        | 1.00       |                    | 0.95       | 1.00                  |                   | 0.95                                  | 1.00       | 1.00 |
| Satd. Flow (prot)               | 1881        | 2000            | 1619       | 1863        | 1826       |                    | 1743       | 1908                  |                   | 1900                                  | 1980       | 1650 |
| Flt Permitted                   | 0.38        | 1.00            | 1.00       | 0.35        | 1.00       |                    | 0.09       | 1.00                  |                   | 0.16                                  | 1.00       | 1.00 |
| Satd. Flow (perm)               | 747         | 2000            | 1619       | 677         | 1826       |                    | 173        | 1908                  |                   | 312                                   | 1980       | 1650 |
| Peak-hour factor, PHF           | 0.81        | 0.81            | 0.81       | 0.73        | 0.73       | 0.73               | 0.74       | 0.74                  | 0.74              | 0.84                                  | 0.84       | 0.84 |
| Adj. Flow (vph)                 | 226         | 242             | 384        | 308         | 119        | 112                | 264        | 649                   | 93                | 4                                     | 913        | 44   |
| RTOR Reduction (vph)            | 0           | 0               | 40         | 000         | 38         | 0                  | 0          | 6                     | 0                 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0          | 14   |
| Lane Group Flow (vph)           | 226         | 242             | 344        | 308         | 193        | ŏ                  | 264        | 736                   | ō                 | 4                                     | 913        | 30   |
| Heavy Vehicles (%)              | 1%          | 0%              | 5%         | 2%          | 3%         | 0%                 | 9%         | 2%                    | 9%                | 0%                                    | 1%         | 3%   |
| Turn Type                       | pm+pt       | 070             | pm+ov      | pm+pt       | 070        | 070                | pm+pt      |                       | 070               | Perm                                  |            | Perm |
| Protected Phases                | րուրլ<br>7  | 4 (1997)<br>4   | 5 piniov   | 911191<br>3 | 8          |                    | рш-рс<br>5 | 2                     |                   | CI CIII                               | 6          |      |
| Permitted Phases                | 4           | т<br>96.699.696 | 4          | 8           |            |                    | 2          | <b>_</b><br>1993-1993 |                   | 6                                     |            | 6    |
| Actuated Green, G (s)           | 21.3        | 13.4            | 21.5       | 21.3        | 13.4       | entra en el com    | 50.6       | 50.6                  |                   | 36.6                                  | 36.6       | 36.6 |
| Effective Green, g (s)          | 21.3        | 13.4            | 21.5       | 21.3        | 13.4       |                    | 50.6       | 50.6                  |                   | 36.6                                  | 36.6       | 36.6 |
| Actuated g/C Ratio              | 0.24        | 0.15            | 0.24       | 0.24        | 0.15       | 8.588.510,9.00<br> | 0.56       | 0.56                  |                   | 0.41                                  | 0.41       | 0.41 |
| Clearance Time (s)              | 0.24<br>6.1 | 6.1             | 5.9        | 6.1         | 6.1        |                    | 5.9        | 5.9                   |                   | 5.9                                   | 5.9        | 5.9  |
|                                 | 0.1<br>3.0  |                 | 3.9<br>3.0 | 0.1<br>3.0  | 0.1<br>3.0 |                    | 3.0        | 3.0                   |                   | 3.0                                   | 3.9<br>3.0 | 3.0  |
| Vehicle Extension (s)           |             | 3.0             |            |             |            |                    |            |                       | s and the country |                                       |            |      |
| Lane Grp Cap (vph)              | 276         | 298             | 387        | 264         | 272        |                    | 239        | 1073                  |                   | 127                                   | 805        | 671  |
| v/s Ratio Prot                  | 0.07        | 0.12            | 0.08       | c0.10       | 0.11       |                    | c0.10      | 0.39                  |                   |                                       | 0.46       |      |
| v/s Ratio Perm                  | 0.12        |                 | 0.13       | c0.17       |            |                    | c0.52      |                       |                   | 0.01                                  |            | 0.02 |
| v/c Ratio                       | 0.82        | 0.81            | 0.89       | 1.17        | 0.71       |                    | 1.10       | 0.69                  |                   | 0.03                                  | 1.13       | 0.05 |
| Uniform Delay, d1               | 30.8        | 37.1            | 33.1       | 32.8        | 36.4       |                    | 36.9       | 14.0                  |                   | 16.0                                  | 26.7       | 16.1 |
| Progression Factor              | 1.00        | 1.00            | 1.00       | 1.00        | 1.00       |                    | 1.00       | 1.00                  |                   | 0.77                                  | 0.84       | 0.67 |
| Incremental Delay, d2           | 17.0        | 15.4            | 21.0       | 108.1       | 8.2        |                    | 89.1       | 3.6                   |                   | 0.4                                   | 75.1       | 0.1  |
| Delay (s)                       | 47.8        | 52.5            | 54.1       | 140.9       | 44.6       |                    | 126.0      | 17.6                  |                   | 12.8                                  | 97.6       | 10.9 |
| Level of Service                | D           | D               | D          | , F         | D          |                    | F          | В                     |                   | В                                     | F          | В    |
| Approach Delay (s)              |             | 52.0            |            |             | 99.6       |                    |            | 46.1                  |                   |                                       | 93.3       |      |
| Approach LOS                    |             | D               |            |             | S F        |                    |            | D                     |                   |                                       | State Fra  |      |
| Intersection Summary            |             |                 |            |             |            |                    |            |                       |                   |                                       |            |      |
| HCM Average Control Delay       |             |                 | 69.7       | H           | CM Level   | of Servic          | )e         |                       | Е                 |                                       |            |      |
| HCM Volume to Capacity rat      |             |                 | 1.09       |             |            |                    |            |                       |                   |                                       |            |      |
| Actuated Cycle Length (s)       |             |                 | 90.0       | S           | um of lost | time (s)           |            |                       | 18.1              |                                       |            |      |
| Intersection Capacity Utilizati | ion         |                 | 90.3%      |             | U Level o  |                    | )          |                       | E                 |                                       |            |      |
| Analysis Period (min)           |             |                 | 15         |             |            |                    |            |                       |                   |                                       |            |      |
| o Critical Long Group           |             |                 |            |             |            |                    |            |                       |                   |                                       |            |      |

|  | ٨     |                     | >     | *                 | 4              | Ł          | ٩     | <b>Å</b> | 1    | 6    | ţ     | ~    |
|--|-------|---------------------|-------|-------------------|----------------|------------|-------|----------|------|------|-------|------|
| Movement                                       | EBL   | EBT                 | EBR   | WBL               | WBT            | WBR        | NBL   | NBT      | NBR  | SBL  | SBT   | SBR  |
| Lane Configurations                            | ሻ     | ተኈ                  |       | ٦.                | <b>ት</b> ፞፞፝፝፝ |            | ኻ     | 1≽       |      | ኻ    | ₿     |      |
| Volume (vph)                                   | 22    | 687                 | 120   | 34                | 582            | 14         | 83    | 222      | 50   | 51   | 486   | 12   |
| Ideal Flow (vphpl)                             | 2000  | 2000                | 2000  | 2000              | 2000           | 2000       | 2000  | 2000     | 2000 | 2000 | 2000  | 2000 |
| Total Lost time (s)                            | 6.0   | 6.0                 |       | 6.0               | 6.0            |            | 6.0   | 6.0      |      | 6.0  | 6.0   |      |
| Lane Util. Factor                              | 1.00  | 0.95                |       | 1.00              | 0.95           |            | 1.00  | 1.00     |      | 1.00 | 1.00  |      |
| Frt  | 1.00  | 0.98                |       | 1.00              | 1.00           |            | 1.00  | 0.97     |      | 1.00 | 1.00  |      |
| Flt Protected                                  | 0.95  | 1.00                |       | 0.95              | 1.00           |            | 0.95  | 1.00     |      | 0.95 | 1.00  |      |
| Satd. Flow (prot)                              | 1863  | 3642                |       | 1863              | 3712           |            | 1863  | 1906     |      | 1863 | 1954  |      |
| FIt Permitted                                  | 0.95  | 1.00                |       | 0.95              | 1.00           |            | 0.95  | 1.00     |      | 0.95 | 1.00  |      |
| Satd. Flow (perm)                              | 1863  | 3642                |       | 1863              | 3712           |            | 1863  | 1906     |      | 1863 | 1954  |      |
| Peak-hour factor, PHF                          | 0.79  | 0.79                | 0.79  | 0.70              | 0.70           | 0.70       | 0.95  | 0.95     | 0.95 | 0.81 | 0.81  | 0.81 |
| Adj. Flow (vph)                                | 28    | 870                 | 152   | 49                | 831            | 20         | 87    | 234      | 53   | 63   | 600   | 15   |
| RTOR Reduction (vph)                           | 0     | 15                  | 0     | 0                 | 1              | 0          | 0     | 9        | 0    | 0    | 1     | 0    |
| Lane Group Flow (vph)                          | 28    | 1007                | 0     | 49                | 850            | 0          | 87    | 278      | 0    | 63   | 614   | 0    |
| Turn Type                                      | Prot  |                     |       | Prot              |                |            | Prot  |          |      | Prot |       |      |
| Protected Phases                               | 5     | 2                   |       | 1                 | 6              |            | 3     | 8        |      | 7    | 4     |      |
| Permitted Phases                               |       | lin Africa di Maria |       |                   |                |            |       |          |      |      |       |      |
| Actuated Green, G (s)                          | 3.1   | 26.1                |       | 4.7               | 27.7           |            | 5.6   | 29.6     |      | 5.6  | 29.6  |      |
| Effective Green, g (s)                         | 3.1   | 26.1                |       | 4.7               | 27.7           |            | 5.6   | 29.6     |      | 5.6  | 29.6  |      |
| Actuated g/C Ratio                             | 0.03  | 0.29                |       | 0.05              | 0.31           |            | 0.06  | 0.33     |      | 0.06 | 0.33  |      |
| Clearance Time (s)                             | 6.0   | 6.0                 |       | 6.0               | 6.0            |            | 6.0   | 6.0      |      | 6.0  | 6.0   |      |
| Vehicle Extension (s)                          | 3.0   | 3.0                 |       | 3.0               | 3.0            |            | 3.0   | 3.0      |      | 3.0  | 3.0   |      |
| Lane Grp Cap (vph)                             | 64    | 1056                |       | 97                | 1142           |            | 116   | 627      |      | 116  | 643   |      |
| v/s Ratio Prot                                 | 0.02  | c0.28               |       | c0.03             | 0.23           |            | c0.05 | 0.15     |      | 0.03 | c0.31 |      |
| v/s Ratio Perm                                 |       |                     |       |                   |                |            |       |          |      |      |       |      |
| v/c Ratio                                      | 0.44  | 0.95                |       | 0.51              | 0.74           |            | 0.75  | 0.44     |      | 0.54 | 0.95  |      |
| Uniform Delay, d1                              | 42.6  | 31.4                |       | 41.5              | 28.0           |            | 41.5  | 23.7     |      | 41.0 | 29.5  |      |
| Progression Factor                             | 1.00  | 1.00                |       | 0.78              | 1.20           |            | 0.92  | 1.02     |      | 1.00 | 1.00  |      |
| Incremental Delay, d2                          | 4.7   | 18.6                |       | 3.9               | 4.2            |            | 23.0  | 0.5      |      | 5.1  | 24.5  |      |
| Delay (s)                                      | 47.3  | 49.9                |       | 36.1              | 37.7           |            | 61.0  | 24.6     |      | 46.1 | 54.1  |      |
| Level of Service                               | D     | D                   |       | D                 | D              |            | Е     | С        |      | D    | D     |      |
| Approach Delay (s)                             |       | 49.9                |       |                   | 37.6           |            |       | 33.1     |      |      | 53.3  |      |
| Approach LOS                                   |       | D                   |       |                   | D              |            |       | С        |      |      | D     |      |
| Intersection Summary                           |       |                     |       |                   |                |            |       |          | _    |      |       |      |
| HCM Average Control Delay                      |       |                     | 44.9  | H                 | CM Level       | of Servic  | e     |          | D    |      |       |      |
| HCM Volume to Capacity ratio                   |       |                     | 0.90  | <u>arasatar</u> i | 경험관리를          |            |       |          |      |      |       |      |
| Actuated Cycle Length (s)                      |       |                     | 90.0  |                   | um of lost     |            |       |          | 24.0 |      |       |      |
| Intersection Capacity Utilization              | 12933 |                     | 72.7% | IC                | U Level o      | of Service |       |          | С    |      |       |      |
| Analysis Period (min)<br>c Critical Lane Group |       |                     | 15    |                   |                |            |       |          |      |      |       |      |
|  |       |                     |       |                   |                |            |       |          |      |      |       |      |

|                                   | ≯   | >       | $\mathbf{k}$ | 1     | <b>4</b>   | Ł                              | ٩    | <b>Å</b> | p     | \$    | ₩<br>₩   | ~     |
|-----------------------------------|---|---------|--------------|-------|------------|--------------------------------|------|----------|-------|-------|----------|-------|
| Movement                          | EBL   | EBT     | EBR          | WBL   | WBT        | WBR                            | NBL  | NBT      | NBR   | SBL   | SBT      | SBR   |
| Lane Configurations               | ሻ   | 朴       |              | ሻ     | <b>ት</b> ኩ |                                | ሻ    | Å        | ۴     | ሻ     | <b>A</b> | ሻ     |
| Volume (vph)                      | 5   | 711     | 186          | 235   | 746        | 135                            | 61   | 25       | 251   | 212   | 48       | 12    |
| Ideal Flow (vphpl)                | 2000  | 2000    | 2000         | 2000  | 2000       | 2000                           | 2000 | 2000     | 2000  | 2000  | 2000     | 2000  |
| Lane Width                        | 12  | 12      | 12           | 12    | 12         | 12                             | 11   | 11       | 11    | 12    | 12       | 12    |
| Total Lost time (s)               | 6.1   | 6.1     |              | 6.1   | 6.1        |                                | 6.0  | 6.0      | 6.1   | 6.0   | 6.0      | 6.0   |
| Lane Util. Factor                 | 1.00  | 0.95    |              | 1.00  | 0.95       |                                | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  |
| Frt                               | 1.00  | 0.97    |              | 1.00  | 0.98       |                                | 1.00 | 1.00     | 0.85  | 1.00  | 1.00     | 0.85  |
| Fit Protected                     | 0.95  | 1.00    |              | 0.95  | 1.00       |                                | 0.95 | 1.00     | 1.00  | 0.95  | 1.00     | 1.00  |
| Satd. Flow (prot)                 | 1863  | 3610    |              | 1863  | 3640       | a di generale e de la compañía | 1801 | 1895     | 1611  | 1863  | 1961     | 1667  |
| Flt Permitted                     | 0.27  | 1.00    |              | 0.10  | 1.00       |                                | 0.72 | 1.00     | 1.00  | 0.47  | 1.00     | 1.00  |
| Satd. Flow (perm)                 | 528   | 3610    |              | 204   | 3640       |                                | 1356 | 1895     | 1611  | 930   | 1961     | 1667  |
| Peak-hour factor, PHF             | 0.76  | 0.76    | 0.76         | 0.83  | 0.83       | 0.83                           | 0.83 | 0.83     | 0.83  | 0.75  | 0.75     | 0.75  |
| Adj. Flow (vph)                   | 7   | 936     | 245          | 283   | 899        | 163                            | 73   | 30       | 302   | 283   | 64       | 16    |
| RTOR Reduction (vph)              | 0   | 24      |              |       | 13         | 0                              | 0    | 0        | 0     |       | 0        | 12    |
| Lane Group Flow (vph)             | 7   | 1157    | 0            | 283   | 1049       | 0                              | 73   | 30       | 302   | 283   | 64       | <br>4 |
| Parking (#/hr)                    |   |         | 0            |       |            | Õ                              |      |          |       |       |          |       |
| Turn Type                         | Perm  |         |              | pm+pt |            |                                | Perm |          | pm+ov | pm+pt |          | Perm  |
| Protected Phases                  |   | 2       |              | 1     | 6          |                                |      | 8        | 1     | 7     | 4        |       |
| Permitted Phases                  | 2   |         |              | 6     |            |                                | 8    |          | 8     | 4     |          | 4     |
| Actuated Green, G (s)             | 32.4  | 32.4    |              | 53.5  | 53.5       |                                | 10.8 | 10.8     | 25.8  | 24.4  | 24.4     | 24.4  |
| Effective Green, g (s)            | 32.4  | 32.4    |              | 53.5  | 53.5       |                                | 10.8 | 10.8     | 25.8  | 24.4  | 24.4     | 24.4  |
| Actuated g/C Ratio                | 0.36  | 0.36    |              | 0.59  | 0.59       |                                | 0.12 | 0.12     | 0.29  | 0.27  | 0.27     | 0.27  |
| Clearance Time (s)                | 6.1   | 6.1     |              | 6.1   | 6.1        |                                | 6.0  | 6.0      | 6.1   | 6.0   | 6.0      | 6.0   |
| Vehicle Extension (s)             | 3.0   | 3.0     |              | 3.0   | 3.0        |                                | 3.0  | 3.0      | 3.0   | 3.0   | 3.0      | 3.0   |
| Lane Grp Cap (vph)                | 190   | 1300    |              | 398   | 2164       |                                | 163  | 227      | 462   | 331   | 532      | 452   |
| v/s Ratio Prot                    |   | c0.32   |              | c0.12 | 0.29       |                                |      | 0.02     | 0.11  | c0.07 | 0.03     |       |
| v/s Ratio Perm                    | 0.01  |         |              | 0.30  |            |                                | 0.05 |          | 0.08  | c0.16 |          | 0.00  |
| v/c Ratio                         | 0.04  | 0.89    |              | 0.71  | 0.48       |                                | 0.45 | 0.13     | 0.65  | 0.85  | 0.12     | 0.01  |
| Uniform Delay, d1                 | 18.7  | 27.1    |              | 21.0  | 10.4       |                                | 36.8 | 35.4     | 28.2  | 30.6  | 24.7     | 24.0  |
| Progression Factor                | 0.76  | 0.95    |              | 1.00  | 1,00       |                                | 1.00 | 1.00     | 1.00  | 1.00  | 1.00     | 1.00  |
| Incremental Delay, d2             | 0.3   | 8.6     |              | 5.9   | 0.8        |                                | 2.0  | 0.3      | 3.3   | 18.9  | 0.1      | 0.0   |
| Delay (s)                         | 14.6  | 34.3    |              | 26.9  | 11.2       |                                | 38.8 | 35.7     | 31.5  | 49.4  | 24.8     | 24.0  |
| Level of Service                  | В   | С       |              | С     | В          |                                | D    | D        | С     | D     | С        | С     |
| Approach Delay (s)                |   | 34.2    |              |       | 14.5       |                                |      | 33.1     |       |       | 44.0     |       |
| Approach LOS                      |   | С       |              |       | В          |                                |      | С        |       |       | D        |       |
| Intersection Summary              |   |         |              |       |            |                                |      |          |       |       |          |       |
| HCM Average Control Delay         | a faith | <u></u> | 27.1         | Н     | CM Level   | of Servic                      | е    |          | С     |       |          |       |
| HCM Volume to Capacity ratio      |   |         | 0.82         |       |            |                                |      |          |       |       |          |       |
| Actuated Cycle Length (s)         |   |         | 90.0         | Sı    | im of lost | time (s)                       |      |          | 18.2  |       |          |       |
| Intersection Capacity Utilization |   |         | 69.7%        |       |            | of Service                     |      |          | С     |       |          |       |
| Analysis Period (min)             |   |         | 15           |       |            |                                |      |          |       |       |          |       |
| c Critical Lane Group             |   |         |              |       |            |                                |      |          |       |       |          |       |

|                               | ٨     | >    | ~     | 1    | 4          | Ł          | 1           | ↑          | p    | 1     | ļ     | 4    |
|-------------------------------|-------|------|-------|------|------------|------------|-------------|------------|------|-------|-------|------|
| Movement                      | EBL   | EBT  | EBR   | WBL  | WBT        | WBR        | NBL         | NBT        | NBR  | SBL   | SBT   | SBR  |
| Lane Configurations           | ሻሻ    | ቶ    | ሻ     | ኻኻ   | ŕ          | 7          | ħ           | <u></u> ↑₽ |      | 1     | ትት    | 7    |
| Volume (vph)                  | 721   | 175  | 411   | 554  | 170        | 341        | 87          | 469        | 163  | 188   | 750   | 165  |
| Ideal Flow (vphpl)            | 2000  | 2000 | 2000  | 2000 | 2000       | 2000       | 2000        | 2000       | 2000 | 2000  | 2000  | 2000 |
| Total Lost time (s)           | 6.0   | 6.0  | 6.0   | 6.0  | 6.0        | 6.0        | 6.6         | 6.6        |      | 6.6   | 6.6   | 6.6  |
| Lane Util. Factor             | 0.97  | 1.00 | 1.00  | 0.97 | 1.00       | 1.00       | 1.00        | 0.95       |      | 1.00  | 0.95  | 1.00 |
| Frt                           | 1.00  | 1.00 | 0.85  | 1.00 | 1.00       | 0.85       | 1.00        | 0.96       |      | 1.00  | 1.00  | 0.85 |
| FIt Protected                 | 0.95  | 1.00 | 1.00  | 0.95 | 1.00       | 1.00       | 0.95        | 1.00       |      | 0.95  | 1.00  | 1.00 |
| Satd. Flow (prot)             | 3614  | 1961 | 1667  | 3614 | 1961       | 1667       | 1863        | 3582       |      | 1863  | 3725  | 1667 |
| Flt Permitted                 | 0.95  | 1.00 | 1.00  | 0.95 | 1.00       | 1.00       | 0.21        | 1.00       |      | 0.20  | 1.00  | 1.00 |
| Satd. Flow (perm)             | 3614  | 1961 | 1667  | 3614 | 1961       | 1667       | 415         | 3582       |      | 383   | 3725  | 1667 |
| Peak-hour factor, PHF         | 0.92  | 0.92 | 0.92  | 0.92 | 0.92       | 0.92       | 0.92        | 0.92       | 0.92 | 0.92  | 0.92  | 0.92 |
| Adj. Flow (vph)               | 784   | 190  | 447   | 602  | 185        | 371        | 95          | 510        | 177  | 204   | 815   | 179  |
| RTOR Reduction (vph)          | 0     | 0    | 154   | 0    | 0          | 158        | 0           | 37         | 0    | 0     | 0     | 79   |
| Lane Group Flow (vph)         | 784   | 190  | 293   | 602  | 185        | 213        | 95          | 650        | 0    | 204   | 815   | 100  |
| Turn Type                     | Prot  |      | Perm  | Prot |            | Perm       | pm+pt       |            |      | pm+pt |       | Perm |
| Protected Phases              | 7     | 4    |       | 3    | 8          |            | 5           | 2          |      | 1     | 6     |      |
| Permitted Phases              |       |      | 4     |      |            | 8          | 2           |            |      | 6     |       | 6    |
| Actuated Green, G (s)         | 20.6  | 18.0 | 18.0  | 18.6 | 16.0       | 16.0       | 24.7        | 18.9       |      | 27.9  | 20.5  | 20.5 |
| Effective Green, g (s)        | 20.6  | 18.0 | 18.0  | 18.6 | 16.0       | 16.0       | 24.7        | 18.9       |      | 27.9  | 20.5  | 20.5 |
| Actuated g/C Ratio            | 0.23  | 0.20 | 0.20  | 0.21 | 0.18       | 0.18       | 0.28        | 0.21       |      | 0.32  | 0.23  | 0.23 |
| Clearance Time (s)            | 6.0   | 6.0  | 6.0   | 6.0  | 6.0        | 6.0        | 6.6         | 6.6        |      | 6.6   | 6.6   | 6.6  |
| Vehicle Extension (s)         | 3.0   | 3.0  | 3.0   | 3.0  | 3.0        | 3.0        | 3.0         | 3.0        |      | 3.0   | 3.0   | 3.0  |
| Lane Grp Cap (vph)            | 845   | 401  | 341   | 763  | 356        | 303        | 212         | 768        |      | 246   | 867   | 388  |
| v/s Ratio Prot                | c0.22 | 0.10 |       | 0.17 | 0.09       |            | 0.03        | 0.18       |      | c0.07 | c0.22 |      |
| v/s Ratio Perm                |       |      | c0.18 |      |            | 0.13       | 0.10        |            |      | 0.19  |       | 0.06 |
| v/c Ratio                     | 0.93  | 0.47 | 0.86  | 0.79 | 0.52       | 0,70       | 0.45        | 0.85       |      | 0.83  | 0.94  | 0.26 |
| Uniform Delay, d1             | 33.0  | 30.9 | 33.8  | 32.9 | 32.6       | 33.8       | 25.1        | 33.2       |      | 24.2  | 33.2  | 27.6 |
| Progression Factor            | 1.00  | 1.00 | 1.00  | 1.00 | 1.00       | 1.00       | 1.00        | 1.00       |      | 1.00  | 1.00  | 1.00 |
| Incremental Delay, d2         | 16.0  | 0.9  | 19.3  | 5.4  | 1.3        | 7.2        | 1.5         | 11.1       |      | 20.1  | 19.1  | 1.6  |
| Delay (s)                     | 49.0  | 31.8 | 53.2  | 38.3 | 33.9       | 41.0       | 26.6        | 44.3       |      | 44.3  | 52.3  | 29.2 |
| Level of Service              | D     | С    | D     | D    | С          | D          | С           | D          |      | D     | D     | С    |
| Approach Delay (s)            |       | 48.0 |       |      | 38.5       |            |             | 42.2       |      |       | 47.5  |      |
| Approach LOS                  |       | D    |       |      | D          |            |             | D          |      |       | D     |      |
| Intersection Summary          |       | -    |       |      |            |            |             |            |      |       |       |      |
| HCM Average Control Dela      |       |      | 44.4  | H    | CM Level   | of Servic  | e           |            | D    |       |       |      |
| HCM Volume to Capacity ra     | atio  |      | 0.80  |      |            |            |             |            |      |       |       |      |
| Actuated Cycle Length (s)     |       |      | 88.1  |      | im of lost |            |             |            | 12.6 |       |       |      |
| Intersection Capacity Utiliza | ntion |      | 76.2% | IC   | U Level c  | of Service | • S.S. (199 |            | D    |       |       |      |
| Analysis Period (min)         |       |      | 15    |      |            |            |             |            |      |       |       |      |
| c Critical Lane Group         |       |      |       |      |            |            |             |            |      |       |       |      |

|                                | ٨                      |           | $\mathbf{k}$ | 1     |            | Ł          | ٩               | Î        | p    | 1    | Ť    | 4               |
|--------------------------------|------------------------|-----------|--------------|-------|------------|------------|-----------------|----------|------|------|------|-----------------|
| Movement                       | EBL                    | EBT       | EBR          | WBL   | WBT        | WBR        | NBL             | NBT      | NBR  | SBL  | SBT  | SBR             |
| Lane Configurations            | ሻ                      | ŕ         | آم           | ሻ     | ₿          |            | ኻ               | ₽        |      | ኻ    | ተ    | ۲               |
| Volume (vph)                   | 128                    | 183       | 334          | 197   | 312        | 5          | 374             | 897      | 89   | 4    | 504  | 167             |
| Ideal Flow (vphpl)             | 2000                   | 2000      | 2000         | 2000  | 2000       | 2000       | 2000            | 2000     | 2000 | 2000 | 2000 | 2000            |
| Total Lost time (s)            | 6.1                    | 6.1       | 5.9          | 6.1   | 6.1        |            | 5.9             | 5.9      |      | 5.9  | 5.9  | 5.9             |
| Lane Util. Factor              | 1.00                   | 1.00      | 1.00         | 1.00  | 1.00       |            | 1.00            | 1.00     |      | 1.00 | 1.00 | 1.00            |
| Frt                            | 1.00                   | 1.00      | 0.85         | 1.00  | 1.00       |            | 1.00            | 0.99     |      | 1.00 | 1.00 | 0.85            |
| Flt Protected                  | 0.95                   | 1.00      | 1.00         | 0.95  | 1.00       |            | 0.95            | 1.00     |      | 0.95 | 1.00 | 1.00            |
| Satd. Flow (prot)              | 1881                   | 2000      | 1619         | 1863  | 1938       |            | 1743            | 1922     |      | 1900 | 1980 | 1650            |
| Flt Permitted                  | 0.28                   | 1.00      | 1.00         | 0.35  | 1.00       |            | 0.13            | 1.00     |      | 0.17 | 1.00 | 1.00            |
| Satd. Flow (perm)              | 562                    | 2000      | 1619         | 690   | 1938       |            | 245             | 1922     |      | 332  | 1980 | 1650            |
| Peak-hour factor, PHF          | 0.83                   | 0.83      | 0.83         | 0.80  | 0.80       | 0.80       | 0.90            | 0.90     | 0.90 | 0.95 | 0.95 | 0.95            |
| Adj. Flow (vph)                | 154                    | 220       | 402          | 246   | 390        | 6          | 416             | 997      | 99   | 4    | 531  | 176             |
| RTOR Reduction (vph)           | 0                      | 0         | 71           | 0     | 1          | 0          | 0               | 4        | 0    | 0    | 0    | 93              |
| Lane Group Flow (vph)          | 154                    | 220       | 331          | 246   | 395        | 0          | 416             | 1092     | 0    | 4    | 531  | 83              |
| Heavy Vehicles (%)             | 1%                     | 0%        | 5%           | 2%    | 3%         | 0%         | 9%              | 2%       | 9%   | 0%   | 1%   | 3%              |
| Turn Type                      | pm+pt                  |           | pm+ov        | pm+pt |            |            | pm+pt           |          |      | Perm |      | Perm            |
| Protected Phases               | 7                      | 4         | 5            | 3     | 8          |            | 5               | 2        |      |      | 6    | 1004 (1977 ALC) |
| Permitted Phases               | 4                      | Antonio   | 4            | 8     |            |            | 2               |          |      | 6    |      | 6               |
| Actuated Green, G (s)          | 21.9                   | 14.1      | 31.2         | 27.7  | 17.0       |            | 47.1            | 47.1     |      | 24.1 | 24.1 | 24.1            |
| Effective Green, g (s)         | 21.9                   | 14.1      | 31.2         | 27.7  | 17.0       |            | 47.1            | 47.1     |      | 24.1 | 24.1 | 24.1            |
| Actuated g/C Ratio             | 0.24                   | 0.16      | 0.35         | 0.31  | 0.19       |            | 0.52            | 0.52     |      | 0.27 | 0.27 | 0.27            |
| Clearance Time (s)             | 6.1                    | 6.1       | 5.9          | 6.1   | 6.1        |            | 5.9             | 5.9      |      | 5.9  | 5.9  | 5.9             |
| Vehicle Extension (s)          | 3.0                    | 3.0       | 3.0          | 3.0   | 3.0        |            | 3.0             | 3.0      |      | 3.0  | 3.0  | 3.0             |
| Lane Grp Cap (vph)             | 251                    | 313       | 561          | 352   | 366        |            | 413             | 1006     |      | 89   | 530  | 442             |
| v/s Ratio Prot                 | 0.05                   | 0.11      | 0.11         | c0.08 | c0.20      |            | 0.19            | c0.57    |      |      | 0.27 |                 |
| v/s Ratio Perm                 | 0.00                   | 0,11      | 0.09         | 0.13  | 00.20      |            | 0.34            | 00.01    |      | 0.01 |      | 0.05            |
| v/c Ratio                      | 0.61                   | 0.70      | 0.59         | 0.70  | 1.08       |            | 1.01            | 1.09     |      | 0.04 | 1.00 | 0.19            |
| Uniform Delay, d1              | 28.7                   | 36.0      | 24.2         | 25.2  | 36.5       |            | 31.4            | 21.4     |      | 24.4 | 33.0 | 25.4            |
| Progression Factor             | 1.00                   | 1.00      | 1.00         | 1.00  | 1.00       |            | 1.00            | 1.00     |      | 0.92 | 0.95 | 0.89            |
| Incremental Delay, d2          | 4.4                    | 7.0       | 1.7          | 6.0   | 70.0       |            | 46.1            | 54.6     |      | 0.9  | 38.9 | 0.9             |
| Delay (s)                      | 33.1                   | 42.9      | 25.8         | 31.2  | 106.5      |            | 77.6            | 76.0     |      | 23.4 | 70.2 | 23.4            |
| Level of Service               | 00.1<br>C              | D         | 20.0<br>C    | C C   | 100.0      |            | E E             | <br>E    |      | 0.1  | E    | C               |
| Approach Delay (s)             | an Baar A <b>ye</b> ay | 32.1      | <b>-</b>     |       | 77.6       |            | Hall Bark Halls | 76.4     |      |      | 58.4 |                 |
| Approach LOS                   |                        | 02.1<br>C |              |       | E          |            |                 | ν.τ<br>Ε |      |      | E    |                 |
| Intersection Summary           |                        |           |              |       |            |            |                 |          |      |      |      |                 |
| HCM Average Control Delay      |                        |           | 63.7         | H     | CM Level   | of Servic  | ce              |          | E    |      |      |                 |
| HCM Volume to Capacity rat     | tio                    |           | 1.07         |       |            |            |                 |          |      |      |      |                 |
| Actuated Cycle Length (s)      |                        |           | 90.0         | S     | um of lost | time (s)   |                 |          | 18.1 |      |      |                 |
| Intersection Capacity Utilizat | tion                   |           | 100.9%       | IC    | CU Level c | of Service | •               |          | G    |      |      |                 |
| Analysis Period (min)          |                        |           | 15           |       |            |            |                 |          |      |      |      |                 |

|                                   | ٨    |            | $\mathbf{k}$ | <b>*</b> | <b>«</b> — | ۹.         | ٩     | Î     | p    | \$   | Ļ    | 1    |
|-----------------------------------|------|------------|--------------|----------|------------|------------|-------|-------|------|------|------|------|
| Movement                          | EBL  | EBT        | EBR          | WBL      | WBT        | WBR        | NBL   | NBT   | NBR  | SBL  | SBT  | SBR  |
| Lane Configurations               | ሻ    | <b>ሰ</b> ኑ |              | ኻ        | <b>ት</b> ጮ |            | ሻ     | Þ     |      | ኻ    | Þ    |      |
| Volume (vph)                      | 60   | 680        | 106          | 77       | 762        | 121        | 122   | 470   | 43   | 80   | 400  | 21   |
| ldeal Flow (vphpl)                | 2000 | 2000       | 2000         | 2000     | 2000       | 2000       | 2000  | 2000  | 2000 | 2000 | 2000 | 2000 |
| Total Lost time (s)               | 6.0  | 6.0        |              | 6.0      | 6.0        |            | 6.0   | 6.0   |      | 6.0  | 6.0  |      |
| Lane Util. Factor                 | 1.00 | 0.95       |              | 1.00     | 0.95       |            | 1.00  | 1.00  |      | 1.00 | 1.00 |      |
| Frt                               | 1.00 | 0.98       |              | 1.00     | 0.98       |            | 1.00  | 0.99  |      | 1.00 | 0.99 |      |
| Flt Protected                     | 0.95 | 1.00       |              | 0.95     | 1.00       |            | 0.95  | 1.00  |      | 0.95 | 1.00 |      |
| Satd. Flow (prot)                 | 1863 | 3650       |              | 1863     | 3649       |            | 1863  | 1936  |      | 1863 | 1946 |      |
| Fit Permitted                     | 0.95 | 1.00       |              | 0.95     | 1.00       |            | 0.95  | 1.00  |      | 0.95 | 1.00 |      |
| Satd. Flow (perm)                 | 1863 | 3650       |              | 1863     | 3649       |            | 1863  | 1936  |      | 1863 | 1946 |      |
| Peak-hour factor, PHF             | 0.90 | 0.90       | 0.90         | 0.92     | 0.92       | 0.92       | 0.89  | 0.89  | 0.89 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph)                   | 67   | 756        | 118          | 84       | 828        | 132        | 137   | 528   | 48   | 89   | 444  | 23   |
| RTOR Reduction (vph)              | 0    | 14         | 0            | 0        | 14         | 0          | 0     | 3     | 0    | 0    | 2    | 0    |
| Lane Group Flow (vph)             | 67   | 860        | 0            | 84       | 946        | 0          | 137   | 573   | 0    | 89   | 465  | 0    |
| Turn Type                         | Prot |            |              | Prot     |            |            | Prot  |       |      | Prot |      |      |
| Protected Phases                  | 5    | 2          |              | 1        | 6          |            | 3     | 8     |      | 7    | 4    |      |
| Permitted Phases                  |      |            |              |          |            |            |       |       |      |      |      |      |
| Actuated Green, G (s)             | 6.8  | 24.8       |              | 7.0      | 25.0       |            | 10.1  | 27.8  |      | 6.4  | 24.1 |      |
| Effective Green, g (s)            | 6.8  | 24.8       |              | 7.0      | 25.0       |            | 10.1  | 27.8  |      | 6.4  | 24.1 |      |
| Actuated g/C Ratio                | 0.08 | 0.28       |              | 0.08     | 0.28       |            | 0.11  | 0.31  |      | 0.07 | 0.27 |      |
| Clearance Time (s)                | 6.0  | 6.0        |              | 6.0      | 6.0        |            | 6.0   | 6.0   |      | 6.0  | 6.0  |      |
| Vehicle Extension (s)             | 3.0  | 3.0        |              | 3.0      | 3.0        |            | 3.0   | 3.0   |      | 3.0  | 3.0  |      |
| Lane Grp Cap (vph)                | 141  | 1006       |              | 145      | 1014       |            | 209   | 598   |      | 132  | 521  |      |
| v/s Ratio Prot                    | 0.04 | 0.24       |              | c0.05    | c0.26      |            | c0.07 | c0.30 |      | 0.05 | 0.24 |      |
| v/s Ratio Perm                    |      |            |              |          |            |            |       |       |      |      |      |      |
| v/c Ratio                         | 0.48 | 0.86       |              | 0.58     | 0.93       |            | 0.66  | 0.96  |      | 0.67 | 0.89 |      |
| Uniform Delay, d1                 | 39.9 | 30.9       |              | 40.1     | 31.7       |            | 38.3  | 30.5  |      | 40.8 | 31.7 |      |
| Progression Factor                | 1.00 | 1.00       |              | 1.10     | 1.23       |            | 1.36  | 0.66  |      | 1.00 | 1.00 |      |
| Incremental Delay, d2             | 2.5  | 9.2        |              | 4.4      | 13.6       |            | 6.6   | 24.9  |      | 12.8 | 17.3 |      |
| Delay (s)                         | 42.4 | 40.1       |              | 48.6     | 52.5       |            | 58.8  | 45.0  |      | 53.6 | 49.0 |      |
| Level of Service                  | D    | D          |              | D        | D          |            | Е     | D     |      | D    | D    |      |
| Approach Delay (s)                |      | 40.3       |              |          | 52.2       |            |       | 47.6  |      |      | 49.8 |      |
| Approach LOS                      |      | D          |              |          | D          |            |       | D     |      |      | D    |      |
| Intersection Summary              |      |            |              |          |            |            |       |       |      |      |      |      |
| HCM Average Control Delay         |      |            | 47.3         | Н        | CM Level   | of Service | Э     |       | D    |      |      |      |
| HCM Volume to Capacity ratio      |      |            | 0.84         |          |            |            |       |       |      |      |      |      |
| Actuated Cycle Length (s)         |      |            | 90.0         |          | im of lost |            |       |       | 18.0 |      |      |      |
| Intersection Capacity Utilization | 1    |            | 81.3%        | IC       | U Level o  | f Service  |       |       | D    |      |      |      |
| Analysis Period (min)             |      |            | 15           |          |            |            |       |       |      |      |      |      |
| c Critical Lane Group             |      |            |              |          |            |            |       |       |      |      |      |      |

|                                   | ٨    | <b>→</b>            | >     | *         | 4          | ×.         | ٩    | Å                                     | p     | 1       | Ļ    | 1    |
|-----------------------------------|------|---------------------|-------|-----------|------------|------------|------|---------------------------------------|-------|---------|------|------|
| Movement                          | EBL  | EBT                 | EBR   | WBL       | WBT        | WBR        | NBL  | NBT                                   | NBR   | SBL     | SBT  | SBR  |
| Lane Configurations               | ሻ    | 个序                  |       | ሻ         | 个际         |            | ሻ    | ŧ                                     | ሾ     | ሻ       | 个    | ሻ    |
| Volume (vph)                      | 18   | 982                 | 101   | 261       | 876        | 464        | 220  | 82                                    | 323   | 344     | 156  | 40   |
| Ideal Flow (vphpl)                | 2000 | 2000                | 2000  | 2000      | 2000       | 2000       | 2000 | 2000                                  | 2000  | 2000    | 2000 | 2000 |
| Lane Width                        | 12   | 12                  | 12    | 12        | 12         | 12         | 11   | 11                                    | 11    | 12      | 12   | 12   |
| Total Lost time (s)               | 6.1  | 6.1                 |       | 6.1       | 6.1        |            | 6.0  | 6.0                                   | 6.1   | 6.0     | 6.0  | 6.0  |
| Lane Util. Factor                 | 1.00 | 0.95                |       | 1.00      | 0.95       |            | 1.00 | 1.00                                  | 1.00  | 1.00    | 1.00 | 1.00 |
| Frt                               | 1.00 | 0.99                |       | 1.00      | 0.95       |            | 1.00 | 1.00                                  | 0.85  | 1.00    | 1.00 | 0.85 |
| Flt Protected                     | 0.95 | 1.00                |       | 0.95      | 1.00       |            | 0.95 | 1.00                                  | 1.00  | 0,95    | 1.00 | 1.00 |
| Satd. Flow (prot)                 | 1863 | 3673                |       | 1863      | 3532       |            | 1801 | 1895                                  | 1611  | 1863    | 1961 | 1667 |
| Flt Permitted                     | 0.13 | 1.00                |       | 0.11      | 1.00       |            | 0.65 | 1.00                                  | 1.00  | 0.54    | 1.00 | 1.00 |
| Satd. Flow (perm)                 | 262  | 3673                |       | 218       | 3532       |            | 1231 | 1895                                  | 1611  | 1057    | 1961 | 1667 |
| Peak-hour factor, PHF             | 0.88 | 0.88                | 0.88  | 0.92      | 0.92       | 0.92       | 0.94 | 0.94                                  | 0.94  | 0.92    | 0.92 | 0.92 |
| Adj. Flow (vph)                   | 20   | 1116                | 115   | 284       | 952        | 504        | 234  | 87                                    | 344   | 374     | 170  | 43   |
| RTOR Reduction (vph)              | 0    | 9                   | 0     | 0         | 74         | 0          | 0    | 0                                     | 0     | 0       | 0    | 28   |
| Lane Group Flow (vph)             | 20   | 1222                | 0     | 284       | 1382       | 0          | 234  | 87                                    | 344   | 374     | 170  | 15   |
| Parking (#/hr)                    |      |                     | 0     |           |            | Ō          |      |                                       |       |         |      |      |
| Turn Type                         | Perm | <u></u>             |       | pm+pt     |            |            | Perm | · · · · · · · · · · · · · · · · · · · | pm+ov | pm+pt   |      | Perm |
| Protected Phases                  |      | 2                   |       | <u> 1</u> | 5          |            |      | 8                                     | ંંાા  | · · · 7 | 4    |      |
| Permitted Phases                  | 2    | an data da da sa ta |       | 5         |            |            | 8    |                                       | 8     | 4       |      | 4    |
| Actuated Green, G (s)             | 29.9 | 29.9                |       | 46.9      | 46.9       |            | 20.0 | 20.0                                  | 30.9  | 31.0    | 31.0 | 31.0 |
| Effective Green, g (s)            | 29.9 | 29.9                |       | 46.9      | 46.9       |            | 20.0 | 20.0                                  | 30.9  | 31.0    | 31.0 | 31.0 |
| Actuated g/C Ratio                | 0.33 | 0.33                |       | 0.52      | 0.52       |            | 0.22 | 0.22                                  | 0.34  | 0.34    | 0.34 | 0.34 |
| Clearance Time (s)                | 6.1  | 6.1                 |       | 6.1       | 6.1        |            | 6.0  | 6.0                                   | 6.1   | 6.0     | 6.0  | 6.0  |
| Vehicle Extension (s)             | 3.0  | 3.0                 |       | 3.0       | 3.0        |            | 3.0  | 3.0                                   | 3.0   | 3.0     | 3.0  | 3.0  |
| Lane Grp Cap (vph)                | 87   | 1220                |       | 313       | 1841       |            | 274  | 421                                   | 553   | 409     | 675  | 574  |
| v/s Ratio Prot                    |      | c0.33               |       | 0.11      | c0.39      |            |      | 0.05                                  | 0.08  | c0.05   | 0.09 |      |
| v/s Ratio Perm                    | 0.08 |                     |       | 0.36      |            |            | 0.19 |                                       | 0.14  | c0.26   |      | 0.01 |
| v/c Ratio                         | 0.23 | 1.00                |       | 0.91      | 0.75       |            | 0.85 | 0.21                                  | 0.62  | 0.91    | 0.25 | 0.03 |
| Uniform Delay, d1                 | 21.7 | 30.1                |       | 23.6      | 17.0       |            | 33.6 | 28.5                                  | 24.7  | 29.1    | 21.2 | 19.5 |
| Progression Factor                | 0.67 | 0.65                |       | 1.00      | 1.00       |            | 1.00 | 1.00                                  | 1.00  | 1.00    | 1.00 | 1.00 |
| Incremental Delay, d2             | 5.6  | 25.2                |       | 28.2      | 1.8        |            | 21.9 | 0.2                                   | 2.2   | 24.6    | 0.2  | 0.0  |
| Delay (s)                         | 20.1 | 44.6                |       | 51.8      | 18.7       |            | 55.5 | 28.8                                  | 26.9  | 53.7    | 21.4 | 19.5 |
| Level of Service                  | С    | D                   |       | D         | В          |            | E    | С                                     | С     | D       | С    | В    |
| Approach Delay (s)                |      | 44.2                |       |           | 24.1       |            |      | 37.2                                  |       |         | 41.8 |      |
| Approach LOS                      |      | D                   |       |           | С          |            |      | D                                     |       |         | D    |      |
| Intersection Summary              |      |                     |       |           |            |            |      |                                       |       |         |      |      |
| HCM Average Control Delay         |      |                     | 34.5  | Н         | CM Leve    | of Servic  | e    |                                       | С     |         |      |      |
| HCM Volume to Capacity ratio      |      |                     | 0.94  |           |            |            |      |                                       |       |         |      |      |
| Actuated Cycle Length (s)         |      |                     | 90.0  | S         | um of los  | t time (s) |      |                                       | 18.2  |         |      |      |
| Intersection Capacity Utilization | 1    |                     | 92.1% | IC        | CU Level o | of Service |      |                                       | F     |         |      |      |
| Analysis Period (min)             |      |                     | 15    |           |            |            |      |                                       |       |         |      |      |
| c Critical Lane Group             |      |                     |       |           |            |            |      |                                       |       |         |      |      |

Appendix E

Roundabout Level of Service Capacity Analysis

|  |                                 |  |   | •                             |
|--|---------------------------------|--|---|-------------------------------|
| * * * * * * * * * * * * * * * * * * *                            | *****                           | *****                                  | * | * * * * * * * * * * * * * * * |
| * 10:4:08  |                                 | - • ·                                  | -96 WESTBOUND RAMP                      | 174 *                         |
|  |                                 |  |   |                               |
| * E (m) 8.50<br>* L' (m) 10.00                                   |                                 |  | * TIME PERIOD<br>* TIME SLICE           | min 90 *<br>min 15 *          |
| * V (m) 7.60   |                                 |  | * RESULTS PERIOD                        |                               |
| * RAD (m) 42.00  |                                 |  |   | \$/hr 15.00 *                 |
| * PHI (d) 20.00  |                                 |  | * FLOW PERIOD                           | min 15 75 *                   |
| * DIA (m) 65.00  |                                 |  | * FLOW TYPE pcu                         |                               |
| * GRAD SEP 0   |                                 |  | * FLOW PEAK am/op                       |                               |
| *  | 0 0                             | 0                                      | *                                       | 5, bii 111<br>*               |
| * * * * * * * * * * * * * * * * * * *                            | ****                            | * * * * * * * * * *                    | * | * * * * * * * * * * * * * *   |
| * LEG NAME *PCU *F<br>* * *                                      | LOWS (1st exit                  | 2nd etc.                               | U)*FLOF*CL* FLOW RATIO<br>* * *         | *FLOW TIME*<br>* *            |
| *D-19 SB *1.05*  | 136 923 425                     | 0                                      | *1.00*50*0.75 1.125 0.                  | .75*15 45 75 *                |
| *I-96 EB *1.05*  | 125 185 287                     | 0                                      | *1.00*50*0.75 1.125 0.                  | .75*15 45 75 *                |
| *D-19 NB *1.05*  | 341 467 122                     | 0                                      | *1.00*50*0.75 1.125 0.                  | .75*15 45 75 *                |
| *NATIONL WB*1.05*  | 99 51 182                       | 0                                      | *1.00*50*0.75 1.125 0.                  | .75*15 45 75 *                |
| *****  | * * * * * * * * * * * * * * * * | * * * * * * * * * *                    | * | *****                         |
| * FLOW veh   | 1484 597                        | 930                                    | 332 *                                   | *                             |
| * CAPACITY veh   | 2289 1984                       |  | 1866 * AVDE                             | ELs 5.1 *                     |
| * AVE DELAY mins   | 0.08 0.04                       |  | 0.04 * L C                              |                               |
| * MAX DELAY mins   | 0.11 0.06                       |  | 0.05 * VEH                              |                               |
| * AVE QUEUE veh  | 2 0                             | 2                                      | 0 * COSI                                | r\$ 71.0 *                    |
| * MAX QUEUE veh  | 3 1                             | ++++++++++++++++++++++++++++++++++++++ | · · · · · · · · · · · · · · · · · · ·   | *****                         |
| * * * * * * * * * * * * * * * * * * *                            | * * * * * * * * * * * * * * * * | * * * * * * * * * * *                  | * | *****                         |
| * * * * * * * * * * * * * * * * * * *                            | ****                            | *******                                | ****                                    | ****                          |
| * 10:4:08  |                                 |  | -96 WESTBOUND RAMP                      | 175 *                         |
|  |                                 | •                                      | ****                                    |                               |
| *E (m) 8.50  | 12.80 8.50                      | 8.50                                   | * TIME PERIOD                           | min 90 *                      |
| * L' (m) 10.00   | 53.00 10.00                     | 150.0                                  | * TIME SLICE                            | min 15 *                      |
| *∨ (m) 7.60  | 5.50 4.50                       | 4.00                                   | * RESULTS PERIOD                        | min 15 75 *                   |
| * RAD (m) 42.00  | 56.00 65.50                     | 36.50                                  | * TIME COST \$                          | 5/hr 15.00 *                  |
| * PHI (d) 20.00  | 20.00 20.00                     | 20.00                                  | * FLOW PERIOD                           | min 15 75 *                   |
| * DIA (m) 65.00  | 65.00 65.00                     | 65.00                                  | * FLOW TYPE pcu/                        | 'veh VEH *                    |
| * GRAD SEP 0   | 0 0                             | 0                                      | * FLOW PEAK am/op                       | /pm PM *                      |
| * * * * * * * * * * * * * * * * * * *                            |                                 |  |   | *****                         |
| * LEG NAME *PCU *F:<br>* * * *                                   | ·                               | 2nd etc                                | * * *                                   | *FLOW TIME*<br>*              |
| *D-19 SB *1.05*  | 165 750 188                     | 0                                      | *1.00*50*0.75 1.125 0.                  |                               |
| *I-96 EB *1.05*  | 411 175 721                     | 0                                      | *1.00*50*0.75 1.125 0.                  |                               |
| *D-19 NB *1.05*  | 163 469 87                      | 0                                      | *1.00*50*0.75 1.125 0.                  |                               |
| *NATIONL WB*1.05*  | 341 170 554                     |  | *1.00*50*0.75 1.125 0.                  |                               |
| *  |                                 | ~ ^ ^ ^ ^ ^ ^ ^ ^ ^ ^ ^ ^              | *                                       |                               |
|  | 1103 1307                       | 719                                    | 1065 *                                  | *                             |
| * FLOW veh<br>* CAPACITY veh                                     | 1968 2015                       |  | 1589 * AVDE                             |                               |
| * AVE DELAY mins   | 0.07 0.10                       |  | 0.13 * L C                              |                               |
| * MAX DELAY mins   | 0.10 0.16                       |  | 0.22 * VEH                              |                               |
| * AVE QUEUE veh  | 1 2                             | 1                                      | 2 * COST                                | -                             |
| * MAX QUEUE veh  | 2 3                             | 2                                      | 3 *                                     | * ±00.0                       |
| *  |                                 |  | *                                       | *                             |
| A state to the data to de she to the data to the data based at a | * * * * * * * * * * * * * * * * | ******                                 | *****                                   | ****                          |

50% CL, 15-minute time slice RODEL Analysis (Default)

85% CL, 15-minute time slice RODEL Analysis (Default)

| ****   | * * * * * * * * * * * *   | *****   | *****  | ****  |   |
|--|---|---|--|---|---|
| * 10:4:08  |   |   | 9/I-96 WESTBOU   |   | 176 *   |
|  |   |   | •  | ****  |   |
| *E (m) 8.50  | ) 12.80 8   | .50 8.50  | ) *  | TIME PERIOD min   | 90 *  |
| * L' (m) 10.00   | 53.00 10  | .00 150.0   | ) *  | TIME SLICE min  | 15 *  |
| *V (m) 7.60  |   | .50 4.00  | ) *  | RESULTS PERIOD min 1  | .5 75 *   |
| * RAD (m) 42.00  | ) 56.00 65  | .50 36.50   | ) *  | TIME COST \$/hr 1   | .5.00 *   |
| * PHI (d) 20.00  | 20.00 20  | .00 20.00   | ) *  | FLOW PERIOD min 1   | .5 75 *   |
| * DIA (m) 65.00  | ) 65.00 65  | .00 65.00   | ) *  | FLOW TYPE pcu/veh   | VEH *   |
| * GRAD SEP (   | 0 (   | 0 (   | ) *  | FLOW PEAK am/op/pm  | AM *  |
| * * * * * * * * * * * * * * * * * * *  |   |   |  | *   | ******  |
| * LEG NAME *PCU *H<br>* * *  | FLOWS (1st e  | xit 2nd et  | cU) *FLOF*C<br>* *   | L* FLOW RATIO *FLC<br>* *   | W TIME*<br>*  |
| *D-19 SB *1.05*  | 136 923   | 425 0   | *1.00*8  | 5*0.75 1.125 0.75*15  | 45 75 *   |
| *I-96 EB *1.05*  | 125 185   | 287 0   | *1.00*8  | 5*0.75 1.125 0.75*15  | 45 75 *   |
| *D-19 NB *1.05*  | 341 467   | 122 0   | *1.00*8  | 5*0.75 1.125 0.75*15  | 45 75 *   |
| *NATIONL WB*1.05*  |   | 182 0   |  | 5*0.75 1.125 0.75*15  |   |
|  |   |   |  | *   | * * * * * * *   |
| * FLOW veh   |   | 597 930   |  | *   | *   |
| * CAPACITY veh   |   | 787 1193  |  | * AVDEL s   | 8.5 *   |
| * AVE DELAY mins   |   | .05 0.29  |  | * L O S   | A *   |
| * MAX DELAY mins   |   | .07 0.54  |  | * VEH HRS   | 7.9 *   |
| * AVE QUEUE veh  | 3   | 1 5   |  | * COST \$   | 118.6 *   |
| * MAX QUEUE veh  | 4   | 1 8   | -  | *<br>* * * * * * * * * * * * * * * * * * *  | *   |
|  |   |   |  | ~   | ~ ~ ~ ~ ~ ~ ~ ~   |
|  |   |   |  |   |   |
| * * * * * * * * * * * * * * * * * * *  | ****  | * * * * * * * * * *   | ****   | *   | *****   |
|  |   |   |  | **************************************  |   |
| * 10:4:08  | CITY OF H   | OWELL D-19  | /I-96 WESTBOU  |   | 177 *   |
| * 10:4:08  | CITY OF H   | OWELL D-19  | /I-96 WESTBOU  | ND RAMP<br>*********  | 177 *<br>*****  |
| * 10:4:08<br>****  | CITY OF H<br>************************************   | OWELL D-19  | /I-96 WESTBOUN   | ND RAMP<br>************************************   | 177 *<br>******<br>90 *   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>************************************   | OWELL D-19<br>*********<br>.50 8.50   | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>**************************<br>TIME PERIOD min<br>TIME SLICE min  | 177 *<br>******<br>90 *   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>************************************   | OWELL D-19<br>**********<br>.50 8.50<br>.00 150.0   | /I-96 WESTBOUN<br>*****************<br>* ;<br>* ;              | ND RAMP<br>******************************<br>TIME PERIOD min<br>TIME SLICE min<br>RESULTS PERIOD min 1  | 177 *<br>*******<br>90 *<br>15 *  |
| * 10:4:08<br>***********************<br>* E (m) 8.50<br>* L' (m) 10.00<br>* V (m) 7.60 | CITY OF H<br>************************************   | OWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00   | /I-96 WESTBOUN<br>***************<br>* ;<br>* ;<br>* ;         | ND RAMP<br>****************************<br>TIME PERIOD min<br>TIME SLICE min<br>RESULTS PERIOD min 1<br>TIME COST \$/hr 1                         | 177 *<br>******<br>90 *<br>15 *<br>5 75 *   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>***********<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20   | OWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00<br>.50 36.50  | /I-96 WESTBOUN<br>****************<br>* 1<br>* 1<br>* 1<br>* 1 | ND RAMP<br>****************************<br>TIME PERIOD min<br>TIME SLICE min<br>RESULTS PERIOD min 1<br>FIME COST \$/hr 1                         | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>***********<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65                             | OWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00<br>.50 36.50<br>.00 20.00   | /I-96 WESTBOU<br>************************************          | ND RAMP<br>*******************************<br>TIME PERIOD min<br>TIME SLICE min<br>RESULTS PERIOD min 1<br>TIME COST \$/hr 1<br>FLOW PERIOD min 1 | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>************************************   | OWELL D-19         .50       8.50         .00       150.0         .50       4.00         .50       36.50         .00       20.00         .00       65.00         0       0         .50       4.00 | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *  |
| * 10:4:08<br>************************************                                      | CITY OF H<br>************************************   | OWELL D-19         .50       8.50         .00       150.0         .50       4.00         .50       36.50         .00       20.00         .00       65.00         0       0         .50       4.00 | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *  |
| * 10:4:08<br>************************************                                      | CITY OF H<br>**********<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>***********          | OWELL D-19         .50       8.50         .00       150.0         .50       4.00         .50       36.50         .00       20.00         .00       65.00         0       0         .50       4.00 | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>*   |
| * 10:4:08<br>************************************                                      | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | OWELL D-19         .50       8.50         .00       150.0         .50       4.00         .50       36.50         .00       20.00         .00       65.00         0       0         .50       4.00 | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>*   |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00<br>.50 36.50<br>.00 20.00<br>.00 65.00<br>0 0<br>**********<br><it 2nd="" et<br="">188 0<br/>721 0</it>                             | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5.75 *<br>5.00 *<br>5.75 *<br>VEH *<br>PM *<br>******<br>W TIME*<br>*<br>45 75 *<br>45 75 *  |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00<br>.50 36.50<br>.00 20.00<br>.00 65.00<br>0 0<br>**********<br>xit 2nd et<br>188 0<br>721 0<br>37 0                                 | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>*******<br>90 *<br>15 *<br>5.00 *<br>5.00 *<br>5.75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *   |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>**********<br>.50 8.50<br>.00 150.0<br>.50 4.00<br>.50 36.50<br>.00 20.00<br>.00 65.00<br>0 0<br>**********<br>xit 2nd et<br>188 0<br>721 0<br>37 0<br>554 0                        | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *  |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>*******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *   |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *  |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *  |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOUN<br>************************************         | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>10.0 *<br>B *  |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>*******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>10.0 *<br>B *                                |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>10.0 *<br>B *<br>11.7 *<br>175.2 *            |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>*******<br>90 *<br>15 *<br>5 75 *<br>5.00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>10.0 *<br>B *                                |
| <pre>* 10:4:08 ************************************</pre>                              | CITY OF H<br>12.80 8<br>53.00 10<br>5.50 4<br>56.00 65<br>20.00 20<br>65.00 65<br>0<br>********************************** | DWELL D-19<br>************************************  | /I-96 WESTBOU<br>************************************          | ND RAMP<br>************************************   | 177 *<br>******<br>90 *<br>15 *<br>5 75 *<br>5 00 *<br>5 75 *<br>VEH *<br>PM *<br>*******<br>W TIME*<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>45 75 *<br>10.0 *<br>B *<br>11.7 *<br>175.2 * |

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| * 10:4:08 CITY OF HOWELL D-19/   |  |
|  |  |
|  |  |
|  |  |
| (11) , 100 3.30 1.30 1.00  | * RESULTS PERIOD min 15 75 *   |
| * RAD (m) 42.00 56.00 65.50 36.50<br>* PHT (d) 20.00 20.00 20.00 20.00             | * TIME COST \$/hr 15.00 *  |
| 1111 (d) 20.00 20.00 20.00 20.00   | * FLOW PERIOD min 15 75 *  |
| * DIA (m) 65.00 65.00 65.00  | * FLOW TYPE pcu/veh VEH *  |
| * GRAD SEP 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0                                   | * FLOW PEAK am/op/pm AM *  |
|  |  |
| * LEG NAME *PCU *FLOWS (1st exit 2nd etc<br>* * *                                  | U)*FLOF*CL* FLOW RATIO *FLOW TIME*<br>* * * *  |
| *D-19 SB *1.05* 136 923 425 0  | *1.00*50*0.75 1.125 0.75*15 45 75 *  |
| *I-96 EB *1.05* 125 185 287 0  | *1.00*50*0.75 1.125 0.75*15 45 75 *  |
| *D-19 NB *1.05* 341 467 122 0  | *1.00*50*0.75 1.125 0.75*15 45 75 *  |
| *NATIONL WB*1.05* 99 51 182 0  | *1.00*50*0.75 1.125 0.75*15 45 75 *  |
| ****   |  |
| * FLOW veh 1484 597 930  | 332 * *  |
| * CAPACITY veh 2289 1983 1390  | 1866 * AVDEL s 5.3 *   |
| * AVE DELAY mins 0.08 0.04 0.15  | 0.04 * L O S A *   |
| * MAX DELAY mins 0.10 0.05 0.21  | 0.04 * VEH HRS 5.0 *   |
| * AVE QUEUE veh 2 0 2  | 0 * COST \$ 74.3 *   |
| * MAX QUEUE veh 3 1 4  | 0 * *  |
| ****   | ****************   |
|  |  |
|  |  |
| ************   | *  |
| **************************************   |  |
|  | I-96 WESTBOUND RAMP 181 *  |
| * 10:4:08 CITY OF HOWELL D-19/   | I-96 WESTBOUND RAMP 181 *  |
| * 10:4:08 CITY OF HOWELL D-19/   | I-96 WESTBOUND RAMP 181 *  |
| * 10:4:08 CITY OF HOWELL D-19/2<br>************************************            | I-96 WESTBOUND RAMP 181 * *********************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | I-96 WESTBOUND RAMP 181 * *********************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP 181 * *********************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | I-96 WESTBOUND RAMP 181 * *********************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP 181 * *********************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/3 ************************************</pre>    | <pre>I-96 WESTBOUND RAMP 181 * *********************************</pre>   |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | <pre>I-96 WESTBOUND RAMP 181 * *********************************</pre>   |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | <pre>I-96 WESTBOUND RAMP 181 * *********************************</pre>   |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | I-96 WESTBOUND RAMP<br>************************************  |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | <pre>I-96 WESTBOUND RAMP 181 * *********************************</pre>   |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP       181 *         *       *         *       TIME PERIOD min       90 *         *       TIME SLICE min       1         *       RESULTS PERIOD min       15 75 *         *       TIME COST       \$/hr         *       FLOW PERIOD min       15 75 *         *       FLOW PEAK am/op/pm       PM *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       * |
| <pre>* 10:4:08 CITY OF HOWELL D-19/<br/>************************************</pre> | <pre>I-96 WESTBOUND RAMP 181 * *********************************</pre>   |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP       181 *         *       *         *       TIME PERIOD min 90         *       TIME SLICE min 1         *       RESULTS PERIOD min 15 75         *       TIME COST \$/hr 15.00         *       FLOW PERIOD min 15 75         *       TIME COST \$/hr 15.00         *       FLOW PERIOD min 15 75         *       FLOW TYPE pcu/veh VEH *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *         *       *                               |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP       181 *         *       *         *       TIME PERIOD min       90 *         *       TIME SLICE min       1         *       RESULTS PERIOD min       15 75 *         *       TIME COST       \$/hr         *       TIME COST       \$/hr         *       FLOW PERIOD min       15 75 *         *       FLOW PERIOD min       15 75 *         *       FLOW PERIOD min       15 75 *         *       FLOW PEAK am/op/pm       PM *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *         *       *       *       *             |
| <pre>* 10:4:08 CITY OF HOWELL D-19/? ************************************</pre>    | I-96 WESTBOUND RAMP       181 *         *       *         *       TIME PERIOD min 90         *       TIME SLICE min 1         *       RESULTS PERIOD min 15 75         *       TIME COST \$/hr 15.00         *       FLOW PERIOD min 15 75         *       TIME COST \$/hr 15.00         *       FLOW PERIOD min 15 75         *       FLOW TYPE pcu/veh VEH *         *       *     <   |

50% CL, 1-minute time slice RODEL Analysis

85% CL, 1-minute time slice RODEL Analysis

| * 10:4:08   |  | CITY O   | F HOWEI  | LL D-19/   | I-96 WEST   | BOUND R  | АМР   | * * * * * * * *   | 182  |
|---|--|--|--|--|---|--|---|---|--|
| *******   |  |  |  |  |   |  |   | ******  |  |
| * E (m)   | 8.50   | 12.80  | 8.50   | 8.50   |   | * TIME   | PERIOD  | min   | 90   |
| * L' (m)  | 10.00  |  | 10.00  | 150.0  |   | * TIME   |   | min   | 1  |
| * V (m)   | 7.60   |  | 4.50   | 4.00   |   |  | LTS PERI  |   | 15 75  |
| * RAD (m)   | 42.00  |  | 65.50  | 36.50  |   | * TIME   |   | \$/hr   |  |
| * PHI (d)   | 20.00  |  | 20.00  | 20.00  |   |  | PERIOD  | min   | 15.00  |
| * DIA (m)   | 65.00  |  | 65.00  | 65.00  |   | * FLOW   |   | bcu/veh   | VEH  |
| * GRAD SEP  | 00.00  | 00.00  | 00.00  | 00.00  |   |  | PEAK an   |   | AM   |
| ****  |  |  |  |  | *****   | ******   |   | *********   | MM<br>*******  |
|   |  |  |  |  | U) *FLOI  |  |   |   | FLOW TIM   |
| r   | * *  | 1000 (10   | e ente   | Ziid CCC   | *   | * *  |   | *   |  |
| ′D-19 SB  | *1.05*   | 136 92   | 3 425  | 0  | *1.00   | )*85*0.  | 75 1.125  | 5 0.75*1  | L5 45 75   |
| 1-96 EB   | *1.05*   | 125 18   | 5 287  | 0  |   |  | 75 1.125  |   |  |
| D-19 NB   | *1.05*   | 341 46   |  | 0  |   |  | 75 1.125  |   |  |
| NATIONL W   |  | 99 51  |  | 0<br>0   |   |  | 75 1.125  |   |  |
| *****   |  |  |  |  |   |  |   |   |  |
| FLOW  | veh  | 1484   | 597  | 930  | 332   |  | *   |   |  |
| CAPACITY  | veh  | 2092   | 1786   | 1193   | 1669  |  | * д   | VDEL s  | 9.0  |
| AVE DELA  |  | 0.11   | 0.05   | 0.31   | 0.05  |  | * I   |   | A  |
| MAX DELAY   |  | 0.15   | 0.06   | 0.56   | 0.05  |  |   | EH HRS  | 8.3  |
| AVE QUEU  |  | 3  | 1  | 5  | 0   |  |   | COST \$   | 124.8  |
| MAX OUEU  |  | 4  | 1  | 10   | 0   |  | *   | ,001 ý  | 124.0  |
|   |  |  |  |  | *******   |  |   |   |  |
| * * * * * * * * * *   |  | * * * * * * * * *  | * * * * * *  | *****  | * * * * * * * * * *   | ******   | * * * * * * * *   |   | * * * * * * *  |
| 10:4:08   | * * * * * * * * *                              | *******<br>CITY 03   | ******<br>F HOWEI  | L D-19/1   | *********<br>1-96 WESTE   | ******<br>30UND R4   | *******<br>\MP  | *****   | *******  |
| *********<br>10:4:08<br>*******   | ******   | *******<br>CITY O:<br>*******  | ******<br>F HOWEL<br>******  | L D-19/1   | *********<br>1-96 WESTE   | *******<br>30UND RA  | *******<br>\MP<br>******  | *****   | *******<br>183<br>******   |
| *********<br>10:4:08<br>*********<br>E (m)  | *********<br>*********<br>8.50                 | ********<br>CITY O<br>********<br>12.80  | ******<br>F HOWEI<br>******<br>8.50  | L D-19/2<br>*********<br>8.50  | *********<br>1-96 WESTE   | *******<br>30UND RA<br>*******<br>* TIME   | *******<br>AMP<br>********<br>PERIOD  | ******<br>******<br>min   | *******<br>183<br>*******<br>90  |
| **********<br>10:4:08<br>**********<br>E (m)<br>L' (m)  | *********<br>*********<br>8.50<br>10.00        | ********<br>CITY 03<br>********<br>12.80<br>53.00  | ******<br>F HOWEL<br>******<br>8.50<br>10.00   | L D-19/2<br>L D-19/2<br>********<br>8.50<br>150.0  | *********<br>I-96 WESTE<br>********   | *******<br>30UND RA<br>*******<br>* TIME<br>* TIME   | ********<br>AMP<br>********<br>PERIOD<br>SLICE  | *******<br>*******<br>min<br>min  | *******<br>183<br>*******<br>90<br>1   |
| **********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)  | *********<br>********<br>8.50<br>10.00<br>7.60 | ********<br>CITY O:<br>********<br>12.80<br>53.00<br>5.50  | ******<br>F HOWEL<br>******<br>8.50<br>10.00<br>4.50   | L D-19/2<br>*******<br>8.50<br>150.0<br>4.00   | *********<br>I-96 WESTE<br>********   | 30UND RA<br>*******<br>* TIME<br>* TIME<br>* RESUI   | ********<br>AMP<br>********<br>PERIOD<br>SLICE<br>LTS PERI  | *******<br>*******<br>min<br>Min<br>OD min  | 183<br>*******<br>90<br>1<br>15 75   |
| **************************************  | **************************************         | CITY O:<br>********<br>12.80<br>53.00<br>5.50<br>56.00   | *******<br>F HOWEI<br>*******<br>8.50<br>10.00<br>4.50<br>65.50  | L D-19/2<br>********<br>8.50<br>150.0<br>4.00<br>36.50   | *********<br>I-96 WESTE<br>********   | 30UND RA<br>*******<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* TIME   | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST   | *******<br>*******<br>min<br>OD min<br>\$/hr  | 183<br>183<br>1*******<br>90<br>1<br>15 75<br>15.00  |
| ***********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)   | **************************************         | ********<br>CITY O:<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00  | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00   | L D-19/2<br>********<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00  | *********<br>I-96 WESTE<br>*********  | 30UND RA<br>********<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* TIME<br>* FLOW  | ********<br>AMP<br>PERIOD<br>SLICE<br>CTS PERI<br>COST<br>PERIOD  | *******<br>min<br>min<br>OD min<br>\$/hr<br>min   | 183<br>183<br>183<br>10<br>15<br>15<br>15.00<br>15<br>75   |
| **************************************  | **************************************         | ********<br>CITY 03<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00   | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00  | L D-19/2<br>********<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00<br>65.00   | *********<br>I-96 WESTE<br>*********  | 30UND RA<br>********<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW  | AMP<br>PERIOD<br>SLICE<br>SLICE<br>COST<br>PERIOD<br>TYPE P   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh   | 183<br>*******<br>90<br>1575<br>15.00<br>1575<br>VEH   |
| ***********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP  | **************************************         | ********<br>CITY O:<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0  | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0   | L D-19/2<br>********<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00<br>65.00<br>0  | ********<br>I-96 WESTE<br>********  | 30UND RA<br>*******<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW   | AMP<br>PERIOD<br>SLICE<br>COST<br>PERIOD<br>TYPE P<br>PEAK am   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm   | 183<br>183<br>183<br>1<br>15<br>15<br>15.00<br>15<br>75<br>VEH<br>PM   |
| **********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP<br>*********  | **************************************         | *********<br>CITY O:<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0   | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******  | L D-19/2<br>*********<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00<br>65.00<br>0<br>********   | **********<br>I-96 WESTE<br>*********   | 30UND RA<br>********<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW  | AMP<br>PERIOD<br>SLICE<br>COST<br>PERIOD<br>TYPE P<br>PEAK am   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******  | 183<br>183<br>183<br>1<br>15<br>15<br>15.00<br>15<br>75<br>VEH<br>PM   |
| **********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP<br>**********<br>LEG NAME   | **************************************         | CITY O:<br>CITY O:<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0<br>constants<br>LOWS (1st   | *******<br>F HOWEI<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******  | L D-19/2<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00<br>65.00<br>0<br>*******<br>2nd etc.   | **********<br>I-96 WESTE<br>***********<br>************<br>**********   | 30UND RA<br>*******<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* CL* E                                  | AMP<br>PERIOD<br>SLICE<br>SLICE<br>COST<br>PERIOD<br>TYPE P<br>PEAK am<br>COST<br>PERIOD  | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>*  | ********<br>183<br>*******<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM  |
| **************************************  | **************************************         | *********<br>CITY 03<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0<br>********<br>LOWS (1st  | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit  | L D-19/1<br>***********************************  | **********<br>I-96 WESTE<br>**********<br>***********<br>************   | 30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* *****<br>* CL* F<br>* *                 | AMP<br>PERIOD<br>SLICE<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COST<br>TYPE p<br>PEAK am   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>*<br>0.75*1  | 183<br>********<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75  |
| **************************************  | **************************************         | CITY O:<br>CITY O:<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0<br>constants<br>LOWS (1st   | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit  | L D-19/1<br>***********************************  | **********<br>I-96 WESTE<br>**********<br>***********<br>************   | 30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* *****<br>* CL* F<br>* *                 | AMP<br>PERIOD<br>SLICE<br>SLICE<br>COST<br>PERIOD<br>TYPE P<br>PEAK am<br>COST<br>PERIOD  | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>*<br>0.75*1  | 183<br>********<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75  |
| **************************************  | **************************************         | <pre>************************************</pre>  | <pre>******* F HOWEL ****** 8.50 10.00 4.50 65.50 20.00 65.00 0 ******* c exit 0 188 5 721 87</pre>  | L D-19/1<br>***********************************  | **********<br>I-96 WESTE<br>**********<br>***********<br>************   | 30UND RA<br>*******<br>* TIME<br>* TIME<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>*******<br>**85*0.7<br>*85*0.7                                | ********<br>PERIOD<br>SLICE<br>SLICE<br>SLICE<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>*******<br>FLOW RAT<br>75 1.125<br>75 1.125<br>75 1.125   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1   | ********<br>183<br>*******<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>5 45 75   |
| **********<br>10:4:08<br>*********<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP<br>**********<br>LEG NAME<br>D-19 SB<br>I-96 EB<br>D-19 NB<br>NATIONL WE  | **************************************         | ********<br>CITY 02<br>********<br>12.80<br>53.00<br>5.50<br>56.00<br>20.00<br>65.00<br>0<br>********<br>LOWS (1st<br>165 750<br>411 175<br>163 469<br>341 170 | *******<br>F HOWEL<br>*******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit<br>0 188<br>5 721<br>9 87<br>0 554   | L D-19/1<br>***********************************  | **********<br>I-96 WESTE<br>**********<br>U) *FLOF<br>*<br>*1.00<br>*1.00<br>*1.00  | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | ********<br>PERIOD<br>SLICE<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>********<br>COW RAT<br>25 1.125<br>25 1.125<br>25 1.125<br>25 1.125   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1                                       | ********<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>5 45 75   |
| **************************************  | **************************************         | <pre>************************************</pre>  | <pre>******* F HOWEI ****** 8.50 10.00 4.50 65.50 20.00 65.00 0 ******* c exit 188 5 721 9 87 0 554 *******</pre>  | L D-19/2<br>************************************   | **********<br>I-96 WESTE<br>***********<br>************<br>U) *FLOF<br>*<br>1.00<br>*1.00<br>*1.00<br>*1.00   | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | ********<br>PERIOD<br>SLICE<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>********<br>COW RAT<br>25 1.125<br>25 1.125<br>25 1.125<br>25 1.125   | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1                                       | ********<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>5 45 75   |
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| 10:4:08<br>10:4:08<br>(m)<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP<br>************************************  | **************************************         | <pre>************************************</pre>  | ******<br>F HOWEI<br>******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit<br>0 188<br>5 721<br>9 87<br>0 554<br>******<br>1307<br>1817                                     | L D-19/2<br>************************************   | **********<br>I-96 WESTE<br>**********<br>***********<br>U) *FLOF<br>*<br>1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00 | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COW RAT<br>COW RAT<br>COM RAT<br>COM RAT<br>COM RAT<br>COW RAT<br>COM RAT<br>CO | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1<br>*******                            | ********<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>5 45 75   |
| 10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10:4:08<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10)<br>(10) | **************************************         | <pre>************************************</pre>  | ******<br>F HOWEI<br>******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit<br>188<br>5721<br>87<br>554<br>******<br>1307<br>1817<br>0.16                                    | L D-19/2<br>************************************   | **********<br>I-96 WESTE<br>***********<br>***********<br>***********   | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COW RAT<br>COW RAT<br>COM RAT<br>COW RAT<br>COW RAT<br>COW RAT<br>COM RAT<br>COM RAT<br>COW RAT<br>COM RAT<br>CO | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1<br>*******<br>VDEL s<br>O S           | ********<br>183<br>*******<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8   |
| 10:4:08<br>10:4:08<br>(m)<br>E (m)<br>L' (m)<br>V (m)<br>RAD (m)<br>PHI (d)<br>DIA (m)<br>GRAD SEP<br>************************************  | **************************************         | <pre>************************************</pre>  | ******<br>F HOWEI<br>******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit<br>0 188<br>5 721<br>9 87<br>0 554<br>******<br>1307<br>1817                                     | L D-19/2<br>************************************   | **********<br>I-96 WESTE<br>**********<br>***********<br>U) *FLOF<br>*<br>1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00<br>*1.00 | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COW RAT<br>COW RAT<br>CO | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1<br>*******<br>VDEL s<br>O S<br>EH HRS | *******<br>183<br>*******<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>1000 75<br>10000 75<br>1000 75<br>1000 75<br>1000 75<br>10000 |
| <pre>     10:4:08     10:4:08     (m)     E (m)     L' (m)     V (m)     RAD (m)     PHI (d)     DIA (m)     GRAD SEP     *********************************</pre>   | **************************************         | <pre>************************************</pre>  | ******<br>F HOWEL<br>******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>*******<br>c exit<br>188<br>5721<br>87<br>188<br>5721<br>87<br>554<br>*******<br>1307<br>1817<br>0.16<br>0.28<br>4 | L D-19/2<br>************************************   | **********<br>I-96 WESTE<br>***********<br>***********<br>***********   | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COW RAT<br>COW RAT<br>CO | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1<br>*******<br>VDEL s<br>O S           | ********<br>183<br>*******<br>90<br>1<br>15 75<br>15.00<br>15 75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5 45 75<br>5 45 75<br>8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8   |
| 10:4:08       ************************************  | **************************************         | <pre>************************************</pre>  | ******<br>F HOWEL<br>******<br>8.50<br>10.00<br>4.50<br>65.50<br>20.00<br>65.00<br>0<br>******<br>c exit<br>188<br>5721<br>87<br>188<br>5721<br>87<br>554<br>*******<br>1307<br>1817<br>0.16<br>0.28       | L D-19/2<br>8.50<br>150.0<br>4.00<br>36.50<br>20.00<br>65.00<br>0<br>*********<br>2nd etc.<br>0<br>0<br>0<br>0<br>*********<br>2nd etc.<br>0<br>0<br>0<br>0<br>********* | **********<br>I-96 WESTE<br>***********<br>***********<br>***********   | *******<br>30UND RA<br>* TIME<br>* TIME<br>* TIME<br>* RESUI<br>* TIME<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* FLOW<br>* S5*0.7<br>*85*0.7<br>*85*0.7 | AMP<br>PERIOD<br>SLICE<br>TS PERI<br>COST<br>PERIOD<br>TYPE p<br>PEAK am<br>COW RAT<br>COW RAT<br>CO | *******<br>min<br>min<br>OD min<br>\$/hr<br>min<br>cu/veh<br>/op/pm<br>*******<br>IO *F<br>0.75*1<br>0.75*1<br>0.75*1<br>0.75*1<br>*******<br>VDEL s<br>O S<br>EH HRS | 183<br>183<br>115<br>15<br>15<br>15<br>15<br>00<br>15<br>75<br>VEH<br>PM<br>*******<br>LOW TIM<br>5<br>45<br>75<br>5<br>45<br>75<br>5<br>45<br>75<br>5<br>45<br>75<br>5<br>45<br>75<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  |

Appendix F

SEMCOG Letter

## SEVCOG ... Local Governments Advancing Southeast Michigan

Southeast Michigan Council of Governments • 535 Griswold Street, Suite 300 • Detroit, Michigan 48226-3602 • 313-961-4266 • Fax 313-961-486: www.semcog.org

February 18, 2005

Richard F. Beaubien Hubbell, Roth & Clark, Inc. 555 Hulet Bloomfield Hills, MI 48302

Dear Mr. Beaubien:

Per your request, enclosed is a summary of the projected SEMCOG travel demand forecast model results. Specifically, the growth rate is an increase of around 21 percent, between year 2005 base and 2005 alternative with Howell Loop Rd.

The project limits used are:

Howell Loop Rd. connecting I-96 to WB off ramps at Pinckney to Grand River at National.

The projections use SEMCOG 2030 Regional Transportation Plan land use data sets. The input data for the travel model are based on the forecasted socio-economic data adopted for SEMCOG 2030 RTP process. Please note that the model is designed to analyze traffic patterns and congestion on a regional level. When looking at the community level, the data may be skewed due to the relatively large size of our regional activity zones, the detail level of roadway network (i.e., only major roadways are included in our regional model), and the location of centroid connectors.

Please be advised that the SEMCOG network is not dense enough in the study area to provide adequate representation of traffic patterns in this analysis. If you would like us to complete a more refined model run as part of your study, please contact us.

To determine the growth rates, traffic count and socioeconomic data should be used. Traffic count data is available on the SEMCOG web site at: <u>www.semcog.org</u>. Further study of the socioeconomic impacts to the study area is highly recommended.

If you have any questions regarding the enclosed information, please give me a call at 313-961-4266.

Sincerely,

Stephanice & Dayslow

Stephanie J. Taylor Senior Transportation Planner

Cc: Li-yang Feng, Coordinator

Joan Flynn Chairperson Commissioner, Macomb County Maryonn Mahaffey

immediate Past Chair

Council President.

City of Detroit

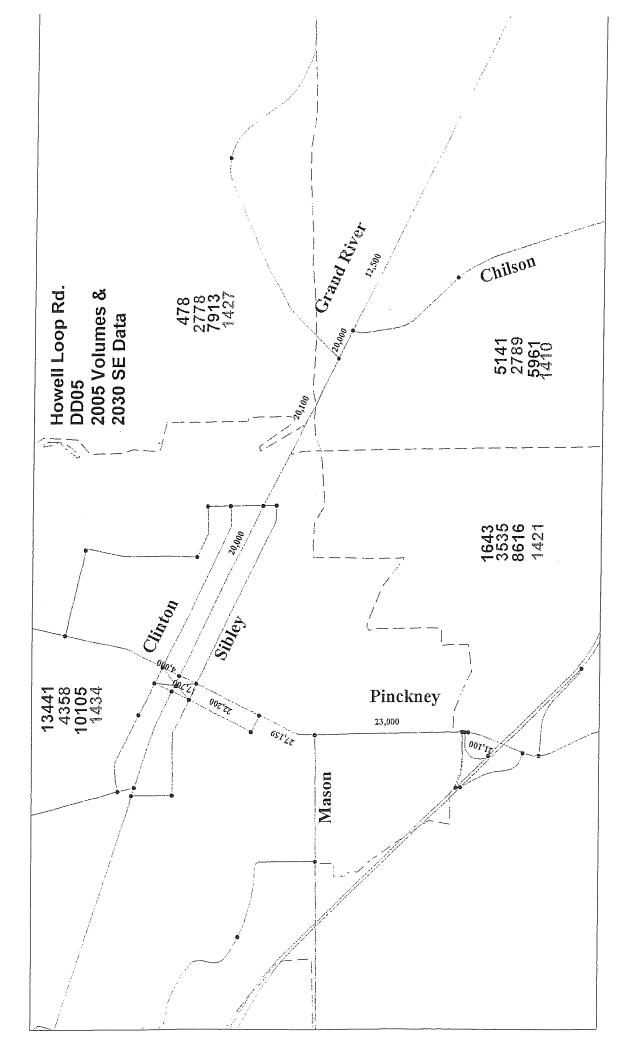
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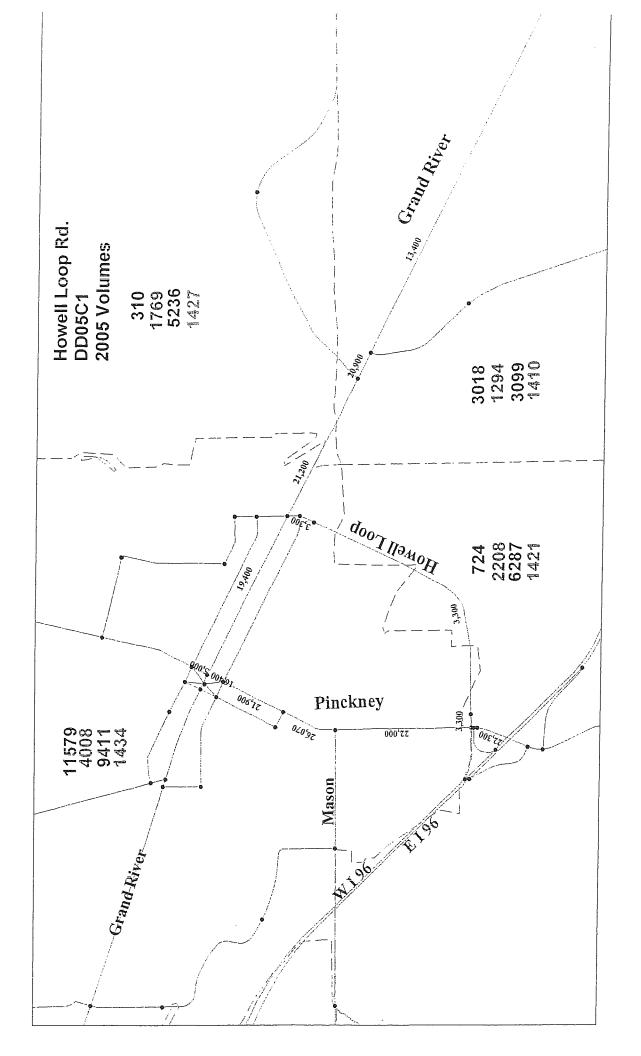
|            | 20(        | 2005 Socioecono       | omic Data  | 2030       | 2030 Socioeconomic Data |            | Since<br>And<br>And<br>And<br>And<br>And<br>And<br>And<br>And<br>And<br>And |                        | 1/0/     |
|------------|------------|-----------------------|------------|------------|-------------------------|------------|---|------------------------|----------|
|            |            |                       |            | 2001       | 111010000000            |            |   | vitality recentade (%) | ade (%)  |
|            | Population | Population Households | Employment | Population | Households              | Employment | POP   | HH                     | EMP      |
| 1410       | 3,099      | 1,294                 | 3,018      | 18 5,961   | 2.789                   |            | 1. (  | <del>+</del>           | 70 U 20/ |
| TOTT       |            |                       |            |            |                         |            | 0/ F.J.   | 0/0.01                 | 0/ 0· 0/ |
| 1441       | 0,28/      |                       |            | 724 8,616  | 3.535                   | 1 643      | 37 0%   | 60 1%                  | 106 0%   |
| 107        |            |                       |            |            |                         | -          |   |                        | 0.01     |
| 1421       | 0,230      | 1,/69                 |            | 310 7,913  | 2.778                   | 3 478      | 51 1%   | 57 0%                  | 51 201   |
| LOL F      | T T T T    |                       |            |            |                         |            |   | 0,0.10                 | 0/ 1.40  |
| 1404       | J 3,4 1    |                       | A/G, L1    | /9] 10,105 | 4,358                   | 3 13,441   | 7.4%  | 8.7%                   | 16 1%    |
| Totol/Aug  |            |                       |            |            |                         |            |   |                        |          |
| I Ulal/Avy | 24,033     | B/Z/A                 | 15,631     | 31 32,595  | 13,460                  | 20,703     | 35.6%   | 45.1%                  | 32 4%    |

Table 1. Projected Howell Loop Rd. Zones Socioeconomic Data Chandes Between Model Years 2005 and 2030

Tatile 2. Projected Howell Loop Rd. Volume Changes Between Model Runs Base 2005 and Alt. 2005

|           |                   |                       |              |                | 1       |                     |                |              |        |
|-----------|-------------------|-----------------------|--------------|----------------|---------|---------------------|----------------|--------------|--------|
|           | Namo              | Inters                | Intersection |                |         | Changing            | No             | No. of Lanes | F      |
|           |                   | From                  | Tọ           | 10 A CUU2 9480 |         | Percentage (%) AB05 |                | 5 CENTOS     | T      |
| 4813      | Grand River       | Pinckney              | Howell Loop  | 20,000         | 19.400  |                     | 0              | 6            |        |
| 4814      | Grand River       | Howell Loop Golf Club | Golf Club    | 20.100         | 21,200  |                     | <u>1</u> C     | <br>         |        |
| 4815      | Grand River       | Golf Club             | Chilson      | 20,000         | 20.900  | -                   | 10             |              |        |
| 4816      | Grand River       | Chilson               | Latson       | 12.500         | 13 400  |                     | 10             |              |        |
| 5189      | Pinckney          | 1-96                  | Howell Loop  | 21.100         | 22,300  |                     | <u>1</u> C     | - c          |        |
| 5192      | Pinckney          | Howell Loop           | Mason        | 23.000         | 22 000  | 0/ //0              | <u> </u>       |              | 2 - 24 |
| 48784954  | 48784954 Pinckney | Mason                 | Sibley       | 24.650         | 24 000  | -2.6%               | J Ŧ            |              |        |
| 49534952  | 49534952 Pinckney | Sibley                | Clinton      | 10.850         | 10,700  | -1.4%               | - +            |              |        |
| 20032     | 20032 Howell Loop | Grand River           |              |                | 3 300   |                     | - c            | - 0          |        |
| 20033     | Howell Loop       |                       |              |                | 000000  |                     | J <del>-</del> | D T          |        |
| 20034     |                   |                       | Pinckney     |                | 3,300   |                     | - 0            | - c          |        |
| Total/Avg |                   |                       |              | 176,700        | 214,600 | 21.4%               | 1              |              |        |
|           |                   |                       |              |                |         |                     | -              | -            | -      |







Rusty Orben - Director, State Relations State Government and Community Affairs

500 Water Street, J-150 Jacksonville, Florida 32202

March 31, 2025

Via Email Attachment

The Honorable Jason Woolford N-899 House Office Building P.O. Box 30014 Lansing, MI 48909

#### **Re:** CSX Support – City of Howell Grade Separation Funding Request

Dear Representative Woolford:

I write to provide CSX Transportation's support to the City of Howell's request for state funding towards improvements at the D-19 and I-96 interchange. This project will advance important public safety projects, including a critical bypass road and a grade separation and at-grade crossing elimination.

CSX Transportation has been engaged with City on mitigation efforts around occupied crossings due to normal rail service to local and regional customers. Our team has made adjustments to railroad operations in response to the City's requests since 2024. However, as you know, the only way to permanently address the issue is to eliminate crossings altogether. To that end, CSX stands ready to support the City's request for funding towards this local project.

Should you have any questions or require additional information, feel free to contact me directly.

Sincerely,

May L

Rusty Orben Director of State Relations – Ohio & Michigan CSX Transportation, Inc.

Michael J. Murphy Sheriff Jason C. Pless Undersheriff

#### LIVINGSTON COUNTY

# OFFICE OF THE SHERIFF

150 S. HIGHLANDER WAY • HOWELL, MICHIGAN 48843 TELEPHONE (517) 546-2440 • FAX (517) 552-2542

March 25, 2025

Dear Representative Woolford,

Please allow this correspondence to serve as overwhelming support for any funding that can improve the I-96/D-19 interchange in Howell and request your support in constructing a new roundabout. This area is already a hot mess, and with future development it will only get worse. This area was never designed to handle the amount of traffic it sees daily. Improvements are needed to enhance our transportation network's functionality, safety, and future resilience.

As you know, traffic congestion at this interchange has long been a challenge. This is compounded by the frequent blockage of South Michigan Avenue (D-19) and other roads at train crossings in the area. These backups disrupt daily commutes and pose significant safety risks, as emergency response vehicles are often delayed in reaching their destinations during peak congestion.

This area experiences severe congestion, causing delays and challenges for residents, businesses, and commuters alike. More critically, the congestion hinders emergency response vehicles, slowing their ability to reach those in need quickly and safely. A roundabout would effectively address these issues by offering:

- 1. **Smoother Traffic Flow**: This modern design would reduce stop-and-go delays, facilitating faster and more efficient movement through this busy area.
- 2. Enhanced Emergency Response: By improving accessibility and alleviating bottlenecks, emergency vehicles can navigate the interchange more efficiently, saving precious time in critical situations.
- 3. **Future-Ready Infrastructure**: The proposed roundabout design accommodates the planned **loop road**, ensuring the interchange remains functional and sustainable as our community grows.

This project represents a significant opportunity to create a safer, more reliable transportation network for our county while demonstrating a forward-thinking approach to urban planning. We ask you to advocate for this vital improvement and work with your colleagues to allocate the funds necessary to bring this vision to life.

Thanks in advance for your support of this important project.

Michael J Murphy - Sheriff



### **HOWELL AREA FIRE AUTHORITY**

1211 W. GRAND RIVER AVENUE, HOWELL, MI 48843 EMAIL: hafdmain@gmail.com PHONE: (517) 546-0560

Dear Representative Woolford,

We hope this letter finds you well. We are reaching out to emphasize the urgent need for funding improvements to the I-96/D-19 interchange in Howell and request your support in constructing a new roundabout. This is a crucial step toward enhancing our transportation network's functionality, safety, and future resilience.

As you may be aware, traffic congestion at this interchange has long been a challenge. This is compounded by the frequent blockage of South Michigan Avenue (D-19) and other roads at train crossings in the area. These backups disrupt daily commutes and could pose significant safety risks, as emergency response vehicles are sometimes delayed in reaching their destinations during peak congestion.

The current design of this exchange does not meet the demands of our rapidly growing community. Livingston County has been the highest growth rate county in Michigan for many years. This area experiences severe congestion, causing delays and challenges for residents, businesses, and commuters alike. The congestion can hinder emergency response vehicles, slowing their ability to reach those in need quickly and safely. A roundabout would effectively address these issues by offering:

- 1. **Smoother Traffic Flow**: This modern design would reduce stop-and-go delays, facilitating faster and more efficient movement through this busy area.
- 2. Enhanced Emergency Response: By improving accessibility and alleviating bottlenecks, emergency vehicles can navigate the interchange more efficiently, saving precious time in critical situations.
- 3. **Future-Ready Infrastructure**: The proposed roundabout design accommodates the planned **loop road**, ensuring the interchange remains functional and sustainable as our community grows.

This project represents a significant opportunity to create a safer, more reliable transportation network for our city while demonstrating a forward-thinking approach to urban planning. We ask you to advocate for this vital improvement and work with your colleagues to allocate the funds necessary to bring this vision to life.

Ronald Hicks Fire Chief







### Livingston County Emergency Management



1911 Tooley Road Howell, Michigan 48855 Telephone 517.540-7926 Fax 517.546.6788



**Emergency Management Director: Therese Cremonte** 

Dear Representative Woolford,

March 25, 2025

We hope this letter finds you well. We are reaching out to emphasize the urgent need for funding improvements to the I-96/D-19 interchange in Howell and request your support in constructing a new roundabout. This is a crucial step toward enhancing our transportation network's functionality, safety, and future resilience.

As you may be aware, traffic congestion at this interchange has long been a challenge. This is compounded by the frequent blockage of South Michigan Avenue (D-19) and other roads at train crossings in the area. These backups disrupt daily commutes and pose significant safety risks, as emergency response vehicles are often delayed in reaching their destinations during peak congestion.

The current design of this exchange does not meet the demands of our rapidly growing community.

Livingston County has been the highest growth rate county in Michigan for many years. This area experiences severe congestion, causing delays and challenges for residents, businesses, and commuters alike. More critically, the congestion hinders emergency response vehicles, slowing their ability to reach those in need quickly and safely. A roundabout would effectively address these issues by offering:

1. Smoother Traffic Flow: This modern design would reduce stop-and-go delays, facilitating faster and more efficient movement through this busy area.

2. Enhanced Emergency Response: By improving accessibility and alleviating bottlenecks, emergency vehicles can navigate the interchange more efficiently, saving precious time in critical situations.

Livingston County Emergency Management Department

3. Future-Ready Infrastructure: The proposed roundabout design accommodates the planned loop road, ensuring the interchange remains functional and sustainable as our community grows.

This project represents a significant opportunity to create a safer, more reliable transportation network for our city while demonstrating a forward-thinking approach to urban planning. We ask you to advocate for this vital improvement and work with your colleagues to allocate the funds necessary to bring this vision to life.

Thank you for your attention to this critical matter. We are happy to provide additional details or discuss this project at your earliest convenience.

Sincerely,

Revere Cremonto

Therese Cremonte P.E.M. Emergency Management Director Livingston County Emergency Management



MICHAEL DUNN Chief of Police 611 E. Grand River \* Howell, MI 48843 (517) 546-1330 \* FAX (517) 546-2114

POLICE DEPARTMENT

Dear Representative Woolford,

03/25/2025

I hope this letter finds you well. I am reaching out to emphasize the urgent need for funding improvements to the I-96/D-19 interchange in Howell and request your support in constructing a new roundabout. This is a crucial step toward enhancing our transportation network's functionality, safety, and future resilience.

As you may be aware, traffic congestion at this interchange has long been a challenge. This is compounded by the frequent blockage of South Michigan Avenue (D-19) and other roads at train crossings in the area. These backups disrupt daily commutes and pose significant safety risks, as emergency response vehicles are often delayed in reaching their destinations during peak congestion. Most recently the transport of a 14-year-old critically injured car accident victim had to be re-routed back through the crash scene by EMS due to the train stoppage on South Michigan Avenue in order to get the child to Mott Children's Hospital.

The current design of this exchange does not meet the demands of our rapidly growing community. Livingston County has been the highest growth rate county in Michigan for many years. This area experiences severe congestion, causing delays and challenges for residents, businesses, and commuters alike. More critically, the congestion hinders emergency response vehicles, slowing their ability to reach those in need quickly and safely. A roundabout would effectively address these issues by offering:

- 1. **Smoother Traffic Flow**: This modern design would reduce stop-and-go delays, facilitating faster and more efficient movement through this busy area.
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3. **Future-Ready Infrastructure**: The proposed roundabout design accommodates the planned **loop road**, ensuring the interchange remains functional and sustainable as our community grows.

This project represents a significant opportunity to create a safer, more reliable transportation network for our city while demonstrating a forward-thinking approach to urban planning. We ask you to advocate for this vital improvement and work with your colleagues to allocate the funds necessary to bring this vision to life.

Thank you for your attention to this critical matter. We are happy to provide additional details or discuss this project at your earliest convenience.

Respectfully,

Michael P. Dunn **Chief of Police**